

# Combined surface acoustic wave and surface plasmon resonance measurement of collagen and fibrinogen layer physical properties

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## Abstract

We use an instrument combining optical (surface plasmon resonance) and acoustic (Love mode surface acoustic wave device) real-time measurements on a same surface for the identification of water content in collagen and fibrinogen protein layers. After calibration of the surface acoustic wave device sensitivity by copper electrodeposition and surfactant adsorption, the bound mass and its physical properties – density and optical index – are extracted from the complementary measurement techniques and lead to thickness and water ratio values compatible with the observed signal shifts. Such results are especially usefully for protein layers with a high water content as shown here for collagen on an hydrophobic surface. We obtain the following results: collagen layers include  $70\pm 20\%$  water and are  $16\pm 3$  to  $19\pm 3$  nm thick for bulk concentrations ranging from 30 to 300  $\mu\text{g/ml}$ . Fibrinogen layers include  $50\pm 10\%$  water for layer thicknesses in the  $6\pm 1.5$  to  $13\pm 2$  nm range when the bulk concentration is in the 46 to 460  $\mu\text{g/ml}$  range.

*Keywords:* surface acoustic wave, surface plasmon resonance, collagen, fibrinogen, density, thickness

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## 1. Introduction

Sorption processes at the solid/liquid interface by which (bio)molecules bind to material surfaces are of interest for biosensors, biomaterials, material and surface science. Understanding the three-dimensional organization (including  
5 density, solvent content and thickness) of the resulting sorbed film and its evolution during the adsorption process is crucial for many applications in these domains. For biosensors, more specifically, there is a need to monitor the response in real-time, in order to assess the adsorption kinetics, and to be able to

distinguish contributions coming from the dry sorbed mass, which is the physical  
10 criterion for estimating sensitivity, and those that should be attributed to effects  
intimately associated to the layer organization, like sorbent-bound water and  
hydrodynamic effects for example. While a wide variety of methods can qualita-  
tively detect the formation of the sorbed film, almost none of them, taken alone,  
is quantitative and able to reveal the film organization, and only few can moni-  
15 tor the process in real-time. Scanning probe microscopies might fulfill all these  
requirements, mainly for submonolayers sorbed on smooth surfaces [1]. Neutron  
reflectivity [2], X-ray Photoelectron Spectroscopy (XPS) [3], mass spectroscopy  
and radiolabeling are quantitative techniques able to directly measure the dry  
sorbed amount. Of all the direct detection (*i.e.* label-less) techniques, we have  
20 identified acoustic and optical methods as being the only ones fulfilling two fun-  
damental criteria of our measurements: time resolved and in-situ (liquid phase)  
measurement of the physical properties of the adsorbed layer.

Various methods of direct detection of biochemical layers have been devel-  
oped, either based on the disturbance of an acoustic wave [4] (quartz crystal  
25 microbalance [5] – QCM – and surface acoustic wave devices [6] – SAW) or of an  
evanescent electromagnetic wave (optical waveguide sensors [7, 8], surface plas-  
mon resonance [9, 10] – SPR). While each one of these transducers individually  
provides reliable qualitative curves during protein adsorption on their function-  
alized surfaces, extraction of quantitative physical parameters such as optical  
30 index, density, viscosity or water content requires modeling of the adsorbed lay-  
ers [11]. The modeling includes multiple parameters which must be identified  
simultaneously: hence the need for the combination of (acoustic and optical)  
detection methods in a single instrument [12, 13, 14, 15] to separate contribu-  
tions as a same layer is reacting with the surface under investigation. Multiple  
35 investigators have identified such a combination of measurement methods as  
fruitful means of extracting independent physical properties of adsorbed layers,  
including the challenging combination of QCM and SPR [16, 17, 18, 19, 20]  
or comparing the results of successive experiments using different instruments  
[21, 22, 23, 24], combining QCM and reflectometry [25] or measuring separately  
40 using the two techniques [26], or SAW and SPR [27].

We here use a combination of Love mode SAW device and SPR to identify  
values of density, water content and thickness of surfactant films and protein  
layers (collagen and fibrinogen) adsorbed on methyl-terminated surfaces. This  
combined measurement is necessary when attempting to convert a raw signal as  
45 observed at the output of a transducer (angle shift for SPR, phase and magni-  
tude shift for SAW or frequency and damping for a QCM) to the actual protein  
mass bound to the surface, which is the physical criterion for estimating the  
expected highest possible sensitivity of a biosensor since it provides an esti-  
mate of the density of active sites on the surface. We furthermore compare the  
50 signals obtained from quartz crystal microbalance with dissipation monitoring  
(QCM-D [28, 29]) measurements to that of the SAW and, based on the results  
obtained from the analysis of the SAW/SPR combination, show how SAW and  
QCM interact differently with the layer. The QCM displays a strong sensitivity  
to viscous interactions with adsorbed layers as was shown previously [30, 31].

55 SAW devices are sensitive to mass loading, visco-elastic interactions and electrical charge accumulation on the sensing area [32], but with different influences due to the different frequencies and hence penetration ratio of the shear acoustic wave with respect to the layer thickness.

Love mode surface acoustic waves were chosen for their high mass sensitivity and their compatibility with measurements in liquid media [33, 34, 35, 36]. Being based on the propagation of a shear horizontal acoustic wave, their interaction with the surrounding liquid is restricted to an evanescent coupling with the viscous liquid. Although bulk liquid viscosity properties affect the acoustic wave propagation [37, 38], including the phase shift of Love mode SAW [39], we will throughout this investigation consider that the phase shift affecting the SAW device is solely related to adsorbed mass and not to viscous effects of the adsorbed layer, in order to reduce the number of unknowns. Such a crude assumption could be removed by exploiting the SAW insertion losses, for introducing the adsorbed layer viscosity. Throughout the analysis proposed here, we consider hydrodynamic interactions of the acoustic wave with the solvent filled adsorbed layer, as well as the equivalent optical index of the protein-solvent mixture, without focusing on the dynamic viscosity of this adsorbed layer but only on the viscosity of the fluid yielding shear wave evanescent coupling with the solvent.

75 The chosen protein layers consist of collagen and fibrinogen, selected as references both for their interest in engineering biocompatible surfaces [40, 41] but most significantly for their strong solvent content and hence acoustic properties challenging to analyze. Collagen is a fibrillar protein of the extracellular matrix possessing self-assembly properties, involved in biorecognition processes. The collagen macromolecule consists of a triple helix with dimensions about 300 nm in length and about 1.5 nm in diameter, and weights about 300 kilodaltons [42]. Organization of collagen films adsorbed on hydrophobic surfaces - CH<sub>3</sub> - terminated self-assembled monolayers (SAMs) and polystyrene - from 30 to 40  $\mu\text{g}/\text{ml}$  - were fully characterized under water or after drying using AFM [43, 44], X-ray photoelectron spectroscopy [45] and radioassays. By AFM scratching experiments, thicknesses of the film adsorbed on methyl-terminated surfaces was estimated to be about 20 nm under water and 7-8 nm after drying. Furthermore, it was found that the measurement was strongly influenced at weak applied forces ( $<0.5$  nN), in relation with the long-range repulsion ( $\sim 50$  to  $\sim 250$  nm) observed by AFM force-distance curves, strongly suggesting that at least some molecules of the film must protrude into the solution [44]. Adsorbed amount of (dry) collagen on methyl-terminated surfaces were estimated to be between 0.4 and 0.8  $\mu\text{g}/\text{cm}^2$  by combining AFM and XPS measurements. Values near 0.5  $\mu\text{g}/\text{cm}^2$  were determined to be adsorbed on polystyrene by radiolabeling.

Fibrinogen, on the other hand, is a blood protein that presents three globular domains linked together by fibrillar segments. Similarly to collagen, its molecular weight is about 340 kilodaltons. Fibrinogen adsorbed on various surfaces has been imaged by AFM as well [46], down to molecular resolution [47, 48, 49, 50].

100 In this presentation, similar films will be investigated, but under the new

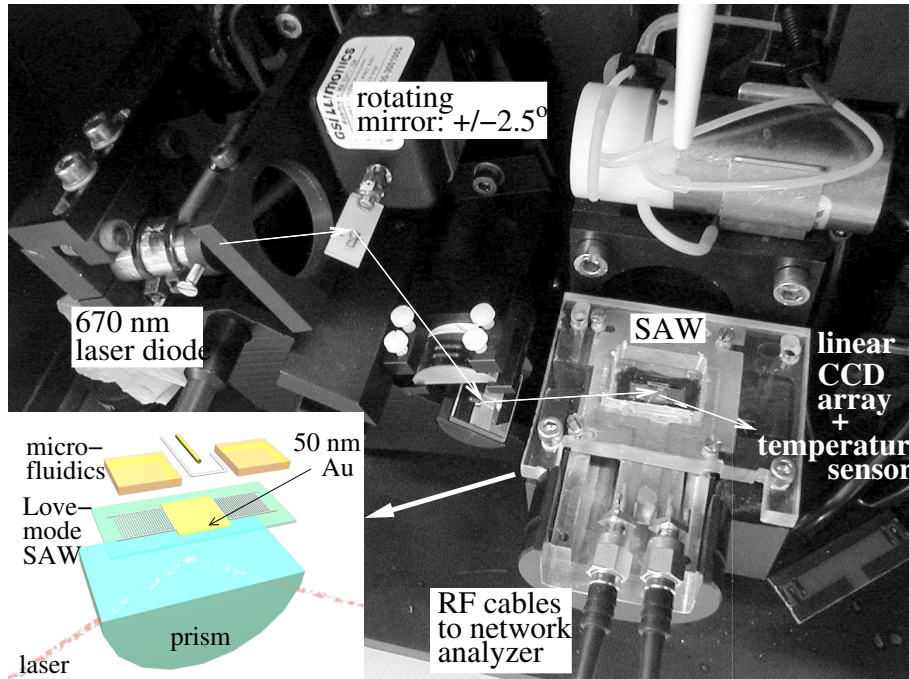


Figure 1: Picture of the experimental setup combining a SPR instrument (670 nm-wavelength laser with mechanical sweep of the illumination angle) with a piezoelectric (ST-cut quartz) substrate acting as both SPR sensing area since coated with a 50-nm Au layer and propagating a Love-mode SAW. Bottom-left inset: schematic view of the measurement head, emphasizing the need for integrated microfluidics to prevent liquid from reaching the interdigitated transducers. In this schematic chart, an electrochemical application is considered by showing the (bent) counter electrode and (straight) reference electrode located over the gold-coated sensing area acting as working electrode.

perspective of combined acoustic and optical measurements for extracting the thickness, mass, and solvent density in a buffer medium. While the SAW/SPR technique (Fig. 1) and data processing with our proposed formalism was already shown [51] to be appropriate in the identification of some physical properties of a rigid adsorbed layer (S-layer) [52], we here quantitatively analyze the organization of collagen and fibrinogen adsorbed layers which are expected to possess a substantial water content. This condition is expected to lead to the largest differences between acoustic and optical signals since both techniques respond differently to a viscous (solvent containing) layer: acoustic methods tend to overestimate the bound mass due to hydrodynamic interactions, while optical methods provide an estimate of the dry bound mass after appropriate modeling of the response but cannot resolve both parameters, thickness and optical index of the layer which SPR is sensitive to. This optical index can be assumed to be the weighted value of the index of water and that of proteins to the volumic part that these components occupy in the film. SPR response is thus dependent

on the film organization and on the dry adsorbed amount.

Unlike the model used in other studies [53], we here assume that the SAW device signal shift is predominantly due to added rigidly bound mass on the electrode. Indeed we have shown that, while the QCM is sensitive via hydrodynamic interactions with the topography induced by rough copper electrodeposition [54], SAW is much less sensitive [55]. The contribution of the wave coupling with the viscous fluid to the phase shift [39] will be neglected throughout this investigation. Indeed, collagen films were analyzed using SAW/SPR after different conditionings, inducing a different film organization and related viscoelastic behavior (as probed by AFM and QCM respectively) for a similar adsorbed amount. These differences in the film properties were found to result in only minor changes in the SAW response. For all these reasons, the SAW phase response is considered in this article to be only mass dependent during adsorption phenomena. Hence, we use a proportionality relationship between the mass of the layer  $\Delta m$  per unit area  $A = 5 \times 5.5 \text{ mm}^2$  here ( $\Delta m/A$ ) – including the rigidly bound water – and the frequency shift:  $\frac{\Delta m}{A} = \frac{\Delta f}{S \times f_0}$  where  $f_0$  is the frequency at which the phase is monitored in an open-loop configuration,  $\Delta f$  is the frequency shift obtained after conversion from phase to frequency shift through the experimentally measured phase to frequency linear relationship, and  $S$  is the mass sensitivity calibrated by copper electrodeposition. Since the mass sensitivity calibration is a central part in extracting quantitative results from the experimental data, we confirm the results obtained with copper electrodeposition by measuring the SAW signal change during adsorption of a surfactant, cetyltrimethylammonium bromide (CTAB). Hence, four sets of experiments will be described in the experimental section below, after presenting the instrument setup:

1. experimental calibration of the gravimetric sensitivity of the SAW transducer in liquid phase is a core step to the quantitative analysis: such a step is performed by reversible copper electrodeposition, allowing for multiple cycles under different deposited mass configurations to be repeated,
2. because the mechanical properties and surface roughness of copper differ from the biofilm we are investigated, the calibration is validated using CTAB monolayer deposition,
3. collagen thick films will be assembled on the surface under different bulk concentrations,
4. fibrinogen thick films will be assembled on the surface under different bulk concentrations.

## 2. Experimental section

**Instrumentation** The combined SAW/SPR instrument developed for performing this experiment has been described previously [52]: a modified Ibis II SPR instrument (IBIS Technologies BV, Netherlands) is used to inject a 670 nm laser in a quartz substrate (Kretschmann configuration) and monitor the reflected intensity *vs.* angle with an accuracy of  $\pm 2.555^\circ/200$  pixels at two

locations separated by about 2 mm on the sensing surface. The ST-cut quartz  
160 substrate is patterned with double-fingers interdigitated electrode for launching  
a Love mode acoustic wave at a center frequency of 123.5 MHz. The guiding  
layer is made of a 1.13  $\mu\text{m}$  thick PECVD silicon dioxide layer. The phase and  
insertion loss of the acoustic wave device are monitored using an HP 4396A  
network analyzer while a custom software records the full reflected intensity *vs.*  
165 angle SPR curve. The  $5 \times 5.5 \text{ mm}^2$  sensing area is coated by e-gun evaporation  
with nominal thicknesses of 10 nm *Ti* and  $50 \pm 5 \text{ nm Au}$  to support surface plas-  
mon resonance, and is either grounded to minimize varying salt concentration  
effects on the signal measured by the SAW device during biological experi-  
ments, or connected as the working electrode during copper electrodeposition  
170 calibration through a bias-T circuit. Both sets of data – SAW phase at a given  
frequency and SPR reflected intensity curves – are time stamped with an ac-  
curacy of 1 second on the common personal computer internal clock reference  
for future processing, which for the SPR curve involves polynomial fitting for  
improving 100-fold the accuracy on the localization of the reflected intensity  
175 minimum. The temperature coefficient of the Love mode device has been mea-  
sured to be  $34 \pm 1 \text{ ppm/K}$ , in agreement with values reported in the literature  
[36], and the insertion loss is in the -22 dB to -30 dB range when the grounded  
sensing area is covered by a liquid. Both dual-finger interdigitated transducers  
(wavelength: 40  $\mu\text{m}$ ) are protected from the liquid by a 100  $\mu\text{m}$ -high SU8 wall  
180 capped with a piece of quartz forming sealed protective chambers [56]. The sides  
of the SAW devices are glued to an  $7 \times 17 \text{ mm}$  opening in a 1.6 mm-thick epoxy  
(FR4) printed circuit board (PCB) with the bottom area of the SAW tangent to  
the PCB, allowing optical contact between the bottom surface of the SAW de-  
vice and a cylindrical prism through optical index matching oil ( $n_{oil} = 1.518$ ).  
185 After wire bonding the SAW device to the PCB, the region surrounding the  
SAW device is coated with 1 mm wide, 1-2 mm thick epoxy walls using H54  
two-parts epoxy glue (Epoxy Technology, Billerica, MA, USA), forming a 180  
to 200  $\mu\text{l}$  open well in which the solution is injected using a micropipette.

While both SPR and SAW sensors display theoretically similar sensitivities  
190 and detection limits [57], the acoustic sensor is extremely sensitive to temper-  
ature variations and care must be taken to properly control the environment  
around the instrument to keep the temperature stable [12].

Recording all SPR curves of the reflected intensity *vs.* angle during the  
experiment for post-processing is required since the shape of the dip is unusual  
195 (Fig. 2) and cannot be processed properly by the commercial software provided  
with the instrument which expects the substrate to be glass. As seen in Fig.  
2 in which the reflected intensity *vs.* angle curve is displayed, the periodic  
dips observed when the gold coated SAW sensor is placed over the half-cylinder  
prism *in air* is attributed to the birefringence of quartz which is the cause of  
200 the interference pattern after reflection of the laser on the metallic surface [52].  
The orientation of the quartz substrate on which the SAW propagates has been  
chosen on purpose to separate as much as possible the successive interference  
minima. The dip due to SPR is identified when the surface is coated with water,  
and the position of this dip only is monitored over time. A typical raw SPR

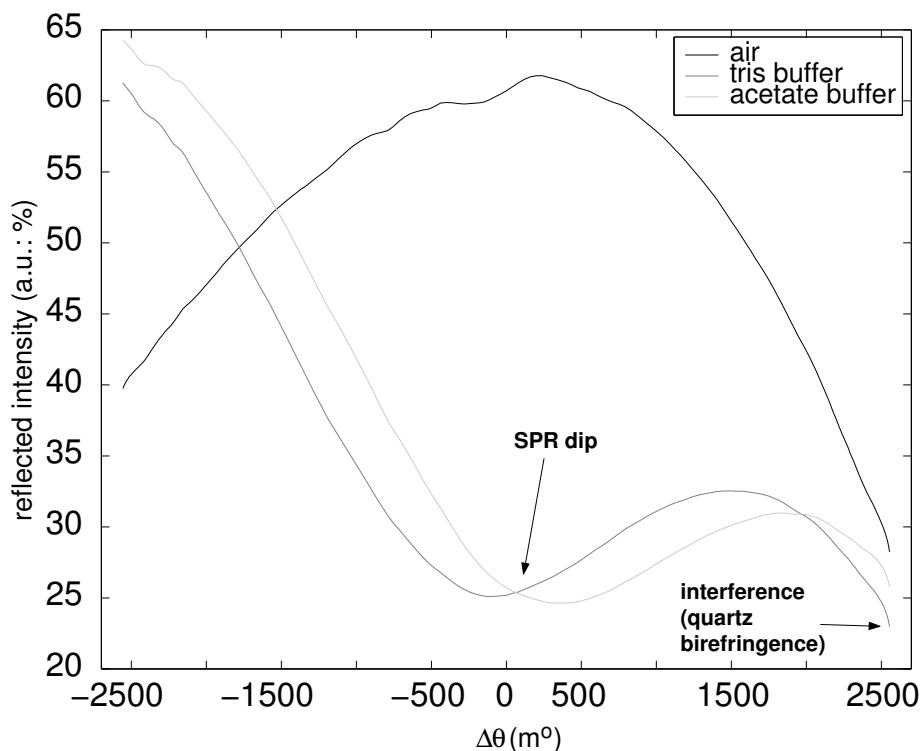


Figure 2: SPR dip observed on a quartz substrate coated with  $1.13 \mu\text{m}$   $\text{SiO}_2$  and  $10+50 \text{ nm}$   $\text{Ti} + \text{Au}$ . Notice the additional features on both angle extrema of the curve attributed to interference from quartz birefringence.

205 reflected intensity *vs.* angle curve is displayed in Fig. 2: the mean incidence angle is about  $72 \pm 2^\circ$  (not calibrated in the Ibis II instrument) and the abscissa is graduated in relative angle shift.

The QCM-D measurements were performed using the electronics supplied by Q-Sense AB (Sweden) using AT-quartz plano-plano resonators (Chintele Quartz  
 210 Technology Co. Ltd, Zhejiang, P.R. China) coated, by evaporation, with  $10 \text{ nm}$   $\text{Ti}$  and  $50 \text{ nm}$   $\text{Au}$ , key-hole shaped counter electrode and fully coated sensing electrode, leading to a fundamental resonance frequency around  $4.7 \text{ MHz}$  and a quality factor in liquid around  $5500$ . These experiments were performed both in a lab-made open cuvette and in the commercially supplied flow cell (with static  
 215 liquid during the measurement). Both sets of measurements are compatible. However, since the QCM setup is distinct from the SAW/SPR setup, we will not attempt any kinetics comparison between both datasets.

**Chemicals and Materials** The  $\text{Cu}$  electrodeposition step was performed using a solution of  $10^{-2} \text{ M}$   $\text{CuSO}_4$  in  $10^{-2} \text{ M}$   $\text{H}_2\text{SO}_4$ . The counter electrode was a  $0.25\text{-mm}$ -diameter platinum wire shaped in  $3/4$  of a circle and  
 220 the pseudo-reference electrode was made of a  $1 \text{ mm}$ -diameter  $99.98\%$  copper



wire (Huntingdon, UK), cleaned by briefly dipping in 70% nitric acid before use. The electrochemical reaction was controlled by a PC3-300 Gamry Instruments (Warminster, USA) potentiostat.

225 Collagen was supplied by Roche (Boehringer-Mannheim, Mannheim, Germany) as a sterile acidic solution of 3 mg/ml solution of collagen type I from calf skin. It was diluted in PBS buffer (137 mM  $NaCl$ , 6.44 mM  $KH_2PO_4$ , 2.7 mM  $KCl$  and 8 mM  $Na_2HPO_4$ ) to reach the wanted concentration just prior to use. Type I fibrinogen from human plasma was obtained from Sigma-  
 230 Aldrich. Both QCM and SAW/SPR  $Au$  sensing electrodes were coated with an octadecanethiol hydrophobic self-assembled layer, leading to a contact angle above  $110^\circ$ . Alkanethiols were self-assembled by dipping the QCMs in a  $10^{-3}$  M octadecanethiol (Sigma-Aldrich) solution in ethanol after a 15 minutes cleaning step in  $UV-O_3$  and rinsing with ethanol. The SAW devices were placed in a  
 235 chamber with an ethanol saturated atmosphere, and 150 to 180  $\mu l$  of the same thiol solution was deposited on the open well above the sensing area. Adsorption was subsequently allowed for 3 hours, after which the surfaces were rinsed with ethanol and dried under a stream of nitrogen. The thiol solution and later biochemical solutions are only in contact with the chemically inert H54 epoxy  
 240 glue and quartz slides capping the SAW device and never with the FR4 epoxy and copper of the PCB, thus minimizing risks of contamination of the solutions and of the sensing surface.

### 3. Results

#### 3.1. SAW sensitivity calibration

245 Figure 3 illustrates the calibration procedure using copper electrodeposition: a cyclic voltametry sweep from +600 mV to -60 to -100 mV (depending on the mass of copper to be deposited) *vs* a copper wire acting as a pseudo-reference electrode provides an estimate of the deposited mass, assuming a 100% efficiency of the electrochemical process. A current  $I_j$  is monitored by the potentiostat at a sampling rate of 5 Hz,  $j$  being a sample index.  
 250

By selecting the voltage range for which the current is negative (copper deposition), we obtain the deposited mass by numerical integration

$$M_{Cu} = \frac{\sum_j I_j \times \delta t}{F} \times \frac{m_{Cu}}{n_e}$$

where  $F$  is the Faraday constant (96440 C),  $\delta t = 0.2$  s is the time interval between two samples,  $m_{Cu} = 63.5$  g/mol is the molar weight of copper and  $n_e = 2$  the number of electrons required for copper reduction. Simultaneously the phase shift  $\Delta\phi$  of the SAW device due to the added mass is measured and converted to a frequency variation  $\Delta f$  via the linear phase to frequency relationship measured on the Bode plot:  $\Delta f/\Delta\phi = 1680 \pm 5$  Hz/ $^\circ$  in our case. Once the deposited mass is estimated, the SAW sensitivity  $S$  is computed considering  
 255 the center oscillation frequency  $f_0 = 123.2$  MHz, the working electrode area  $A$  and the frequency shift  $\Delta f$  due to the added mass:  $S = \frac{\Delta f}{f_0} \times \frac{\Delta m}{A}$ , leading to an



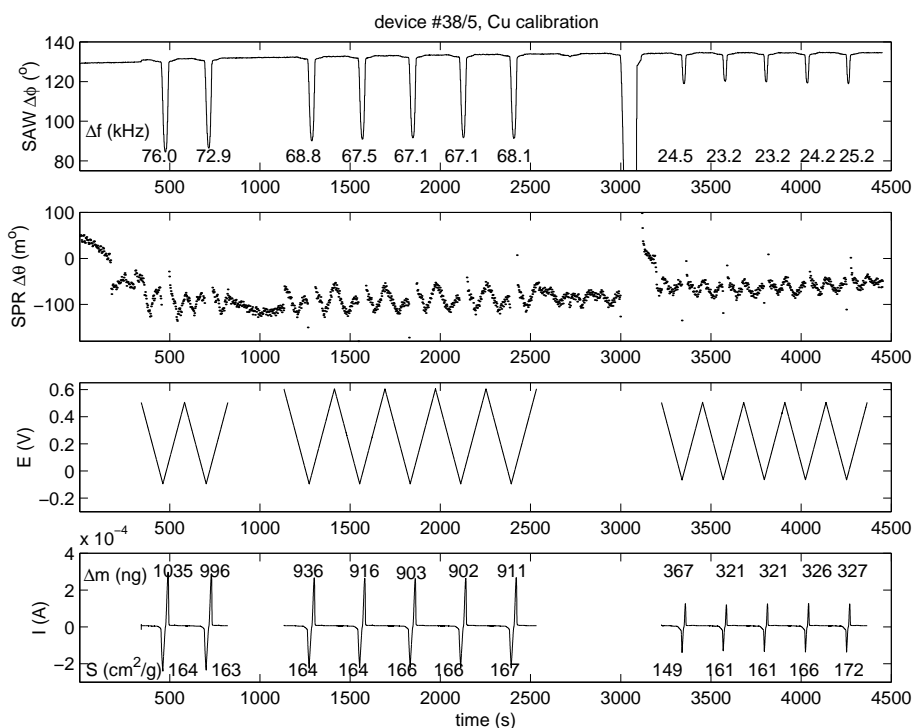


Figure 3: Copper electrodeposition calibration curve. The resulting experimentally measured sensitivity indicated on the bottom graph is  $165 \text{ cm}^2/\text{g}$ . From top to bottom: raw SAW phase shift and converted frequency shift via the phase to frequency linear relationship observed on the Bode plot; SPR angle shift showing fluctuations with the potential sweep due to electroreflectance effects; voltage applied to the potentiostat (*versus* a copper wire pseudo-reference electrode); current flowing through the potentiostat and, on top, the mass deposited on the sensing area obtained by integrating the current over time and converting to a mass of deposited copper, and bottom the experimentally measured sensitivity calculated knowing the frequency shift (top graph) and the deposited mass (bottom graph).

260 experimentally measured sensitivity of  $165 \pm 10 \text{ cm}^2/\text{g}$  for one SAW device and  $145 \pm 15 \text{ cm}^2/\text{g}$  for another similar sensor (data not shown), the difference being related to packaging issues and mostly the influence of the protective SU8 wall on the acoustic path.

265 Both values were confirmed with CTAB adsorption on octadecanethiol coated gold at a bulk concentration of  $1.3 \times 10^{-4} \text{ M}$ : the surface density of surfactant molecules upon adsorption on gold is known from the surface area per molecule of  $50 \text{ \AA}^2$  [58] and the molar weight of  $364 \text{ g/mol}$ , a mass per unit area of  $120 \text{ ng/cm}^2$  is deduced assuming the formation of a monolayer. The monolayer formation lead to a frequency shift of the SAW device of  $2.5 \text{ kHz}$  from which  
 270 a surface density of  $125 \text{ ng/cm}^2$  is obtained. Interestingly, the simultaneously observed SPR angle shift can only be interpreted with a layer of optical index at least 1.5, which leads to a layer thickness of  $1.5 \pm 0.5 \text{ nm}$  fully coated with CTAB

(no solvent) after simulation using the formalism described in [59] and following the procedure described in more details later in this article. The large uncertainty on the layer thickness is related to the low molecular weight of CTAB leading to a small mass increase which leads to a phase shift of only about 5 times the noise level of the SAW phase. Such a high optical index is compatible with that provided in the literature for thiol monolayers as an extension of the optical index of bulk alkane solutions [60]. The surface mass density is compatible with that observed with QCM-D measurements following the assumption of a rigid mass, as validated by the good overlap of curves obtained at overtones 3, 5 and 7 when normalized by the overtone number, and the low dissipation increase ( $\Delta D < 1 \times 10^{-6}$ ).

### 3.2. SAW/SPR measurements

Once the mass sensitivity of the SAW device is calibrated, the combined SAW and SPR measurements are used to monitor protein adsorption and extract the physical properties of the resulting films. Collagen and fibrinogen adsorption were performed on methyl-terminated surfaces of the SAW/SPR device at concentrations of 30 or 300  $\mu\text{g}/\text{ml}$  and 46 or 460  $\mu\text{g}/\text{ml}$  respectively. The sequence of solutions brought in contact with the sensing surface was successively PBS (or PBS-water-PBS), protein in PBS, PBS, water and finally PBS. Figure 4 displays a typical signal observed during collagen adsorption on an hydrophobic surface, for (a) 300  $\mu\text{g}/\text{ml}$  and (b) 30  $\mu\text{g}/\text{ml}$  bulk concentrations. Immediately after the conditioning with the collagen solution, both SAW and SPR show a clear response, reaching after about one hour a clear plateau or a beginning of a plateau, depending on the conditioning collagen concentration.

The SAW and SPR shifts at the end of the adsorption with a collagen concentration of 30  $\mu\text{g}/\text{ml}$  were respectively  $17.0 \pm 0.7^\circ$  and  $0.39 \pm 0.07^\circ$ , while a concentration of 300  $\mu\text{g}/\text{ml}$  lead to  $19.2 \pm 0.5^\circ$  and  $0.65 \pm 0.1^\circ$  for SAW and SPR respectively. Adding PBS, after collagen conditioning, resulted in very small loss ( $< 1^\circ$  for SAW and  $< 0.05^\circ$  for SPR) of the response, stable with time, and subsequent washing by water and PBS again provoked no signal change. This means that molecules do not desorb with time once adsorbed on the substrate. The SAW phase to frequency conversion factor as observed on the Bode plot is 1680 Hz/ $^\circ$ : the resulting frequency variation is translated into a bound mass thanks to the calibrated sensitivities – in our case 165 g/cm<sup>2</sup> or 145 g/cm<sup>2</sup> depending on the SAW device being used. The resulting hydrated collagen adsorbed films are estimated to weight  $1.75 \pm 0.15$  and  $2.10 \pm 0.20$   $\mu\text{g}/\text{cm}^2$  for the 30 and 300  $\mu\text{g}/\text{ml}$  solutions respectively.

Fig. 5 displays a similar measurement on 460  $\mu\text{g}/\text{ml}$  fibrinogen. A similar sequence of conditioning steps as previously presented for collagen were applied. PBS washing results in a stable loss of response attributable, like for collagen, to a loss of fibrinogen molecules physisorbed to the adsorbed film. There is again no significant desorption of adsorbed molecules. The observed shifts resulting from fibrinogen adsorption were  $14.0 \pm 0.7^\circ$  and  $0.65 \pm 0.1^\circ$  for SAW and SPR respectively. For SAW, using the same relations as was presented for col-

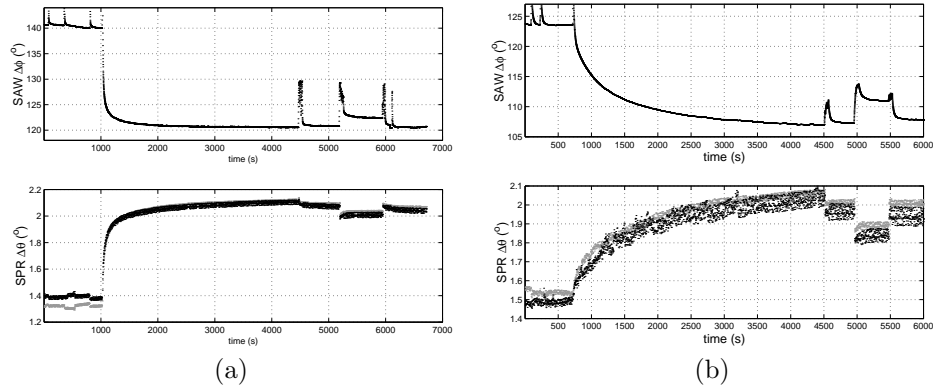


Figure 4: (a) 300  $\mu\text{g/ml}$  and (b) 30  $\mu\text{g/ml}$  collagen adsorption curves. Top: phase shift monitored at the constant frequency of  $f_0=123.2$  MHz, which can then be converted to an equivalent frequency shift as would be observed in a Phase-Locked Loop oscillator configuration via the linear phase to frequency relationship. During experiment (a), collagen adsorption lead to an insertion loss increase of 6.5 dB, from 22.9 dB when the sensing area is covered with buffer to 29.4 dB after collagen adsorption. During experiment (b), this insertion loss increased by 3.3 dB, from 24.4 dB prior to collagen adsorption to 27.7 dB after adsorption. Bottom: SPR dip position angle shift. The sequence is PBS buffer (3 solution exchanges in (a), 2 solution exchanges in (b)), collagen in the same PBS buffer, PBS rinsing step, DI water and PBS.

lagen, the surface density of the hydrated fibrinogen films were estimated to be  $0.75\pm 0.1$  and  $1.5\pm 0.3$   $\mu\text{g/cm}^2$  for 46 and 460  $\mu\text{g/ml}$  concentrations respectively.

### 3.3. QCM-D independent validation measurements

320 Collagen and fibrinogen adsorption were performed on methyl-terminated  
 QCM surfaces following the same conditions as were used for the SAW/SPR.  
 Changes in resonance frequency and dissipation of the first four odd overtones  
 were measured as a function of time. An example of a QCM-D measurement  
 is presented in Fig. 6 for the same 300  $\mu\text{g/ml}$  collagen as in Fig. 4 (b) but on  
 325 a different setup: both experiments (SAW/SPR and QCM) are based on a lab-  
 made open cuvette in which 200  $\mu\text{l}$  of the new solution is manually injected by a  
 micro-pipette. While the kinetics of the SAW and SPR data can be compared,  
 we will not attempt to compare it with the kinetics of the QCM since the  
 latter was included in a different setup – static well geometry does influence the  
 330 adsorption kinetic [61].

We will however see that the asymptotic behavior of both experiments per-  
 formed separately lead to the same conclusion, namely the large amount of water  
 trapped in the collagen layer. Frequency shifts are presented after normalizing  
 by the overtone number as classically done when assuming the adsorbed layer  
 335 to be rigidly bound to the sensing surface, and by the square root of the over-  
 tone number as would be expected for a strong hydrodynamic interaction [54].  
 The frequency responses of the different overtones do not overlap when normal-  
 ized by the overtone number while they do when normalized by the square root

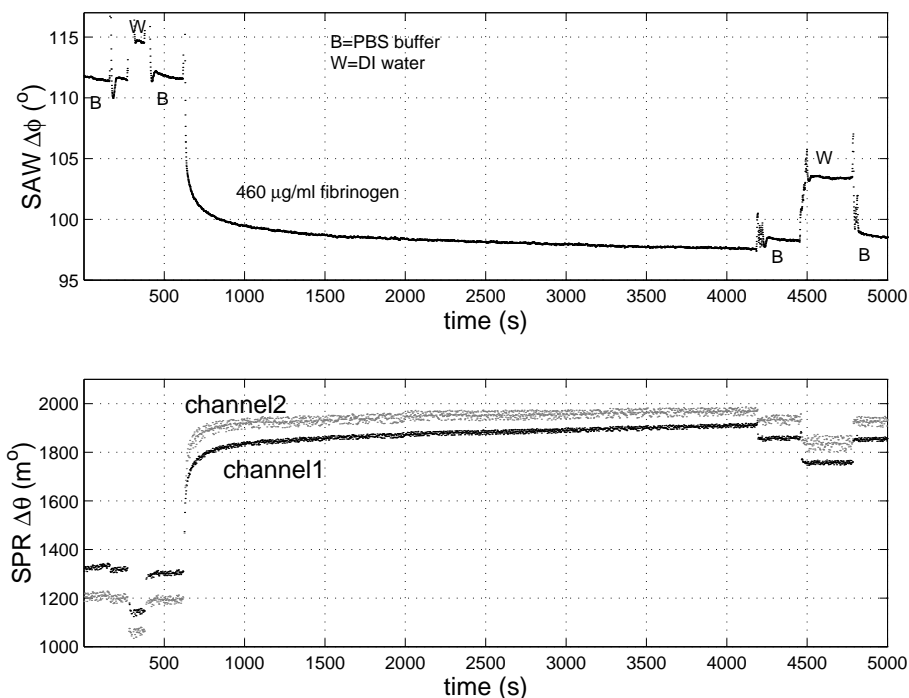


Figure 5: 460  $\mu\text{g}/\text{ml}$  fibrinogen adsorption curves. Top: phase shift monitored at the constant frequency of 123.2 MHz, which can then be converted to an equivalent frequency shift as would be observed in a Phase-Locked Loop oscillator configuration via the linear phase to frequency relationship. Fibrinogen adsorption lead to an insertion loss rise by 0.5 dB, from 23.0 dB prior to adsorption to 23.5 after adsorption. Bottom: SPR dip position angle shift. The sequence is PBS buffer (2 solution exchanges), DI water, PBS, fibrinogen in the same PBS buffer, PBS rinsing step, DI water and PBS.

of the overtone number, indicating a predominantly viscous interaction of the  
 340 QCM with the film and surrounding solvent. Leading to the same conclusion,  
 the dissipation rises to an enormous value above  $100 \times 10^{-6}$ . Quantitatively, if  
 this film was assumed to be a rigid layer, these frequency shifts would corre-  
 spond to wet masses in the range 8 to 12  $\mu\text{g}/\text{cm}^2$  as obtained by applying the  
 Sauerbrey relation. These values are far larger than the corresponding values  
 345 deduced by SAW measurements ( $2.10 \pm 0.20 \mu\text{g}/\text{cm}^2$ ). This points to the fact  
 that SAW measurements are far less sensitive to viscoelastic interactions with  
 the adsorbed film than the QCM. All measurements for collagen and fibrinogen  
 adsorptions at the different concentrations were performed and the characteris-  
 tic results as explained above are summarized in Table 1. The same conclusion  
 350 as above can be made in all cases, QCM measurements denoting a behavior of  
 the adsorbed film strongly interacting through hydrodynamic coupling with the  
 bound and surrounding solvent, and the corresponding wet adsorbed masses be-

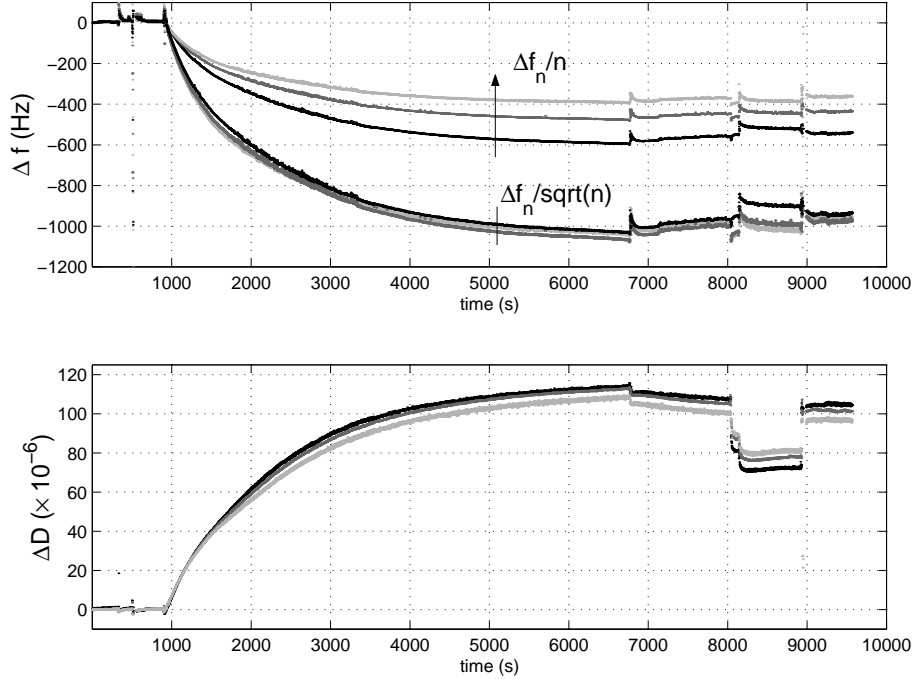


Figure 6: QCM-D 300  $\mu\text{g/ml}$  collagen adsorption experiment. Top: normalized QCM resonance frequency assuming a predominantly hydrodynamic interaction (scaling law as  $1/\sqrt{n}$  with  $n$  being the overtone number) and assuming a rigid layer (scaling law as  $1/n$ ). Notice that the latter set of curves do not overlap and hence the rigid mass hypothesis is not correct. Bottom: QCM dissipation monitoring. Notice the very large damping value reached ( $\Delta D > 100 \times 10^{-6}$ ).

ing always superior to those deduced by SAW. Fibrinogen shows less viscoelastic properties than the collagen film and lower protein concentrations result in a less viscoelastic behavior of the adsorbed film.

Notice the excellent agreement between our results and those cited in the literature about dry mass of collagen layers adsorbed under similar conditions as measured by AFM and XPS: 20 nm thick layers under water and 7-8 nm after drying [44], and adsorbed amount of (dry) collagen between 0.4 and 0.8  $\mu\text{g}/\text{cm}^2$  are consistent with our 19 $\pm$ 3 nm thick layers and a dry mass of  $2.1 \times 0.35 = 0.7 \mu\text{g}/\text{cm}^2$ , justifying our initial assumptions when modeling the adsorbed layer interaction with the acoustic and optical waves.

## 4. Discussion

### 4.1. Physical properties of the layers

The observed SAW phase shift monitored at 123.2 MHz thus translates into a surface mass density of  $1.75 \pm 0.15 \mu\text{g}/\text{cm}^2$  and  $2.10 \pm 0.20 \mu\text{g}/\text{cm}^2$  for bulk

Analyte (bulk concentration, $\mu\text{g/ml}$ )	surface density ( $\text{ng/cm}^2$ )	$d$ (nm) SAW/SPR	$x$ (%) SAW/SPR	$\Delta f_n/\sqrt{n}$ (Hz) QCM	$\Delta f_n/n$ (Hz) QCM	$\Delta D$ ( $\times 10^{-6}$ ) QCM
<i>Cu</i>		2 – 12	?	?-1000	NO	50
S-layer	560 $\pm$ 20	4.7 $\pm$ 0.7	75 $\pm$ 15	NO	45=900	3-5
CTAB	125 $\pm$ 15	1.0 $\pm$ 0.1	100	NO	8=160	0.2-0.5
collagen (30 $\mu\text{g/ml}$ )	1750 $\pm$ 150	16.0 $\pm$ 3.0	25 $\pm$ 15	1000	NO	100
collagen (300 $\mu\text{g/ml}$ )	2100 $\pm$ 200	19.0 $\pm$ 3.0	35 $\pm$ 10	1200	NO	>120
fibrinogen (46 $\mu\text{g/ml}$ )	750 $\pm$ 100	6.0 $\pm$ 1.5	50 $\pm$ 10	110 $\pm$ 5	55 $\pm$ 5 $\simeq$ 1110	4-10
fibrinogen (460 $\mu\text{g/ml}$ )	1500 $\pm$ 500	13.0 $\pm$ 2.0	50 $\pm$ 10	NO	100=1700	8-10

Table 1: Summary of the results extracted from simultaneous SAW and SPR measurements, and comparison with the results obtained from QCM-D measurements. The “surface density” value is obtained by converting the phase shift observed on the SAW device monitored in an open loop configuration to frequency through the linear relationship monitored on the Bode plot, and the resulting frequency shift to a mass density per unit area by using the mass sensitivity deduced from the copper calibration. The layer thickness  $d$  and protein content of the layer  $x$  are deduced from the simulation of the SPR shift as a function of layer thickness and optical index (assuming a protein layer optical index of 1.45 and a protein layer density of 1.4  $\text{g/cm}^3$ ) and correspond to the pair of parameters matching both the SPR and SAW data. The last three columns are related to QCM-D measurements and illustrate the fact that the higher the water content in the layer under investigation, the higher the dissipation ( $\Delta D$ ) and the more appropriate the hydrodynamic model of the wave interacting with the viscous solvent (with a  $1/\sqrt{n}$  normalization factor) over the rigid mass model (with a  $1/n$  normalization factor). The equality sign in the 6th column (in which the rigid mass assumption is made and in which the Sauerbrey relationship is applied) relates the normalized frequency shift to a surface density in  $\text{ng/cm}^2$  using the proportionality factor 20.1  $\text{ng/Hz}$  for the 4.7 MHz resonance frequency resonator.

concentrations of collagen of 30 and 300  $\mu\text{g/ml}$  respectively. The SPR angle shift data are modeled following the formalism developed in [59] in which each component of the electrical field is propagated through a stack a planar dielectric interfaces. The optical indices of the metallic layers were taken from the literature [62] considering the 670 nm wavelength: 10 nm titanium with  $n_{Ti} = 2.76 + i3.84$  and 45 nm gold layer with  $n_{Au} = 0.14 + i3.697$ , while the optical indexes of the underlying dielectric substrate were taken as  $n_{quartz} = 1.518$  coated with 1200 $\pm$ 100 nm silicon dioxide  $n_{SiO_2} = 1.45$ . While only the last dielectric layer ( $SiO_2$ ) below the metallic layer is necessary to estimate the position of the plasmon peak, we include the full stack of planar layers in our simulation in order to include possible interference effects. The optical index of the protein  $n_{protein}$  is assumed to be in the 1.45 to 1.465 range, as is the case for most polymers [63, 64, 9]. The properties of the protein layer, supposed to be homogeneous, are deduced from the assumption that a weighted average of its components (water and protein) can be used: if the ratio of protein in the layer is  $x$ , then the optical index of the layer is assumed to be  $n_{layer} = x \cdot n_{protein} + (1 - x) \cdot n_{water}$  [65] ( $n_{water} = 1.33$ ) and its density  $\rho_{layer} = x \cdot \rho_{protein} + (1 - x) \cdot \rho_{water}$  ( $\rho_{water} = 1 \text{ g/cm}^3$  and  $\rho_{protein}$  is assumed to be equal to 1.4  $\text{g/cm}^3$  range [66, 11, 63, 64]). The latter value is used in our simulations. The methodology for extracting the physical parameters of the

protein layers is the following: we first simulate the predicted SPR dip angle shift as a function of layer protein content  $x$  and layer thickness  $d$ , as shown in Fig. 7 where we display the SPR angle shift due to the added dielectric layer formed by the proteins (*i.e.* dip angle with solvent before adsorption subtracted from the dip angle after adsorption).

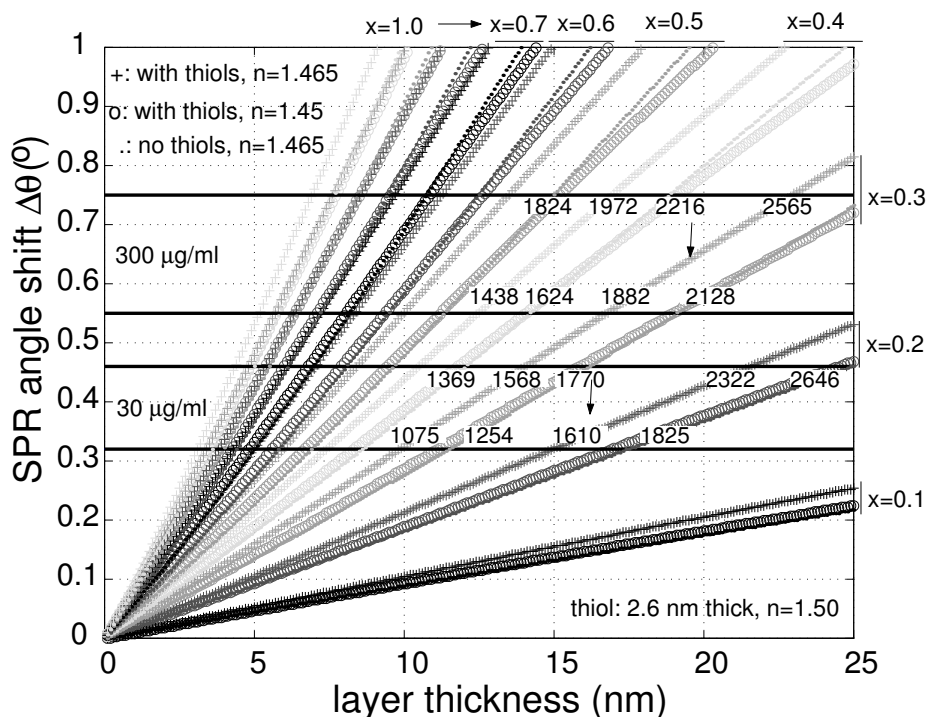


Figure 7: Simulation of the angle shift (ordinate) as a function of layer thickness (abscissa) and protein content ratio  $x$  (right and top margin) for various layers, including or not including the thiol layer and various protein layer optical index (1.45 or 1.465). The mass density in  $\text{ng/cm}^2$  are indicated within the graph for the points compatible with the observed SPR angle shift ( $390 \pm 70 \text{ m}^\circ$  for 30  $\mu\text{g/ml}$  bulk collagen concentration and  $650 \pm 100 \text{ m}^\circ$  for 300  $\mu\text{g/ml}$  bulk collagen concentration): the only point compatible with the  $1750 \pm 150 \text{ ng/cm}^2$  ( $2100 \pm 200$  respectively) observed by the SAW device results in a layer thickness of  $16 \pm 3 \text{ nm}$  ( $19 \pm 3 \text{ nm}$  respectively) and a protein content ratio of  $25 \pm 15\%$  ( $35 \pm 10\%$  respectively). Optics simulations were performed either assuming a 2.6 nm thick thiol layer [60] (refractive index: 1.50) on the  $\text{Ti/Au}$  layer followed by a variable thickness of collagen (mixture of protein with optical index 1.465 or 1.45 and water with optical index 1.33; crosses and circles), or assuming that the thiol layer leads to a negligible effect and not including it in the simulation, with a protein optical index of 1.465 (dots). The resulting mass density ranges (in  $\text{ng/cm}^2$ ) are calculated for the intersection point of each of these curves with the observed angle shift for each possible protein to water content ratio: all values indicated on the figure are for solvent swollen layers, including the mass of the trapped solvent.

We mark on such a plot the experimentally observed angle shift, which leads to a set of possible  $\{x, d\}$  couples compatible with the SPR experiment. For each of these set we compute the surface density of the layer  $d \times \rho_{\text{layer}}$  and



395 compare it with the value  $\Delta m/A = \Delta f/(S \times f_0)$  experimentally observed with the SAW measurement. A single set  $\{x, d\}$  is compatible with both the SAW and SPR data. Notice that the resulting mass density  $d \times \rho_{layer}$  includes the mass of trapped solvent in the layer.

The results of both SPR and SAW signals can only be compatible with  
400 a water content of the collagen layers in the range  $75\% \pm 15\%$  for  $30 \mu\text{g/ml}$  concentration ( $x=0.25 \pm 0.15$ ) and  $65\% \pm 10\%$  for  $300 \mu\text{g/ml}$  ( $x=0.35 \pm 0.1$ ), with a lower water content for higher bulk collagen concentrations, and correspond to the only set of parameters compatible with the SPR angle shift and the mass variation observed by the SAW device, assuming a purely rigid mass effect and  
405 negligible viscous interaction. The very high water content obtained here is confirmed by the large dissipation monitored on the QCM-D.

As was shown earlier in [54] and by others [31], a large dissipation shift indicates strong hydrodynamic interaction of the vibrating QCM surface with the surrounding solvent, and is confirmed by the overtone scaling law  $\Delta f_n/\sqrt{n} = \text{constant}$   
410 (as opposed to the expected  $\Delta f_n/n = \text{constant}$  for a rigid layer). One also sees here the strong overestimate of the bound protein mass if assuming a rigid mass and applying the Sauerbrey proportionality relationship between mass and frequency shift. The estimated collagen film thickness in the 15 to 20 nm range (Fig. 7) is in agreement with AFM topography maps obtained ex-situ under  
415 similar conditions [43].

Table 1 summarizes our measurement results on collagen and fibrinogen layers following the data processing methodology described in the previous paragraph. We observe that the parameters extracted from the SAW/SPR simultaneous measurements are in good qualitative agreement with the QCM-D results:  
420 a layer leading to a high dissipation increase ( $\Delta D > 10 \times 10^{-6}$ ) and an overtone normalization law with the square root of the overtone number is characterized by a high water content, as seen with collagen. On the other hand a small dissipation increase and a normalization law of the QCM frequencies with the overtone number are indicative of a low water content and a layer behaving as a rigid mass bound to the surface, as observed with CTAB and the S-layer.  
425 Fibrinogen is an intermediate case, for which the QCM frequency does not scale well with the overtone number nor with the square root of the overtone number, and for which the dissipation increase is average. We indeed find a rather low water content for such layers. The uncertainty on the collagen layer density and hence thickness is large: as opposed to highly ordered layers such as those  
430 formed by self-assembled monolayers of thiols or by CTAB, we do not expect highly disorganized polymer-like films of fibrous proteins to form exactly similar structures from one experiment to another. The physical property (water content and hence density and optical index) results on the other hand are consistent from one experiment to another, hence the need for the simultaneous  
435 measurements at the same location by both optical and acoustic methods (and eventually additional methods such as scanning probe microscopy [49]) in order to obtain statistically significant properties of the film.

#### 4.2. Kinetics analysis

440 We attempt now to provide some hint at differences in the kinetics as observed by acoustic and optical methods. We compare the kinetics as monitored by SAW and SPR by normalizing the response of the sensor once the saturation level is reached, just after the rinsing buffer step. We thus plot in Figs. 8 (a) and (b) the curves

$$\frac{S(t) - S(t_0)}{S(t_f) - S(t_0)} \quad (1)$$

445 where  $t_0$  is the adsorption starting time,  $t_f$  the time at which a saturation signal has been reached and the protein solution is replaced by buffer, while  $S(t)$  is a signal which can either be in our case the SAW phase shift  $\Delta\phi$  or the SPR angle shift  $\Delta\theta$ . We now first analyze the expected behavior of the normalized quantities of the two signals when assuming a rigid mass interaction and the model presented previously here, and will then discuss some of the possible causes of deviation from this expected behavior.

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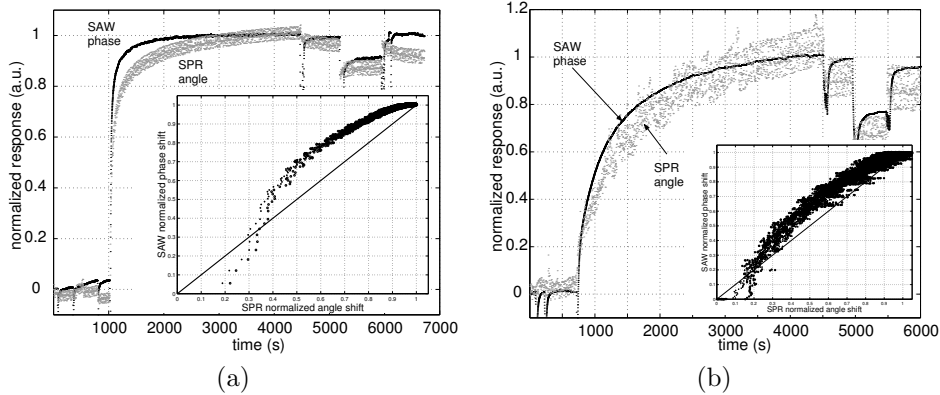


Figure 8: Comparison of the kinetics of collagen adsorption as monitored by an acoustic (SAW) method and an optical (SPR) method, for bulk concentrations of (a) 30 µg/ml and (b) 300 µg/ml. Notice that the *same* hydrophobic-thiols coated gold area of monitored by both techniques. The kinetics as observed by acoustic methods appears faster than that observed by optical methods: as explained in the text, the mass of solvent swollen layer is overestimated by acoustic methods and underestimated by optical methods, leading to differences in the observed kinetics during layer formation. Inset: normalized SAW response as a function of the normalized SPR response. A rigid interaction in which both signal are proportional to the adsorbed protein quantity would lead to all points lying on the line of slope 1 (see text).

If we first assume that the SAW signal shift is proportional to the bound mass – including the trapped solvent – and that the SPR signal is proportional to the added protein quantity, then  $\Delta\phi \propto d \times \rho(x)$  and  $\Delta\theta \propto d \times n(x)$  where  $d$  is the common layer thickness measured by both techniques. By introducing these proportionality relationships in Eq. 1, we obtain normalized quantities expressed as  $\frac{\rho(x) - \rho_0}{\rho_f - \rho_0}$  for the SAW phase and  $\frac{n(x) - n_0}{n_f - n_0}$  for the SPR angle, where

455

an  $f$  index indicates the value of the quantity at the date at which saturation is reached and index 0 indicated the beginning of the adsorption.

460 If we furthermore assume, as has been done previously in the quantitative analysis of the data, that  $\rho_{layer} = x \cdot \rho_{protein} + (1 - x) \cdot \rho_{water}$  and  $n_{layer} = x \cdot n_{protein} + (1 - x) \cdot n_{water}$ , and considering additionally that  $\rho_0 = \rho_{water}$  and  $n_0 = n_{water}$ , we finally find that both normalized quantities express as  $\frac{x \cdot (\rho_{protein} - \rho_{water})}{\rho_f - \rho_{water}}$  and  $\frac{x \cdot (n_{protein} - n_{water})}{n_f - n_{water}}$ . Since both techniques, SAW and  
 465 SPR, are probing the same surface, not only do they measure a common layer thickness, but also a common protein to water ratio, so that a common final value  $x_f$  can be attributed to both  $n_f$  and  $\rho_f$ , and finally the two expressions simplify and give  $\frac{x \cdot (\rho_{protein} - \rho_{water})}{x_f \cdot (\rho_{protein} - \rho_{water})} = \frac{x}{x_f}$  for the normalized SAW data and  $\frac{x \cdot (n_{protein} - n_{water})}{x_f \cdot (n_{protein} - n_{water})} = \frac{x}{x_f}$ .

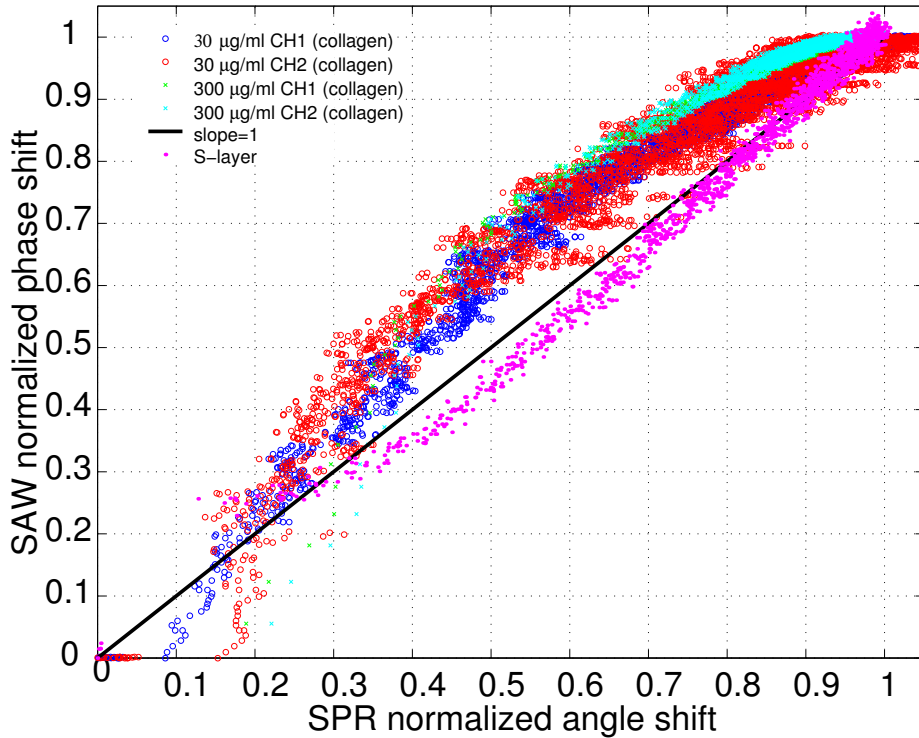


Figure 9: Normalized signal from acoustic (SAW) and optical (SPR) measurements: if both techniques were measuring the same adsorbed mass property, the data would be lying on the  $y = x$  line, as seen for the rigid S-layer. For collagen and fibrinogen, all datasets lie above  $y = x$ .

470 In conclusion of this calculation, we see that following two assumptions about the proportionality of the SAW and SPR signals with the physical properties of the layer and the evolution of the physical property of the protein layer as a function of water content, we reach the same law for the evolution of the

normalized SAW and SPR signals. We test this result by eliminating the time  
475 parameter and plotting the SAW normalized phase shift as a function of SPR  
normalized angle shift. We predict that all points should lie on the line of slope  
1. The S-layer data shown previously [52] do not show any significant difference  
in the kinetics as detected by the optical and acoustic methods, and hence  
indeed all normalized points fall close to this line (Fig. 9). On the other hand  
480 the solvent swollen fibrinogen and collagen adsorbed layers presented here seem  
to display a faster kinetics as detected by the acoustic method than the one  
detected by the optical method. Therefore we see in inset of Fig. 8 (a) and (b)  
that all points lie above the line of slope 1. Such a graph provides a quantitative  
relationship between measurements obtained by acoustic and optical methods.

485 From the calculation we just presented, we can attribute the discrepancy  
of the normalized point distribution to either of the two assumptions: either  
the SAW signal is not strictly proportional to the bound mass (assumption  
 $\Delta\phi \propto d \times \rho_{layer}$ ) or the simple linear law relating the physical properties of  
the layer (density and optical index) to the physical properties of the individual  
490 components of the layer – protein and water – is not accurate. In view of the  
previously published literature [11, 53], we favor the first possibility and propose  
a possible contribution of the hydrodynamic interaction of the collagen layer to  
the SAW signal. The acoustic signal overestimates the bound mass by being  
affected by the bound solvent as well, while the optical method under-estimates  
495 the bound mass due to the lowered optical index of the adsorbed layer associated  
with the bound solvent.

Throughout this analysis, neither the viscoelasticity of the adsorbed layer  
or of the surrounding solvent, nor the experimentally measured acoustic losses,  
have been considered. The shortcoming of these simplifications might be solved  
500 by adding a set of charts relating the frequency shift with layer thickness and  
viscosity, and most significantly insertion loss with these parameters. Such an  
investigation was endeavoured in [39, 67], in the former reference for solvent  
only (no adsorbed layer) and in the latter for a single layer in air, since the  
coupled phase/magnitude shift induced by both mass loading and viscoelastic  
505 coupling makes the separation of each contribution complex when considering  
finite thickness layers coated by a viscous solvent. The insertion loss evolution  
observed between the beginning and end of each experiment has been indicated  
in the caption of each experimental SAW chart result for the reader to assess  
the validity of this assumption: while a minute insertion loss change in the case  
510 of fibrinogen (0.5 dB) hints at the validity of our assumptions, the large (3.3–  
6.5 dB) insertion loss observed during collagen adsorption hints at the need for  
a more complex analysis to grasp all the subtleties of the adsorption process.

## 5. Conclusion

We have shown how a two steps measurement, first using copper electrode-  
515 position for instrument calibration followed by a measurement on the actual  
biological layer under investigation, on a combined SAW/SPR instrument leads  
to an estimate of the water content and layer thickness. While each individual

technique cannot achieve such identification, both common parameters (water content ratio and layer thickness) can be identified with the combination. Such results are especially useful for protein layers with high water content for which the hydrodynamic interaction can become predominant over rigid adsorbed mass. We have verified the calibration process using CTAB, confirming the 120 ng/cm<sup>2</sup> surface density due solely to the densely organized monolayer, and illustrated the technique with an estimate of the water content of collagen, leading to a 70%-water/30%-protein result, which is in agreement with the large dissipation increase (quality factor decrease) observed by QCM-D. Furthermore, QCM-D overtone normalization factor with such solvent swollen layers is the inverse of the square root of the overtone number (and not the inverse of the overtone number as would be the case for a rigid layer). Applying the proportionality factor between QCM frequency shift and surface mass density as predicted by the Sauerbrey relationship, assuming a rigidly bound mass, leads to a strong overestimate of the adsorbed mass. We have also shown that fibrinogen layers have a water content of 50±10 %, compatible with a lower dissipation factor increase in the QCM-D measurements. Finally, we have discussed the comparison of kinetics as observed by optical and acoustic techniques and propose that the discrepancies observed in the case of solvent swollen layers might be attributed to minor hydrodynamic interactions of the SAW with the protein layer. Introducing in this analysis the SAW insertion losses would allow to resolve one more unknown, namely the adsorbed layer dynamic viscosity.

## 6. Acknowledgments

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