

Growth of textured aluminum films on LiNbO_3 piezoelectric substrate with ultrathin tantalum underlayer.

Hala Achahbar
frec|n|sys
Besançon, France
hala.achahbar@femto-st.fr

Florent Bernard
frec|n|sys
Besançon, France
florent.bernard@frecnsys.fr

Emilie Courjon
frec|n|sys
Besançon, France
emilie.courjon@frecnsys.fr

Thomas Baron
FEMTO-ST
Besançon, France
thomas.baron@femto-st.fr

Sylvain Balandras
frec|n|sys
Besançon, France
Sylvain.ballandras@frecnsys.fr

Abstract: In this paper the approach of improving aging of (AlCu2%) electrode of Surface acoustic Wave filters is presented. The goal of this study is to contribute of the improving of aging due to electromigration effect. This effect occur easily in high-frequency Surface Acoustic Wave (SAW) devices. For that purpose, the impact of a tantalum (Ta) thickness deposited between the electrodes (AlCu2%) and a piezoelectric LiNbO_3 is done. A heating post-process is also presented to increase the aging of such devices.

Keywords: Piezoelectric, AlCu2% (111) texture, Ultrathin underlayer, Electromigration, LiNbO_3 , SAW, Free surface energy, IDT,5G.

I. Introduction

In the context of 5G, Surface Acoustic Wave (SAW) filters have to increase their operating frequency. Thus, new technological challenges arise due to the reduction of the dimensions of the electrodes. One of them are the aging of electrodes which contribute to keeping filter characteristics. Most SAW filters are composed of AlCu2% electrodes deposited on a piezoelectric substrate such as Lithium Niobate (LiNbO_3) or Lithium Tantalate (LiTaO_3). Our work has to objective to keep AlCu2% electrode and improve the life time of such filters.

The life time of SAW-filters is limited by the degradation of the AlCu2% electrodes [1]. The degradation of AlCu2% electrodes are due to the migration of Al atoms along grain boundaries (GB). Which causes the formation of voids and hillock-like extrusion (see Figure 1). This phenomenon of migration is called electromigration (EM), which is the

atomic displacement due to momentum transfer to metal atoms [2].

Several studies have found a promising and feasible approach to improve electromigration resistance by imposing a better crystallographic texture of that AlCu2% film [4,5,6,7] It was well demonstrated the AlCu2% electrodes with a highly texture (111) are more resistant to electromigration than those with poor (111) texture [4,5,6,7]

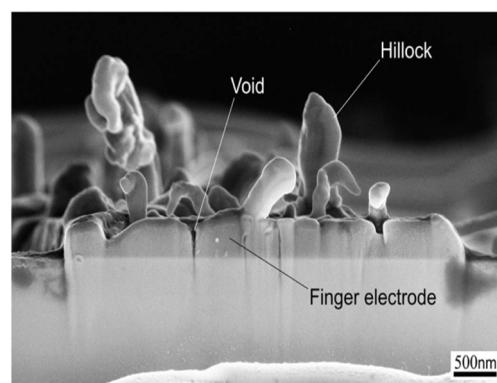


Figure 1: SEM micrograph of a FIB cross section of a damaged Al finger electrode on LiNbO_3 (90° tilted) with strong hillock formation (after 2000 minutes at 3W) [2]

Sulei Fu *et al.* report in a previous work [4] that the presence of ultrathin Ti underlayer between the substrate of LiNbO_3 and AlCu2% film can give a better textured AlCu2% film. It has also been reported by other authors that Ni or Zr as an underlayer provides an improvement in the (111) texture of the AlCu2% film [6][7]. However, Qi Li *et al.* [6] have demonstrated that the AlCu2% texture and structure quality decreases gradually as the underlayer thickness increases. Atsushi Kamijo and Tsutomu Mitsuzuka [5]

noted that a textured AlCu2% film can be obtained on a metal underlayer in a certain thickness range.

Therefore, to obtain fine-dimensional control in high-frequency SAW filters, one solution consists on improving the crystallographic texture and structure of the AlCu2% electrodes by using an ultrathin underlayer [4,5,6,7].

In this work, the presence of a tantalum (Ta) underlayer (with various thicknesses) on a 128-rotated Y-Cut LiNbO₃ substrate during AlCu2% film growth will be studied. Heat treatments of AlCu2% films to improve the crystallographic texture and structure of AlCu2% electrodes will also be investigated.

II. Growth modes

The mechanism of texturing can be explained by growing modes of the AlCu2% film on LiNbO₃ substrates. Theoretical models of thin films growth suggest that, one of the parameters that determine the growth model is the surface-interface energy balance between film and substrate (see Figure 2). allows to define the growth mode of the AlCu2% film as a Volmer-Weber or Frank-Van Der Merwe mode. This is represented by Young's equation (eq1) [8].

$$\cos(\theta) = \frac{(\gamma_s - \gamma_i)}{\gamma_f} \quad (eq1)$$

where θ , γ_s , γ_i and γ_f are respectively the wetting angle of the island, substrate surface energy, film surface free energy, and interfacial free energy between film and substrate.

When the condition (eq2) is satisfied during the film deposition, the film is considered to develop at the Volmer-Weber growth mode (3D). In that case, the film grows randomly in the initial stage, resulting in poor texture [8].

$$\gamma_f + \gamma_i - \gamma_s > 0 \quad (eq2)$$

In the Frank-Van Der Merwe growth mode, the condition changes to (eq3):

$$\gamma_f + \gamma_i - \gamma_s < 0 \quad (eq3)$$

This mode is generally obtained when the substrate surface energy γ_s is higher than γ_f . The film grows by means of successive monolayers (see Figure 2), which favors the formation of a textured film [8].

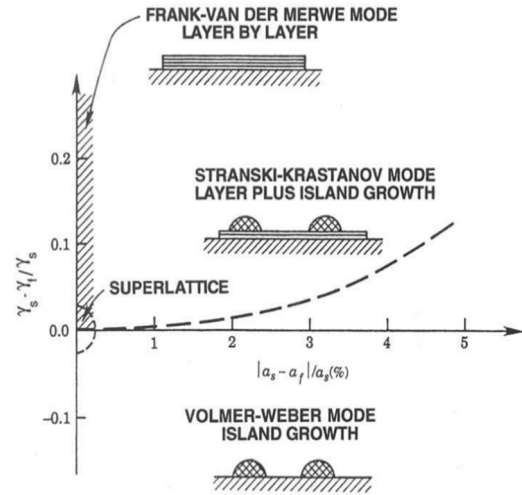


Figure2: Stability regions of the growth modes versus surface energy between substrate and film and of lattice misfit [9]

The work about surface energies of solids of Tu et al. [9] suggests that metals have higher surface energies than oxides, alkali halides, sulfides, and organic substances. The higher values correspond to the transition metals while the lower values is related to alkali and divalent metals.

Therefore, when AlCu2% film is deposited directly onto a LiNbO₃ substrate, the equation (2) is satisfied and the AlCu2% film grows randomly by the Volmer-Weber mode, which results in the formation of an AlCu2% polycrystalline film with poor texture [4,5,6,7].

The goal of this study is to increase the surface free energy (FSE) of the LiNbO₃ substrate by using an ultrathin underlayer (Ta) and then change the growth mode to improve the structure and the texture quality of AlCu2% electrodes

III. Experimentation

A. Film Deposition

A 100nm-thick AlCu2% film with several thicknesses of Ta underlayer (0, 1.3, 5 and 20 nm) has been deposited on 5 128°-rotated Y-Cut LiNbO₃ substrates (with a diameter of 4inches). Both films have been deposited by electron beam evaporation in a Balzers BAK760. Prior to layer deposition, substrates have been cleaned successively in Microposit Remover 1165 (50°C) and rinsed in deionized water for 10 min, then a short pre-clean with O₂ plasma was applied. Deposition of Ta underlayers was carried out with a rate of 0.3 nm.s⁻¹ at room temperature, after the chamber was evacuated down to 10⁻⁶ mbar by a combined vacuum system of mechanical pump and cryopump. Finally, without breaking vacuum, AlCu2% films were evaporated at a rate of 1 nm.s⁻¹ also. The thickness of both films was monitored by a quartz microbalance located inside the vacuum chamber. After deposition, a thermal treatment was carried out by heating the films (AlCu2%/Ta (1.3 nm)/LiNbO₃) in atmosphere at 1 °C/min to 523

and 623 K, holding at temperature for 3 hours before furnace cooling. Heat treatments have been performed in a AET tube furnace.

B. Characterizations

The crystalline structure of the films (100 nm-AlCu2%/LiNbO₃ and 100 nm-AlCu2%/1.3 nm-thick Ta/LiNbO₃) has been analyzed by diffractometer (XRD, SmartLab) in θ - 2θ scan and χ -scan (Cu(K α) wavelength, $\lambda = 0.154056$ nm)).

To determine the FSE of a LiNbO₃ substrate with (0, 1.3, 5, and 20 nm) of Ta underlayer, contact angles of test liquids, whose FSE (γ_l) including their dispersive γ_l^d and polar γ_l^p parts are known [13], are measured. Contact angles θ have been measured by static sessile drop method using a Digidrop – MCAT Goniometer (GBX). The device used for contact angle measurement includes a holder with microliter syringe. Drops are backlighted by LEDs. Evaluation of contact angles from the camera data has been performed on a Visiodrop software. Test liquids were chosen in this study are Formamide (99%), ethylene glycol (99.8%) glycerol (99%) deionized (DI) water, and 50% ethylene glycol +50% DI water (purchased from VWR-Chemicals). The selection of these liquids was based on the following criteria:

1. liquid should not react with substrate;
2. liquids should be non-toxic;
3. the liquid surface tension should be higher than the anticipated solid surface tension [10][11].

The dispersive and polar parts of liquids surface tension are used to calculate FSE of substrates (γ_s) based on a mathematical model. This model, known as Owens-Wendt model [12], considers the geometric mean of the dispersive and polar parts of the liquids surface tension and of the solids FSE (eq4) [12]:

$$\gamma_{sl} = \gamma_s + \gamma_l - 2\sqrt{\gamma_s^d \gamma_l^d} - 2\sqrt{\gamma_s^p \gamma_l^p} \quad (eq4)$$

Substituting this expression in the Young equation: $\gamma_s = \gamma_{sl} + \gamma_l \cos(\theta)$ a linear equation of the type $y = ax + b$ can be obtained [12]:

$$\frac{\gamma_l(1+\cos(\theta))}{2\sqrt{\gamma_l^d}} = \sqrt{\gamma_s^p} \sqrt{\frac{\gamma_l^p}{\gamma_l^d}} + \sqrt{\gamma_s^d} \quad (eq5)$$

These equations $y = \frac{\gamma_l(1+\cos(\theta))}{2\sqrt{\gamma_l^d}}$ and $x = \sqrt{\frac{\gamma_l^p}{\gamma_l^d}}$

contain the known quantities, namely the measured contact angle θ and the dispersive γ_l^d and polar γ_l^p parts of the test liquid's surface tension. The searched dispersive and polar parts of the solids FSE are contained in the axis intercept b and in the slope a , respectively. The regression leads directly to the

components of the solid: $\gamma_s^p = a^2$; $\gamma_s^d = b^2$

$$\gamma_s = \gamma_s^p + \gamma_s^d \quad (eq6)$$

IV. Results and discussion

A. Free surface energy

Firstly, we must note, that the results obtained in this study are qualitative. The goal is to follow the evolution of the FSE of LiNbO₃ as a function of Ta underlayer thickness (1.3, 5, 20 nm).

The abscissa ($y = \frac{\gamma_l(1+\cos(\theta))}{2\sqrt{\gamma_l^d}}$) and ordinate $x =$

$\sqrt{\gamma_l^p/\gamma_l^d}$ pairs are calculated for each measurement.

Table 1 represents the FSE values obtained by the Owens-Wendt method for LiNbO₃ wafers and for 5 nm-thick, 20 nm thick and 1.3 nm-thick Ta films deposited on LiNbO₃ wafers.

Table1 Calculated FSE values using Owens-Wendt method for substrates (all in mJ.m⁻²)

Substrates	LiNbO3	5nm-thick Ta / LiNbO3	20nm-thick Ta / LiNbO3	1.3nm-thick Ta / LiNbO3
$\gamma_l^d = b^2$	17,64	20,95	22,75	21,40
$\gamma_l^p = a^2$	29,45	26,83	23,67	28,69
γ_s	47,09	47,79	46,43	50,10
FSE mJ/m ²	47,09 ± 1,07	47,79 ± 0,78	46,43 ± 0,99	50,10 ± 1,34

The value of the substrate FSE (γ_s) calculated by the Owens method increases in the presence of 1.3nm of Ta, γ_s is equal to 50.10 ± 1.34 mJ/m². Moreover, the FSE value decreases from 47.79 ± 0.78 mJ/m² to 46.43 ± 0.99 mJ/m² when the thickness changes from 5 nm to 20 nm of Ta (see Figure 2).

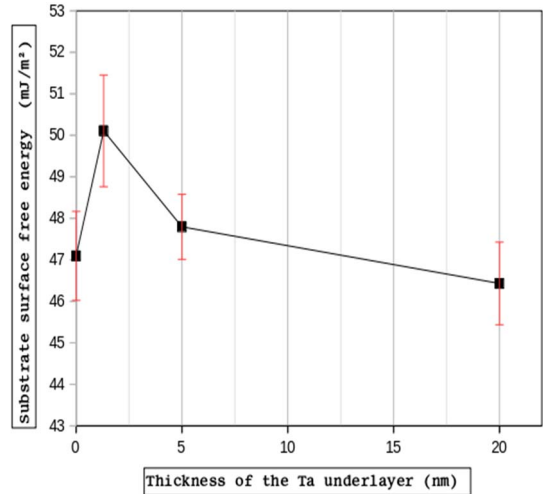


Figure 3: Evolution of the free FSE of LiNbO₃ as a function of the thickness of Ta.

These results confirm the advantage of using an

ultrathin underlayer of Ta (<5 nm) to increase the FSE of the LiNbO₃ substrate. This high surface free energy comes from the fine grains of Ta dispersed on the LiNbO₃ surface. It is assumed that the 1.3 nm-thick Ta underlayer is the best candidate that will allow the γ_5 to increase and therefore promote a switch from Volmer-Weber mode (eq2) to the Frank-Van Der Merwe mode (eq3). Then will allow the AlCu2% film to grow layer by layer with fewer grain boundaries and a single preferred orientation.

B. Crystal structures quality

In order to characterize the AlCu2% (111) texture X-Ray Diffraction was employed. XRD are carried out on the LiNbO₃ bare surface and LiNbO₃ with 100 nm-thick AlCu2% film (see Figure. 4).

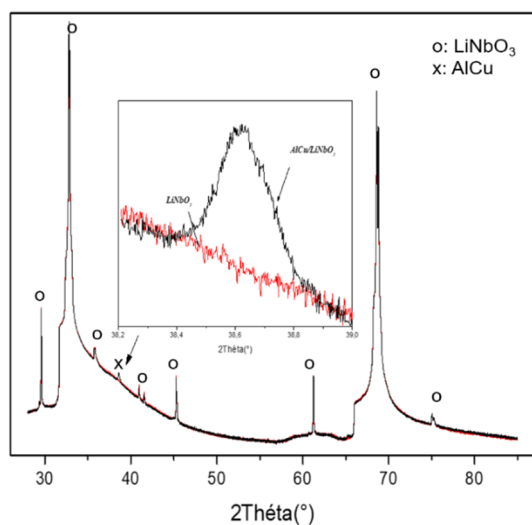


Figure 4: XRD patterns of θ - 2θ scans of AlCu2% electrodes

We can clearly see that only one Bragg peak appears at 2θ of 38° (Figure 4), which corresponds to the Al (111), in the range of 30°–80°. The apparent presence of only Al (111) without other peaks demonstrates that (111) preferred AlCu2% thin films are developed on 128°-rotated-Cut- LiNbO₃.

When inserting an ultrathin Ta underlayer (1.3 nm) between the LiNbO₃ substrate and the AlCu2% film the AlCu2% (111) peak remains the same (see Figure 5).

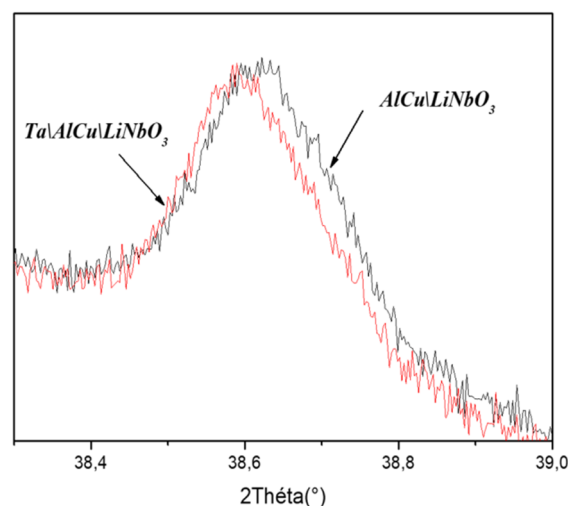


Figure 5: Evolution of the peak AlCu2% (111) in the presence of the Ta underlayer.

The microstructure of AlCu2% thin films grown on Ta (1.3 nm)/LiNbO₃ is stabilized by an annealing step in atmosphere at (523 and 623 K) (see Figure 6).

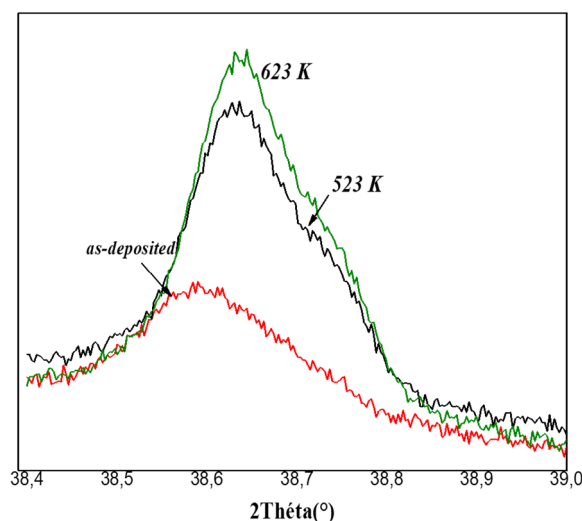


Figure 6: Evolution of the peak (111) as a function of the annealing temperature for the 100 nm AlCu2% film deposited on a 1.3 nm underlayer of Ta

On figure 7, we can see that the full width at half maximum (FWHM) value decreases after heat treatment.

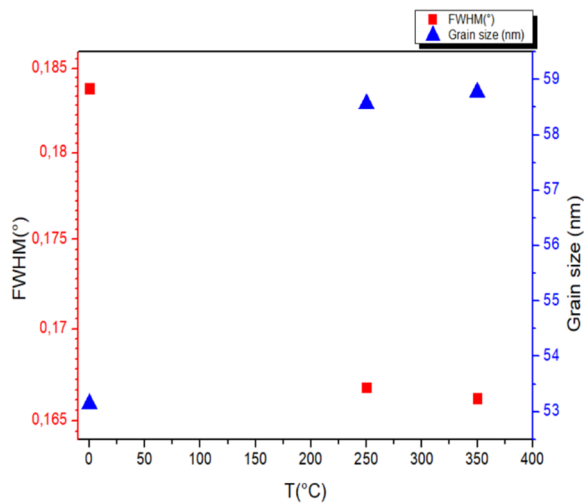


Figure 7: Evolution of the FWHM and grain size of AlCu2% films as a function of the annealing temperatures

The grain size value is 53 nm for samples as-deposited but raises to 58 nm and to 58 nm when the annealing temperature increases to 523 K and 623 K.

At this stage of the study, an improvement in the structure and crystalline quality of the AlCu2% films with 1.3 nm-thick Ta underlayer and annealing was observed. Other XRD analysis of AlCu2% films with Ta underlayer (5 nm and 20 nm) are in progress. Further studies of stress in AlCu2% films without Ta underlayer and with a Ta underlayer lower than 10 nm are ongoing in order to determine the effect of the Ta underlayer in lattice mismatch and strain between the AlCu2% film and the LiNbO₃ substrate and therefore confirm if the Ta ultrathin layer can really allow AlCu films to grow in Frank-van der Merwe mode.

v. Conclusion

A series of AlCu2% films with different Ta underlayer thicknesses has been deposited on LiNbO₃ wafers by electron beam evaporation. Contact angle measurement show that the presence of 1.3 nm-thick Ta underlayer onto LiNbO₃ surface can greatly increase the surface free energy of the LiNbO₃ substrate. The 1.3nm-Ta/AlCu2%/LiNbO₃ seems to be the best configuration to privilege the Frank-van der Merwe mode.

The XRD studies showed that 1.3-nm Ta underlayer and a heat treatment (523-623 K) improves the texture and crystalline quality of AlCu2%. Hence, reduce the diffusion of Al atoms into GB, and subsequently improve the resistant to electromigration phenomenon.

Abbreviations and Acronyms

SAW: Surface Acoustic Wave
EM: Electromigration
IDT: Interdigital transducer

FSE: Free surface energy
FWHM: Full width at half maximum
XRD: X-ray diffraction
AlCu2%: Alloy aluminum copper 2%.

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