

Stand-Alone Renewable Power System Scheduling for a Green Data-Center using Integer Linear Programming

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Abstract Taking into account the spread of data centers around the world and their huge energy consumption, several researchers focused on task scheduling and resource allocation problem in order to minimize the energy consumed by the data center. Other initiatives focus on the implementation of green energy sources in order to minimize the consumption of fossil fuels and their emission of CO₂. As part of the ANR DATAZERO project [34], several research teams aim at defining main concepts of a full green data center, only powered by renewable energies. To achieve this goal, it is mandatory to focus on the efficient management of an autonomous hybrid power system consisting of solar panels, wind turbines, batteries and fuel cell systems. The purpose of this work is not to show that a stand alone data center is economically viable but rather feasible. This paper proposes a set of models based on mixed integer linear programs able to manage the energy commitment to address the data center power demand. The approach takes the season and weather forecasts into account at the time of optimization.

Keywords Renewable energy, wind turbine, photovoltaic panel, hybrid energy storage, data center, integer linear program, optimization.

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1 Introduction

The enormous growth of the Internet and the increase in the number of online services accessible to public have highlighted the cost imposed by the cloud in general and by data centers in particular in terms of energy consumption over the past few years. Nowadays, a typical data center includes hundreds of thousands of servers, cooling equipment, and substation transformers which contribute greatly in global warming as they deliver a huge quantity of CO₂.

In this context, many green initiatives are being taken to make the use of data centers more virtuous in terms of their ecological footprint. One of these initiatives is the use of renewable energy sources (RES) in data center power system and even making sure that energy production is directly integrated into their own facilities. Thus, McGraw-Hill company completed a 14.1 MW solar panel installation to power its data center located in East Windsor, New Jersey [31]. Similarly, Apple has built a 40 MW solar field for its North Carolina data center [2]. Nevertheless, the intermittent nature of renewable energy sources (sun and wind) is driving these data centers to resell surplus energy and use conventional sources to provide continuous service. This economically viable energy policy is not entirely satisfying in terms of carbon footprint.

For this reason, the ANR DATAZERO project [34] adopts an original approach which consists in computing data center's resources provisioned with 100% renewable energy. The purpose of this project is to study the feasibility of a stand alone data center while limiting its carbon footprint. Designing and operating such a data center is however not trivial. There is a need to optimize the IT load to the energy availability, and

conversely, to optimize the energy production to the incoming IT load. The sizing of the system in terms of IT and electrical components is also a huge challenge [17]. Thus, the ANR DATAZERO project is divided into two main decision modules: an IT decision module (ITDM) responsible for the management of the IT part (scheduling tasks, virtualization of servers, etc.) and a power decision module (PDM) responsible for the management of the renewable sources (source commitment, energy storage, etc.). The ambition of the project is to converge user needs with renewable energy production through a negotiation loop (NM) [7] as illustrated in Figure 1. Indeed, at each negotiation step, one asks to receive one or several energy profiles that can be delivered by the electrical part of the data center and able to be consumed by the IT part to satisfy a given level of computation for final clients. The negotiation continues bargaining with the two modules till achieving the convergence between the IT and electrical power profiles [38]. So, depending on the circumstances and on the period of the year, the level of energy available for the calculations may vary. The principle is that the sizing of both the IT and the electrical parts must allow a computation service in accordance with the quality of service announced in full autonomy thanks to short and long-term storage devices. These storage devices help smoothing the energy production available to supply the data center so that it can provide online services all day and all year long. However, the energy demand is not constant over time because client demand varies. So managing the use of storage in an appropriate way, with a view of satisfying a given computing demand, taking the intermittency of electrical power provided by the primary sources into account, is a major challenge. As suggested in [19], short-term and long-term storage are respectively done by using batteries and through the production of hydrogen with electrolyzers and the reverse generation of electricity is done with fuel cells.

Thus, this article presents, as part of the ANR DATAZERO project, an optimal management of a hybrid renewable energy system (HRES) consisting of solar panels, wind turbines, batteries and fuel cell systems with electrolyzers to supply a data center without exchange with the external electricity network. Depending on the quantity of renewable energy produced and the IT power demand over time, the storage sources must be managed. For instance, if the renewable production exceeds the data center’s demand, the energy difference should be stored. Conversely, in case the client demand is higher than the renewable production, the storage devices should provide the energy difference.

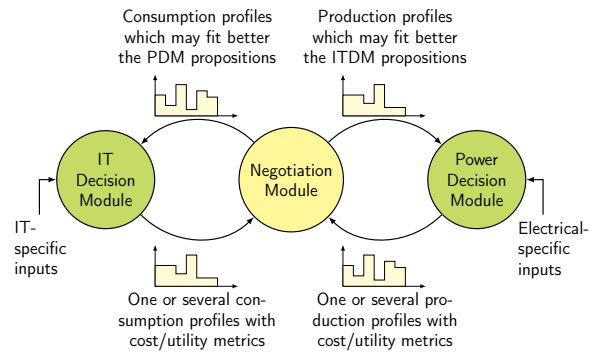


Figure 1 Illustration of the negotiation process, with the information exchanged between the decision modules and the negotiation module.

Then, according to the negotiation phase, we propose several optimization problem consisting of three main objectives: (i) proposing which power profile (constant or not), on a given period of time, the electrical part is able to produce in order to supply the IT part; (ii) proposing alternative power profiles based on a power profile given as an input by the negotiation module and (iii) proposing electrical power commitment in a given time window if we know the expected power demand of the data center that has to be satisfied. Only the power source commitment (iii) is an input of the power system [34]. The other optimization results computed by (i) and (ii) are sent to the negotiation process to help the negotiation process to converge. Once the convergence is obtained, the chosen power profile is delivered to the power decision module to compute the step (iii) as mentioned before. The optimization is based on the optimal solution of the addressed problem by Mixed Integer Linear Programming (MILP) as presented in the following.

This paper is organized as follows: Section 2 is dedicated to related works. In Section 3 we are proposing electrical component models on which constraints of the electrical part are based. Section 4 is focusing on the addressed problem within this paper. Section 5 describes the linearization of the previous non-linear models. Additional constraints and three objective functions are also given in this section to define three MILPs, each of them corresponding to one problem (i), (ii) and (iii) described above. Section 6 shows the usage of the Power Decision Module (PDM) that optimally solves addressed optimization problems. As a result of our approach, traces of executions are given to illustrate the PDM use in a time window of 72 hours.

2 Related work

Taking into account climate change, oil depletion, increasing population and increasing energy demand, energy saving has become a major concern for the world in general and in the computing domain in particular. A large variety of research are working on reducing CO₂ emissions and optimizing energy consumption. For instance, Oró *et al.* and Kaur *et al.* presented these surveys [24, 33] where they summarize all the technologies and tools that can be used in data centers to decrease their energy consumption.

Among many alternative energy sources, using green energy to power data centers can be considered as an attractive solution to succeed in energy saving and reducing gaz emissions. For example, Microsoft's data center in Quincy, WA consumes 48 MW of electricity, enough to power 40,000 homes [23]. In Thibodaux, a city in Louisiana state planned a wind power data center project in urban area [39].

Following Greenpeace report [6] of 2017, the consumption of data centers reached 7% of the world's energy consumption, of which the half was dedicated to cooling [26]. Moreover, the AMD report [29] estimated that the electricity consumption of all data centers in the world costs 7.2 billion per year. Unfortunately, this consumption has a negative impact on the environment as the majority of electricity is produced from fossil resources.

To further reduce the part of fossil fuels, many researchers are interested either in managing the energy resources to meet the user demand (Section 2.1), or in optimizing the use of the computing and the network resources to reduce overall energy consumption (Section 2.2).

2.1 Managing energy sources in data centers.

Uddin *et al.* [40, 41] have proposed papers and surveys that address energy efficiency and CO₂ mitigation strategies and techniques in data centers to reduce the effect of global warming. A wide variety of research tackles the use of batteries in data centers [13, 14, 25, 42, 44]. These studies show that the use of the storage can lower both of the capital cost of the power delivery infrastructure and the operating cost of a data center. In addition, in almost all these papers, authors consider a workload with available grid power. Nevertheless, none of these works have taken into consideration the use of renewable energy sources. Then, many papers consider the coordination among multiple power

sources in data centers. For instance, Arlit *et al* [3] have introduced a management architecture that optimizes the combination of power grid usage and renewable energy sources (RES) from an economic point of view by balancing the demand for computing and resource availability with supply side constraints. In [8], Deng *et al.* have proposed online control policies that uses different characteristics of multiple power sources in order to minimize operation cost. These researchers have used Lyapunov optimization and made a control algorithm which does not depend of statistics of system dynamics. Results show that it provides the trade-off capability between the operational cost, the data center availability, and the uninterruptible power supply lifetime. The algorithm also achieves the robustness to time-varying power demand and supply. Another paper has considered the coordination among multiple power sources in green data centers [28]. In this paper, Li *et al.* have considered that data centers have base-load power supply, intermittent power supply, and backup energy storage. The authors argue that existing studies typically assume certain specific types of renewable energy sources, and overlook the benefits of cross-source coordination. Then, the authors have proposed a hierarchical power coordination scheme, taking into consideration the timing and capacity of different renewable energy sources. With this scheme, the data centers can make multi-objective power management decisions, based on the available base-load power output, renewable power variability, battery capacity, and IT jobs. Similarly, in [36] the source scheduling is based on a priority scheme in order to maximize the use of renewable energy. Thus the power consumption from the grid is minimized. A dynamic power technique is used to cap the energy used from the grid. In [12], Goiri *et al.* have developed a prototype of an ecological data center connected to the grid in a small container including a set of solar panels, an electric battery and inverters. In their management algorithm, the authors have taken into consideration the electricity consumption and its cost. The results show that this algorithm can produce integrated workload and energy source schedules for a low electricity costs.

2.2 Managing workloads in data centers

Work has also been done to optimize IT resources by two ways. The first concerns the possibility to address the problem of scheduling computation tasks under energetic constraints [22, 27], problems of allocation and resource management with server shutdown, migration of virtual machines, network traffic management [5, 11,

32, 37]. The other direction consists in imagining energy aware IT architectures [16, 21].

An early work on green energy utilization in data centers by Aksanli et al. [1] shows the importance of power prediction. The authors designed an adaptive data center job scheduler capable of reducing the number of aborted jobs and improving the green energy utilization. In [10, 11], the authors propose GreenSlot which is a batch scheduler for parallel tasks. The aim is to reduce the brown power consumption of a data center partially powered by solar panels. In GreenSlot, computation jobs have deadlines and the scheduler first reserves resources for these jobs with lower slack (distance from latest possible start time to current time). Based on weather forecasting and power prediction, GreenSlot schedules the tasks on time slots. However the authors do not try to optimize their schedules. They just reduce the consumption and costs while meeting as much deadlines as possible. Similarly [30] presents a holistic approach to optimize the energy cost with incomes from running a batch of jobs and outcomes to buy brown energy. The paper also provides a proposition for net zero scheduling batch of jobs. It is however based on virtualization and is not bounded by the number of resources.

None of the aforementioned work deals with computing resources provisioned with 100% renewable energy that we consider in this paper. The ANR DATAZERO project aims at conceiving an innovative structure of a data center. The DATAZERO IT modules are explained in papers [5, 37]. In the following, the IT load (set of jobs) is converted into a hourly power profile once scheduled. On the other hand, the management of the renewable energy sources of the power decision module (PDM) is explained in the rest of this paper.

3 Model

As mentioned before, the power supply system of the data center consists of photovoltaic panels, a wind farm, an energy storage system (ESS) made of a battery bank, regenerative hydrogen energy units composed of proton exchange membrane fuel cell systems (FC) combined with power exchange membrane electrolyzers (EZ) units to supply the data center as shown in Figure 2. This hybrid system works as follows:

- Solar panels (photo-voltaic panels – PV) and wind turbines (WT) constitute the primary sources to supply the data center. In this paper, all PV (resp. WT) are identical. Then, such sources are considered as a unique PV (resp. WT) system.

- Batteries and hydrogen system are the secondary sources, working as storage elements respectively for short term (within a day) and long term storage (seasonal). In this paper, all batteries (resp. fuel cells and electrolyzers (EZ)) are considered as one battery (resp. one FC and EZ).

Moreover, to ensure the sustainability of the data center, the storage level of hydrogen must follow a predefined level ($LOHtarget_D$) for each day D of a year. We assume that this target is known. It can be obtained thanks to a sizing and weather trend studies depending on the location of the data center. This study constitutes a challenging issue that is not addressed in this paper but is included in the ANR DATAZERO project.

In order to properly analyze and implement this hybrid system, it is mandatory to describe the model of each component. For that, Table 1 lists all the notations used in the following sections. First of all, let $\mathcal{H} = K\Delta t$ a time window discretized into K identical periods of duration Δt unit of time.

Depending on the case, let $k \in \llbracket 0, K \rrbracket$ be defined as both the $(k+1)$ th time step at instant $k\Delta t$ from the beginning of \mathcal{H} and the index of the $(k+1)$ th period Δt of \mathcal{H} defined between the two time step k and $k+1$, i.e., $k=0$ designs the first time step of \mathcal{H} and $k=K$ the first time step of the next time window.

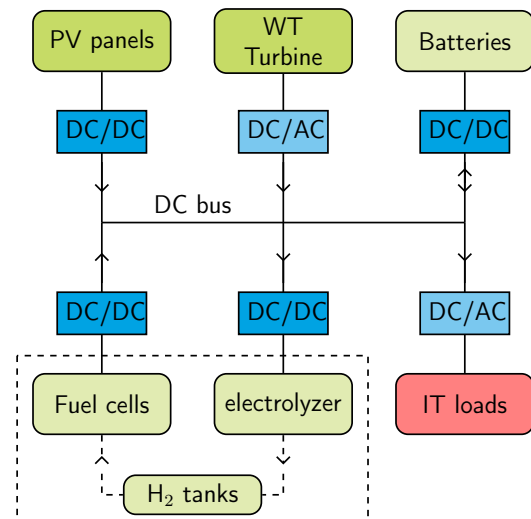


Figure 2 Structure of the DC microgrid supplying the data center loads (source: Robin Roche).

The model of this hybrid renewable energy system is defined as follows:

- **Photovoltaic panels:** The relation between the irradiation data I_k at time step k , the area of the PV

Table 1 Nomenclature

Notations	Description
<i>Time discretization</i>	
\mathcal{H}	a given time window
Δt	interval of time between two time steps
k	index for one time step within \mathcal{H}
K	number of time steps within \mathcal{H}
<i>Solar panel</i>	
A_{pv}	PV area [m^2]
η_{pv}	PV efficiency [%]
I_k	Solar irradiation of tilted surface [$kW.m^{-2}$]
Ppv_k	PV power [kW]
<i>Wind turbines</i>	
A_{wt}	WT rotor swept area [m^2]
η_{wt}	WT efficiency [%]
P_r	rated power of the WT [kW]
Pw_k	WT power produced [kW]
<i>Batteries</i>	
$Cbat$	the maximal capacity of the battery [kWh]
$SOCmax$	State of Charge (SOC) upper limit [%]
$SOCmin$	SOC lower limit [%]
η_{ch}	Battery charge efficiency [%]
η_{dch}	Battery discharge efficiency [%]
σ	Battery self-discharge rate [%]
SOC_k	SOC at instant $k\Delta t$ [%]
Pch_k	Power used to recharge battery [kW]
$Pdch_k$	Power discharged from battery [kW]
<i>Electrolyzer</i>	
$Pezmax$	Electrolyzer power upper limit [%]
$Pezmin$	Electrolyzer power lower limit [%]
η_{ez}	Electrolyzer efficiency [%]
Pez_k	Power put into electrolyzer [kW]
Qez_k	Electrolyzer H_2 mass [kg]
<i>Fuel Cell</i>	
$Pfemax$	Maximum power delivered by fuel cell [kW]
η_{fc}	Fuel Cell efficiency [%]
Pfc_k	Power delivered by fuel cell at $k\Delta t$ [kW]
Qfc_k	Fuel cell H_2 mass [kg]
<i>Hydrogen tank</i>	
$LOHtarget_D$	H_2 tank level targeted for a given day D
$LOHmax$	H_2 tank upper limit [%]
$LHVh_2$	H_2 lower heating value [$kWh.kg^{-1}$]
$HHVh_2$	H_2 higher heating value [$kWh.kg^{-1}$]
η_{tank}	H_2 tank efficiency [%]
LOH_k	H_2 tank inventory level [kg]
<i>others</i>	
η_{inv}	Converter efficiency [%]
x_k	Battery in use ($x_k = 1$) or not ($x_k = 0$)
y_k	Electrolyzer in use ($y_k = 1$) or not ($y_k = 0$)
z_k	H_2 in charge ($z_k = 1$) or discharge ($z_k = 0$)
u_k	used in the mutual exclusion (H_2 vs batteries)
v_k	used in the mutual exclusion (H_2 vs batteries)

panels A_{pv} , PV panels efficiency η_{pv} and the output power Ppv_k of the PV panels defined for each period k ($k \in \llbracket 0, K - 1 \rrbracket$), is described as follows for the whole time period Δt that begins at instant $k\Delta t$:

$$Ppv_k = I_k \times A_{pv} \times \eta_{pv} \quad (1)$$

– **Wind turbines:** The total power output Pwt_k defined for each period k ($k \in \llbracket 0, K - 1 \rrbracket$) of the wind turbine generator as a function of the total swept area by the blades A_{wt} and the efficiency of the wind turbine η_{wt} is given in the following equation:

$$Pwt_k = Pw_k \times A_{wt} \times \eta_{wt} \quad (2)$$

where Pw_k follows the mathematical model (3) depending on the wind speed values:

$$Pw_k = \begin{cases} 0 & \text{if } V_k \leq V_{ci} \\ Pr \cdot \frac{V_k - V_{ci}}{V_r - V_{ci}} & \text{if } V_{ci} < V_k \leq V_r \\ Pr & \text{if } V_r < V_k \leq V_{co} \\ 0 & \text{if } V_{co} < V_k \end{cases} \quad (3)$$

where V_k in the wind speed between time steps k and $k + 1$, V_{ci} is the cut in wind speed for which the wind turbine start working, V_{co} is the cut out wind speed for which the wind turbine stops working, V_r is the rated wind speed for which the wind turbine operate in its rated power P_r .

– **Batteries:** The charging and discharging equations of the battery are calculated for each k with $k \in \llbracket 1, K \rrbracket$ respectively in Equations (5) and (6) and with respect to the previous state of charge of the battery SOC_{k-1} , the self-discharge rate σ , the maximal capacity of the battery $Cbat$, the charging, discharging power Pch_{k-1} , $Pdch_{k-1}$ and the charging, discharging efficiency η_{ch} , η_{dch} . Let SOC_0 be the initial state of the charge of the battery at the beginning of the current horizon \mathcal{H} in the following equations:

$$SOC_k = SOC_{k-1} \times (1 - \sigma) + \frac{Pch_{k-1} \times \eta_{ch} \times \Delta t - \frac{Pdch_{k-1}}{\eta_{dch}} \times \Delta t}{Cbat} \quad (4)$$

with $SOCmin \leq SOC_k \leq SOCmax$

The battery energy system (BES) cannot charge and discharge at the same time. In fact, the charging process ends when either the BES system reaches its maximum capacity or the available energy by renewable sources dedicated to be stored is charged on the BES.

$$SOC_k = \min\{SOC_{k-1} \times (1 - \sigma) \quad (5)$$

$$+ \frac{Pch_{k-1} \times \eta_{ch} \times \Delta t}{Cbat}, SOCmax\} \quad \text{if } Pch_{k-1} > 0$$

$$SOC_k = \max\{SOC_{k-1} \times (1 - \sigma) - \frac{Pdch_{k-1}}{\eta_{dch} Cbat} \times \Delta t, SOCmin\} \quad \text{if } Pdch_{k-1} > 0 \quad (6)$$

On the contrary, if the energy production cannot satisfy the energy demand, the battery starts the discharging process either until its lower capacity limit is reached or the load demand is completely met by the energy sources production.

- **Electrolyzer:** As explained in [4], the output power of the electrolyzer Pez_k able to produce the H_2 mass Qez_k during Δt is defined for each period k ($k \in \llbracket 0, K - 1 \rrbracket$) as follows:

$$Pez_k \times \Delta t = \frac{HHVh_2 \times Qez_k}{\eta_{ez}} \quad (7)$$

with $Pezmin$, $Pezmax$ the operating range of the electrolyzer such that $Pezmin \leq Pez_k \leq Pezmax$, Qez_k the mass of H_2 produced by the electrolyzer during Δt in (kg), η_{ez} the efficiency of the electrolyzer and $HHVh_2$ hydrogen higher heating value.

- **Fuel Cell:** The output power of the fuel cell Pfc_k is calculated at any time during each period k ($k \in \llbracket 0, K - 1 \rrbracket$) in the following equation:

$$Pfc_k \times \Delta t = LHVh_2 \times Qfc_k \times \eta_{fc} \quad (8)$$

with $Pfc_k \leq Pfcmax$, Qfc_k the H_2 mass consumed by the fuel cell during Δt , η_{fc} the efficiency and $LHVh_2$ the low heating value of hydrogen.

- **Hydrogen tank:** The hydrogen produced by the electrolyzer and consumed by the fuel cell is stored in tanks. Thus, the level of hydrogen in the tank is calculated at any time during each period k with $k \in \llbracket 1, K \rrbracket$ as follows:

$$LOH_k = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1}/\eta_{tank} \quad (9)$$

with $0 \leq LOH_k \leq LOHmax$

Let LOH_0 be the initial value of the level of hydrogen.

Considering the previous simplified model for all energy sources, we propose to show how they can be used to solve the optimization problems we face.

4 Problem statement

The negotiation module aims to guide both the decision optimization modules (ITDM and PDM) in order to converge to a power profile, first, close to the one requested by IT and second, feasible by the electrical part. In evidence, the IT decision module would prefer to execute jobs when that is better for Quality of Service (QoS) constraints. However, it most likely may not match with the best usage of renewable energy and storage devices. Then, it is mandatory to confront IT requests with the energy availability which is computed by the PDM. As a consequence, the strategy describing the exchange of power profiles between the three modules is done as illustrated in Figure 3 and is explained in details in the next subsection.

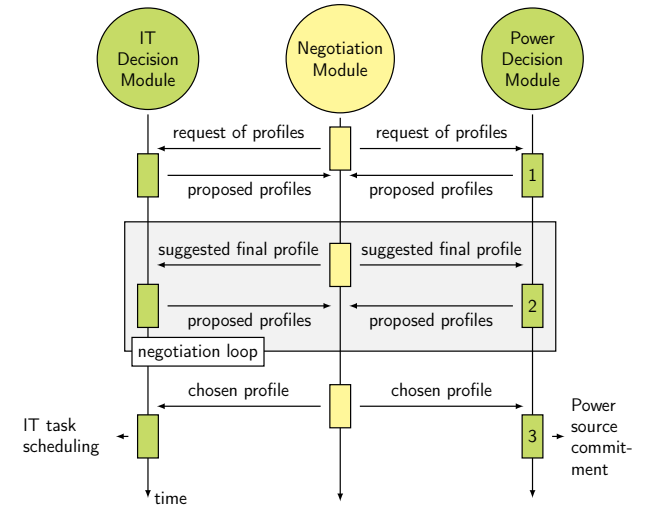


Figure 3 Illustration of the negotiation process, with the information exchanged between the both decision modules (ITDM and PDM) and the negotiation module.

Thus, the negotiation module forces both ITDM and PDM to design one or multiple power profiles and to send them for each negotiation round. In order to converge and to find the best source commitment for both modules, each power profile sent must be different from the one sent in the previous negotiation round. Therefore, the power decision module addresses different optimization problems according to the purpose of the work and the constraints of the system. The primary goal of the power management system consists in defining the best commitment to satisfy the power demand. To make the optimization process readable, the list of notations used is summarized in Table 1.

4.1 Strategies of the power decision module

As seen previously in the negotiation process, several kind of requests are asked to the power management module. This leads to design different kind of power profiles depending on the round of negotiation. So, we can define several optimization programs, each specifically addressing one of the underlying problems. In the strategy proposed (see Figure 3), the negotiation module (NM) starts by requesting different power profiles. PDM has to identify which source commitment can be proposed regarding the energy storage levels and the weather forecasting (green box labeled 1 in Figure 3). This is done following two different goals:

- Providing the maximum constant power profile that the infrastructure is able to produce while respecting all the constraints and the storage state and taking the weather forecasting during the current horizon into account. This process is detailed in Section 6.1.
- Providing a non constant power profile that optimize the power production without using the storage devices. As using the storage devices involves losses because of their efficiency, the power profile given would be the one produced by the renewable sources. This process is detailed in Section 6.2.

In the second round of the negotiation, the NM sends a power profile and asks to design a new profile that is close to the given one (green box labeled 2 in Figure 3). In this case, the optimization program has another goal:

- Matching with the given load profile: the problem consists in finding an alternative power profile as close as possible to the profile required by the NM. If this profile is not reachable, the power constraint is relaxed using a given rate (relaxation factor). Additional constraints and variables force the power production for each period to be over the values of the relaxed power profile while respecting the constraints defined by the model and the storage state. This process is detailed in Section 6.3.

Once the negotiation ends, the NM send the chosen profile to both PDM and ITDM. Then, PDM has to find the best commitment of the power sources to answer to that chosen profile (green box labeled 3 in Figure 3). This third problem follows another goal:

- Satisfying the load demand. The strategy proposed is to maximize the long-term storage (i.e. the hydrogen storage) by setting a target level of stored hydrogen to reach at the end of the horizon. This

allows ensuring the seasonality variation of renewable energy production. This process is detailed in Section 6.4.

From another part, the PDM represents the order for the Power source manager which is responsible for the electrical power command that the latter has to respect. In fact, the electrical sources must follow the commitment of the PDM. All the previously described strategies are based on common constraints that translate the physical laws of the power system. The remainder of this section describes those constraints.

4.2 Flow conservation

The power produced ($Pwt_k + Ppv_k$) by the primary sources during the whole period k is used for three purposes:

- Hydrogen production (Pez_k),
- Charging the batteries (Pch_k),
- Satisfaction of the data center demand ($Pload_k$).

In case there is not enough renewable energy to meet the demand ($Pload_k$), additional electrical power is delivered by the fuel cells (Pfc_k) and batteries ($Pdch_k$). To satisfy the demand, the following equation should be fulfilled for each k with $k \in \llbracket 0, K - 1 \rrbracket$:

$$Pload_k \leq Pwt_k + Ppv_k + (Pfc_k + Pdch_k - Pez_k - Pch_k) \times \eta_{inv} \quad (10)$$

4.3 Constraint Satisfaction Problem

The resulting model can be viewed as a Constraint Satisfaction Problem (CSP). This model is linearized in the next section to be solved using an efficient solver as Gurobi [15]. This allows proposing solutions optimally computed by the PDM: (i) identification of the profile that maximizes the power produced, (ii) computation of an optimal commitment around a target profile considering a given relaxation factor, and (iii) computation of an optimal commitment constrained by the load profile.

As a result, the CSP is defined as follows (with $k \in \llbracket 0, K - 1 \rrbracket$ or $k \in \llbracket 0, K \rrbracket$ for SOC_k and LOH_k variables):

$$\begin{aligned}
Pload_k &\leq Pwt_k + Ppv_k + (Pfc_k + Pdch_k) \\
&\quad \eta_{inv} - (Pez_k + Pch_k)\eta_{inv} \\
SOC_k &= \min\{SOC_{k-1} \times (1 - \sigma) + Pch_{k-1} \\
&\quad \times \eta_{ch} \times \Delta t, SOC_{max}\} \quad \text{if } Pch_{k-1} > 0 \\
SOC_k &= \max\{SOC_{k-1} \times (1 - \sigma) - \frac{Pdch_{k-1}}{\eta_{dch}} \\
&\quad \times \Delta t, SOC_{min}\} \quad \text{if } Pdch_{k-1} > 0 \\
Pez_k \Delta t &= HHVh_2 \times Qez_k / \eta_{ez} \\
Pfc_k \Delta t &= LHVh_2 \times Qfc_k \times \eta_{fc} \\
LOH_k &= LOH_{k-1} + Qez_{k-1} - Qfc_{k-1} / \eta_{tank} \\
\text{Bounds:} \\
Pfc_k &\leq Pfc_{max} \\
Pez_{min} &\leq Pez_k \leq Pez_{max} \\
SOC_{min} &\leq SOC_k \leq SOC_{max} \\
0 &\leq LOH_k \leq LOH_{max}
\end{aligned}$$

(11)

4.4 Context of the resolution

In addition, common sense rules have to be considered to allow the use of power components without any time restriction if the two following constraints are respected:

- When fuel cells start working, it is only used to satisfy the demand and not to charge batteries.
- When batteries start discharging, they are only used to satisfy the demand and not to produce hydrogen.

In the next section, we propose to transform the CSP in a linear constraint satisfaction problem.

5 Constraint Linearization

In this section, in order to be solved, the proposed CSP (11) is linearized.

5.1 Linearization of the constraints

Each non linear constraint of the model is transformed to obtain a linear constraint.

5.1.1 The battery state of charge

The state of charge of the battery is limited by the SOC range (SOC_{min} and SOC_{max}) with $k \in \llbracket 0, K \rrbracket$ and depends both on the charge and discharge phases:

$$\begin{cases}
SOC_{min} \leq SOC_k \leq SOC_{max} \\
SOC_k = SOC_{k-1}(1 - \sigma) \\
\quad + \frac{Pch_{k-1}\Delta t \times \eta_{ch} - Pdch_{k-1}\Delta t / \eta_{dch}}{Cbat}
\end{cases} \quad (12)$$

As the battery can not charge and discharge at the same time, we introduce the set of binary variables x_k , and two sets of variables Pch'_k , $Pdch'_k$ with $k \in \llbracket 0, K - 1 \rrbracket$ such as:

$$\begin{cases}
Pch_k = x_k \times Pch'_k \\
Pdch_k = (1 - x_k) \times Pdch'_k
\end{cases} \quad (13)$$

where $x_k = 0$ means that the battery is discharging and $x_k = 1$ means that the battery is charging. In this way, the battery can not charge and discharge at the same time. Then we propose to rewrite the previous state of charge equations as the following:

$$\begin{cases}
SOC_{min} \leq SOC_k \leq SOC_{max} \\
SOC_k = SOC_{k-1}(1 - \sigma) \\
\quad + \frac{x_k \times Pch'_{k-1} \times \Delta t \times \eta_{ch} - (1 - x_k) \times Pdch'_{k-1} \Delta t / \eta_{dch}}{Cbat}
\end{cases} \quad (14)$$

Due to these substitutions, we add new constraints to linearize Equation (14):

$$\begin{cases}
0 \leq Pch_k \leq Pch_{max} \\
Pch_k \geq 0 \\
Pch_k \leq x_k \times Pch_{max} \\
Pch_k \leq Pch'_k \\
Pch_k \geq Pch'_k - (1 - x_k) Pch_{max}
\end{cases} \quad (15)$$

$$\begin{cases}
0 \leq Pdch_k \leq Pdch_{max} \\
Pdch_k \geq 0 \\
Pdch_k \leq (1 - x_k) \times Pdch_{max} \\
Pdch_k \leq Pdch'_k \\
Pdch_k \geq Pdch'_k - x_k Pdch_{max}
\end{cases} \quad (16)$$

Because Equation (13) is not written within the final linear program, the fact that the battery can not

charge and discharge is introduced by other new equations:

$$\begin{cases} Pch_k \leq x_k \times Pchmax & \text{with } k \in \llbracket 0, K-1 \rrbracket \\ Pdch_k \leq (1-x_k) \times Pdchmax & \text{with } k \in \llbracket 0, K-1 \rrbracket \\ x_k \in \{0, 1\} \end{cases} \quad (17)$$

where $Pchmax$ and $Pdchmax$ are the respective upper-bound of Pch_k and $Pdch_k$.

Battery operation: The battery is supposed to balance underproduction and overproduction during a period of time T . For instance if $T = 24h$ with $\Delta t = 1h$ and $K = 24$, batteries are used for the fluctuations between day and night. It means that the production is smoothed over the day. To make it possible, the level of the state of charge of the battery SOC_K should be its value at the beginning SOC_0 of each period T . This operation is explained by the following to fix values before the resolution of the program if T is larger than $24h$ (one day):

$$\begin{cases} SOC_K = SOC_0 = SOC_{init} & \text{if } K < T = 24 \\ SOC_k = SOC_0 = SOC_{init} & \text{if } K \geq T = 24 \\ \text{and } k\%24 = 0 & (k \in \llbracket 0, K \rrbracket) \end{cases} \quad (18)$$

with SOC_{init} the right level of charge to make possible the daily power compensation from hours where an extra renewable production is existing to hours this production is lacking. That is why this level has to come back to the same level each day. The difference between days is compensated by using long term storage.

5.1.2 Electrolyzer

As explained in Section 3 (Model), the electrolyzer operates only while respecting the power range, otherwise it does not work and its power equals zero. The following bounds express these cases:

$$\begin{cases} \forall k \in \llbracket 0, K-1 \rrbracket & Pezmin \leq Pez_k \leq Pezmax \\ \forall k \in \llbracket 0, K-1 \rrbracket & Pez_k \geq 0 \end{cases} \quad (19)$$

It is then necessary to introduce a set of binary variables y_k (with $k \in \llbracket 0, K-1 \rrbracket$) to model the two alternatives where:

- $y_k = 1$ means that the electrolyzer is in use with $Pezmin \leq Pez_k \leq Pezmax$ during period k ,
- $y_k = 0$ means that the electrolyzer is stopped during period k .

By adding this binary variables, Equations (19) become:

$$\begin{cases} (1-y_k) \times Pez_k = 0 \\ y_k \times Pez_k \leq Pezmax \\ y_k \times Pez_k \geq y_k \times Pezmin \\ y_k \in \{0, 1\} \end{cases} \quad (20)$$

Due to the non linearity of the set of Constraints (20), we propose to add a new substitution of variable Pez'_k to keep Pez_k being the relevant variables that express the use of the electrolyzer. We define the following relation to make the linearization possible:

$$Pez_k = y_k \times Pez'_k \quad (21)$$

then we add the following equations to linearize (20):

$$\begin{cases} Pez_k \leq Pez'_k \\ Pez_k \geq 0 \\ Pez_k \leq y_k \times Pezmax \\ Pez_k \geq Pez'_k - (1-y_k)Pezmax \\ 0 \leq Pez'_k \leq Pezmax \\ Pez_k \geq y_k \times Pezmin \\ y_k \in \{0, 1\} \end{cases} \quad (22)$$

5.1.3 Hydrogen tank level

As mentioned before for the battery, it is necessary to manage Qfc_k and Qez_k in order to control the hydrogen mass flow circulating in the hydrogen tank as mentioned in Equation (9). Equations (7), (8) and (9) can be written by considering the new definition of Qez_k and Qfc_k for $k \in \llbracket 0, K \rrbracket$:

$$\begin{cases} Pez_k \Delta t = HHVh_2 \times Qez_k / \eta_{ez} \\ Pfc_k \Delta t = LHVh_2 \times Qfc_k \times \eta_{fc} \\ LOH_k = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1} / \eta_{tank} \end{cases} \quad (23)$$

Therefore, additionally to the two new sets of variables Qez'_k and Qfc'_k , we introduce an other set of binary variables z_k to model the two alternatives where the fuel cells are in use or not (with $k \in \llbracket 0, K-1 \rrbracket$). As before and for the same reasons, let be the following variable substitutions:

$$\begin{cases} Qez_k = z_k \times Qez'_k \\ Qfc_k = (1 - z_k) \times Qfc'_k \end{cases} \quad (24)$$

where:

- $z_k = 1$ means that $Qfc_k = 0$
- $z_k = 0$ means that $Qez_k = 0$

then we add the following set of equations:

$$\begin{cases} Qez_k \leq Qez'_k \\ Qez_k \geq 0 \\ Qez_k \leq z_k \times Qezmax \\ Qez_k \geq Qez'_k - (1 - z_k)Qezmax \\ 0 \leq Qez_k \leq Qezmax \end{cases} \quad (25)$$

$$\begin{cases} Qfc_k \leq Qfc'_k \\ Qfc_k \geq 0 \\ Qfc_k \leq (1 - z_k) \times Qfcmax \\ Qfc_k \geq Qfc'_k - z_k \times Qfcmax \\ 0 \leq Qfc_k \leq Qfcmax \end{cases} \quad (26)$$

In the rest of the paper, we use these constraints as a basic model for the different usage of the PDM.

5.2 Additional linear constraints

As indicated in Section 4.4, let us recall the common sense usage rules.

5.2.1 Mutual exclusion between hydrogen and battery

The valid usage cases are:

1. The battery is in charge ($x_k = 1$) while electrolyzer can be in use ($y_k = 0$ or 1) and obviously the fuel cell is stopped ($z_k = 1$).
2. The battery is discharging ($x_k = 0$) then the fuel cell can be in use ($z_k = 0$ or 1) and the electrolyzer has to be stopped ($y_k = 0$).

3. Start and stop of the fuel cell and the electrolyzer are allowed in this problem.

Considering these rules, there are only 4 available configurations for the variables x_k, y_k and z_k which are listed in Table 2. Constraint (27) represents the solution to these requirements. Conversely the fourth other combinations do not satisfy these constraints.

x_k	y_k	z_k
0	0	0
0	0	1
1	0	1
1	1	1

Table 2 Valid configurations for variables x_k, y_k and z_k

$$(1 - x_k)(1 - y_k) + x_k \times z_k \geq 1 \quad (27)$$

Due to the non linearity of Constraints (27), we add a new set of variables u_k and v_k (with $k \in \llbracket 0, K-1 \rrbracket$) that express the mutual exclusion between hydrogen system and battery where:

- $u_k = x_k \times y_k$
- $v_k = x_k \times z_k$

then we add the following equation:

$$u_k + v_k - x_k - y_k \geq 0 \quad (28)$$

with

$$\begin{cases} u_k \leq x_k \\ u_k \leq y_k \\ 1 - x_k - y_k + u_k \geq 0 \\ u_k \geq 0 \end{cases} \quad (29)$$

$$\begin{cases} v_k \leq x_k \\ v_k \leq z_k \\ 1 - x_k - z_k + v_k \geq 0 \\ v_k \geq 0 \end{cases} \quad (30)$$

The obtained linear constraint satisfaction problem is used in the following section as a basic model for defining the different mixed integer linear programs designed for solving optimization problems associated with the power decision module.

6 Power Decision Module PDM

The power decision module (PDM) consists in a black box composed by several internal components to ensure the management of the hybrid renewable energy sources by solving different optimization problems corresponding to negotiation rounds. These problems are expressed using linear programming formulation. Thus, as detailed in Section 4.1, the PDM is able to design different profiles depending on the goal it has to ensure.

The problem takes as input the renewable power produced under weather conditions $P_{renew_k} = P_{pv_k} + P_{wt_k}$, power demand P_{load_k} and other information of sizing like the number of wind turbines, the surface area of PV, the energy storage capacity and the efficiency of any component. As a solution, its resolution gives a schedule of each time slot for supply-side source and energy storage usage, according to the availability of renewable power as explained in Section 3.

The optimization problems explained in the next paragraphs are implemented using python and are solved using the GUROBI solver [15]. The power supply sizing and weather conditions are the same for each of the following optimization problems for illustration purpose.

6.1 Providing a constant power profile P_{prod}

In this section, the aim is to obtain a maximum power production P_{prod} from the primary sources for the whole horizon \mathcal{H} , taking into account the efficiency of each storage part used. Then the PDM takes as input the meteorological data (to determine the primary production), the initial values of the storage levels (SOC_0 and LOH_0) and the target set. As an output, the PDM must send the maximum constant profile and the storage variation (SOC_k and LOH_k) to the negotiation module.

To make this possible, some modifications are set in the mixed integer linear program and a new objective function and new constraints are added. To simplify it, the new variables added are explained in Table 3.

Table 3 Additional notations

Notations	Description
P_{prod}	The constant power profile [kW]
LOH_{target_D}	A level of hydrogen defined by the sizing needed to be reached at the end of the horizon \mathcal{H} [kg]

6.1.1 Objective function

The objective function consists of maximizing the constant power profile obtained from the source commitment P_{prod} in order to propose a profile in the first part to the negotiation. The problem is thus mathematically translated to:

$$\text{maximize } P_{prod} \quad (31)$$

6.1.2 Additional constraints

Some constraints are added or modified in order to consider common sense usage rules: consequently, Equation (10) is modified in this program as (32). Another constraint (33) is added to ensure the hydrogen level at the end of the period of simulation reached the target defined. This allows the storage system to handle the next periods.

$$\forall k \in \llbracket 0, K - 1 \rrbracket$$

$$P_{prod} \leq P_{wt_k} + P_{pv_k} + (P_{fc_k} + P_{dch_k} - P_{ez_k} - P_{ch_k})\eta_{inv} \quad (32)$$

$$LOH_{target_D} \leq LOH_K \quad (33)$$

The hydrogen target level LOH_{target_D} is supposed to be computed based on long term weather forecasting and IT load consumption for one year. D represents the day number within the current year and matches with the time horizon $K \times \Delta t$. We assume that the values of LOH_{target_D} with $1 \leq D \leq 365$ are obviously given by the preliminary sizing study of the green data center.

6.1.3 Obtained model

The constraints explained in Section 5.1 are used for each version of the PDM as the basic constraints. Then, the linear program able to produce a constant maximum profile using the storage system composed of batteries and hydrogen system is then written as mentioned in the appendix A.

6.2 Providing a variable power profile

In this section, the aim of providing a non constant profile comes from the fact that the data center can start and stops servers depending on its job scheduler. It consist in obtaining a maximum variable power production profile $Pprod_k$ ($k \in \llbracket 0, K - 1 \rrbracket$) from the primary sources, taking into account the efficiency of each storage part used in order to provide multiple profiles to the negotiation module. Then the PDM takes the meteorological data as an input to determine the primary production along the horizon \mathcal{H} , the initial values of the storage level (SOC_0 and LOH_0).

As an output, the PDM must send the maximum power profile, and the storage variation (SOC_k and LOH_k) to the negotiation module.

To make this possible, some modifications are set to the linear program obtained in the previous section. To simplify it, the variable $Pprod$ is no longer a constant value during the horizon \mathcal{H} but is changes following each step k in the horizon.

6.2.1 Objective function

For this strategy, the objective function consists of maximizing the power profile obtained from the source commitment $Pprod$ in order to address to the data center load. The problem is thus mathematically translated to:

$$\text{maximize } \sum_{k=0}^{K-1} Pprod_k \quad (34)$$

6.2.2 Added constraints

As in the constant power case, some constraints are added or modified to consider common sense usage rules then Equation (10) is modified in this program as (35) ($\forall k \in \llbracket 0, K - 1 \rrbracket$):

$$Pprod_k \leq Pwt_k + Ppv_k + (Pfc_k + Ppch_k - Pez_k - Pch_k)\eta_{inv} \quad (35)$$

The same constraint (33) is added to ensure the target level of hydrogen is reached at the end of the period of simulation, so that the storage system is able to handle the next periods.

6.2.3 Obtained model

The linear program is able to produce a maximum non constant profile using the storage system composed of batteries and hydrogen system. It is then written as in the appendix B.

6.3 Matching with a requested profile

In this subsection, the aim is to obtain a profile which is matching with a profile requested by the negotiation module to end up with the negotiation between both modules. Thus, the PDM takes as an input the data of the profile requested by the negotiation module, the meteorological data to determine the primary production along the horizon \mathcal{H} , the initial values of the storage level (SOC_0 and LOH_0), etc. As an output, the PDM must send the closest profile ($Pprod$) to the one received by the negotiation module ($Pload$). To make this possible, some modifications are set for the basic linear program proposed and a new objective function and new constraints are added.

6.3.1 Objective function

In order to be able to fulfill the data center demand in every situation (overproduction or underproduction), we add a relaxation factor α capable to relax the power demand in order to create a profile $Pprod_k$ that matches the most with the load $Pload_k$

Thus the objective function consists in minimizing the value of the relaxation factor α to be as close as possible to the demand.

$$\text{minimize } \alpha \quad (36)$$

6.3.2 Added constraints

As in the two previous cases, considering common sense usage rules turns Equation (10) into Equation (35). Constraint (33) is added also in order to force the hydrogen level at the end of the period of simulation (LOH_k) to be bigger than or equal to the level of hydrogen target. Thus, the storage system is able to handle the next future power requirement. In this stage of the negotiation, in order to satisfy the profile requested by NM, a new constraint is added to the linear program as defined in Equation (37). Therefore, we introduce a α computed by binary research to enable the power produced $Pprod_k$ in each time step k to be greater than or equal to $(1 - \alpha) \times Pload_k$.

$$Pprod_k \geq (1 - \alpha) \times Pload_k \quad (37)$$

The feasibility of the linear program depends on the α value:

- if $\alpha = 0$ it means that the profile generated is the same as the one provided by the NM;
- if $\alpha = 1$ it means that the profile could be entirely different from the one provided.

As the data center load is relaxed, another management is proposed. The solution is thus sub-optimal compared to the initial power demand, but an alternative feasible solution is proposed to overcome the intermittent nature of renewable sources.

6.3.3 Obtained model

The linear program able to produce a profile that matches with a given one from the negotiation module using the storage system is then written as mentioned in the appendix C.

6.4 Source commitment

This problem is, in fact, the last step of the negotiation process. It is addressed once the negotiation has converged to the appropriate power profile agreed on. This power profile is then sent by the negotiation module to the PDM where used as an input ($Pload$). Moreover, the PDM takes as input the meteorological data to determine the primary production along the horizon \mathcal{H} , the initial values of the storage level (SOC_0 and LOH_0), etc. As an output, the PDM must give the best usage of the power sources and energy storage for the next period of the next time window \mathcal{H} .

6.4.1 Objective function

The objective function is to maximize long-term stocks by setting a target level hydrogen to reach at each end of horizon. Target stocks are set by the provisions of renewable energy production and by the capabilities of the components. The problem is thus mathematically translated by supplying the power demand (Constraint (39)) and by maximizing the level of hydrogen LOH_K at the end of the horizon. This objective allows to store the waste of energy available during that time horizon so as to supply underproduction days in the future.

The objective function is defined as:

$$\text{maximize } LOH_K \quad (38)$$

6.4.2 Added constraints

To satisfy the power demand $Pload_k$, the following constraint is added:

$$Pload_k \leq Pprod_k \quad (39)$$

6.4.3 Obtained model

The linear program obtained for the source commitment is defined, $\forall k \in \llbracket 0, K - 1 \rrbracket$ for all constraints except $k \in \llbracket 0, K \rrbracket$ for constraints containing variables SOC_k , LOH_k , Qez_k , Qfc_k , Qez'_k and Qfc'_k as mentioned in the appendix D.

7 Experiments and results

In this section, the linear programs obtained below are used with the following inputs in order to obtain different optimal commitment of the sources according to the stage of the negotiation. In fact, the program was executed following different resolution time windows for the same horizon (1 year) in [20]. The same sizing is played from the year 2004 till 2012. For each year, several resolution time windows (one week, three days, one day) are simulated with the weather condition of the same year. Simulation results shows that the best resolution time windows is 3 days and that the resolution time is 44.8 s. Experiments are performed on an Intel® Core™ i5-6200U CPU @ 2.30GHz × 4, 8GB RAM, 64-bit using Ubuntu 16.04 LTS as exploitation system. The time for solving each simulation is less than 1 minute using Gurobi optimizer [15].

7.1 Input data

Weather conditions: To simulate the primary sources production (photovoltaic panels and wind turbines), one needs to download meteorological data such as the solar radiation and wind speed data. These data can be obtained from various database online. In our case, the solar radiation data are downloaded from the National Solar Radiation Database (NSRDB) [35], and the wind speed data are downloaded from the wind prospector from the national Renewable Energy Laboratory (NREL) [9]. These data can be taken every hour during a day starting from 2004 till 2012. The chosen localization is Los Angeles with the following coordinates: Latitude: 34.57; Longitude -118.02; and elevation 807.

Workload: The workload \mathcal{W} is generated following the data from user requests recorded during the Soccer World Cup in 1998 and available on the web site¹. We have used the same methodology as in [43]. Each job should not be delayed more than three hours to be complete.

7.2 Settings

The input values of the sources used in the power decision module algorithms are summarized in Table 4.

Table 4 Input values of the power supply sizing process

Notation	Value	Units
P_r	400	[W]
V_r	10	[m/s]
V_{ci}	4	[m/s]
V_{co}	30	[m/s]
η_{pv}	0.163	–
A_{pv}	3149	m^2
η_{fc}	0.4	–
P_{fcmax}	1115	[W]
η_{ez}	0.4	–
P_{ezmax}	832.65	[W]
P_{ezmin}	50	[W]
LOH_{max}	10000	[kg]
η_{ch}	0.82	–
P_{chmax}	800	[W]
η_{dch}	0.82	–
P_{chmin}	800	[W]
C_{bat}	1000	[Wh]

In this article, simulations are given on three days (72 hours) for a better illustrations of the results. The chosen 3 days of reference starts from April the 30th to May the 2nd 2004. Considering the sun and the wind, Figure 4 illustrates the power production obtained the respective models of both primary sources. In order to define the renewable energy produced in each hour for a better use of the storage sources, we compute the sum (renewablePower) of each power production for each hour during these three days.

Based on Figure 4, one can notice a complementary between the sun and the wind in electrical power production which justifies the hybridization of the primary sources [18]. For example, at the 20th hour, the solar production is zero caused by the night and day alternation. Nevertheless, the wind turbine reaches its rated output power equals to $400kW$.

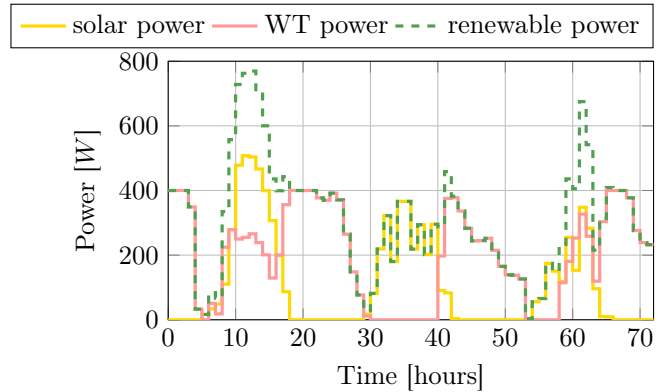


Figure 4 Renewable power production from April the 30th to May the 2nd 2004.

7.3 Experiment scenarios

7.3.1 Results Maximum constant power profile

In this linear program, we suppose that we are in the first stage of the negotiation which explains the absence of load in Figure 5. Actually, in that step of the negotiation, the PDM is supposed to provide the negotiation with profiles without getting data about the load. The same power architecture as in the previous section is used.

Results presented in Figure 5 are obtained by applying this linear program. The solution gives here a maximum constant power that can be delivered equal to $163kW$. As can be seen in this figure, the battery is responsible of the daily smoothing (day/night alternation). Thanks to Constraint (33), the level of hydrogen is even more than target at the end of the horizon \mathcal{H} ($LOH_{target_D} = 400kg$) to be able to assist the next horizon.

7.3.2 Results Maximum Power profile variable

Results presented in Figure 6 are obtained by applying this linear program. The production power P_{prod_k} is variable in some time step k . The same power architecture is used as in the previous subsections.

Moreover, one can notice that the state of the battery is constant all over the horizon considered. Indeed the system does not use the battery in order to get the best profile P_{prod_k} . As the battery cycling efficiency is less than 1, the charging and discharging of the battery would lead to power loss. The level of hydrogen is increasing from 300 kg to 400 kg in order to reach the target level. So, Constraint (33) is respected. As many optimal solutions exist, the MILP gives one optimal proposition. For instance, another solution consists in

¹ WorldCup'98 logs. <http://ita.ee.lbl.gov/html/contrib/WorldCup.html>

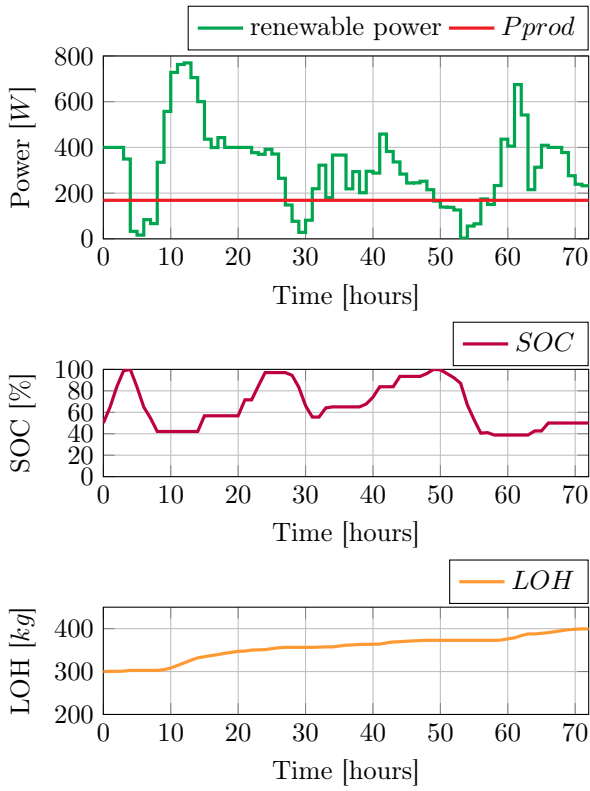


Figure 5 Constant Power Profile management.

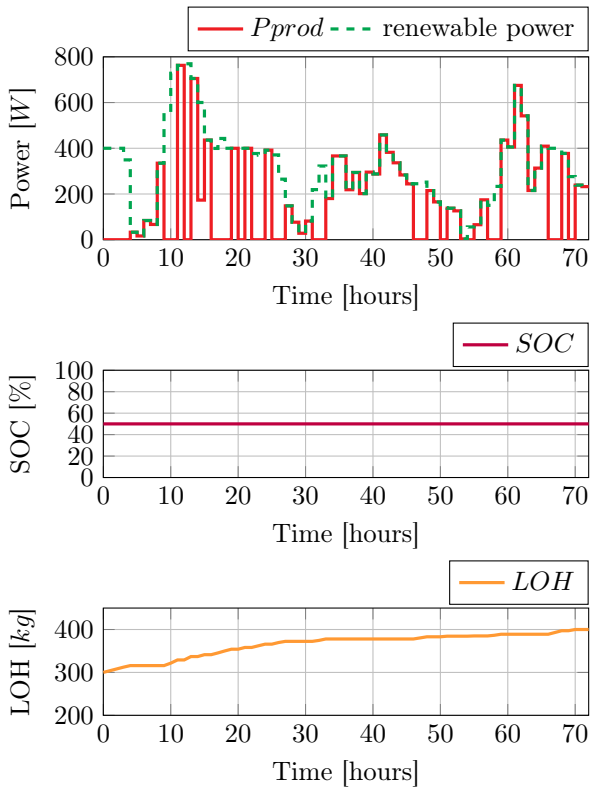


Figure 6 Maximum Power Profile management.

charging the *LOH* at the beginning of the time horizon and stays constant for period left.

7.3.3 Results Matching with a requested profile

Results presented in Figure 7 are obtained by applying this linear program. The production P_{prod} is completely similar to the demand (here the demand represents the power profile received from the negotiation module) as the relaxation factor is zero. The same power architecture is used as in the previous section. The load is variable between 100 kW and 400 kW in this case in order to exhibit large variations in the profile. The battery assures the smoothing of the day/night alternation and come back to the same level each 24h. The level of hydrogen is increasing from 300 kg to 400 kg in order to reach the target level fixed in Constraint (33).

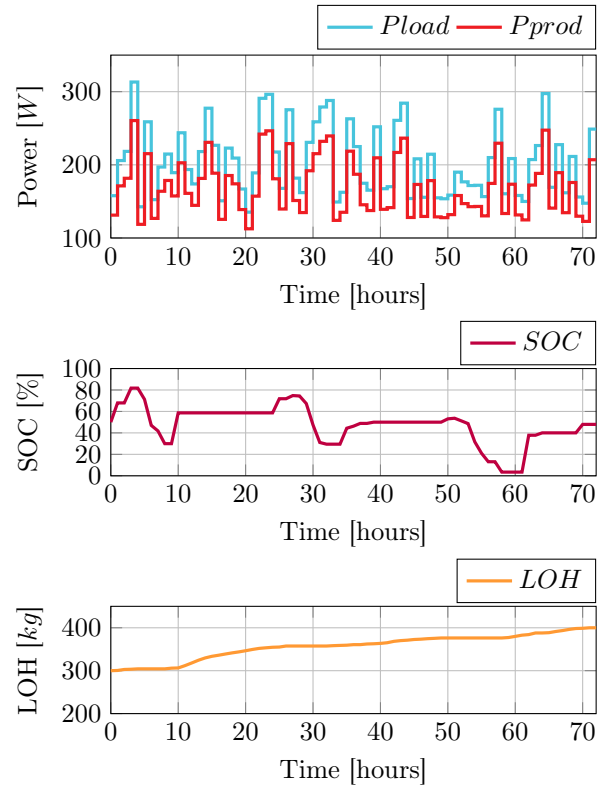


Figure 7 Management of the resources to match with a requested profile with $\alpha = 0.168$

If one considers a $\alpha = 0.168$, the results of the MILP are as showed in Figure 7. As we can see it, the profile generated P_{prod} is different from the provided one and respects the constraint given in Eq (37). In this case, one can see that the storage state of the battery varies all over the horizon in order to help the renewable production to fulfill the demand. The hydrogen level in-

creases in order to reach the target fixed at the end of the horizon $LOH_K = 400 \text{ kg}$.

7.3.4 Results of source commitment

Figure 8 shows the management of the different resources following the constraints explained in the previous sections. The power profile agreed on after the negotiation is designed with the best assignment of the sources and is completely equal to the load of the data center. Given the objective function, it can be noticed that the level of battery is varying all over the horizon in order to help the renewable production to fulfill the demand. Indeed, the level of hydrogen is increasing to maximize this objective at the end of the horizon. This choice can be justified by the difference of both storage device efficiencies.

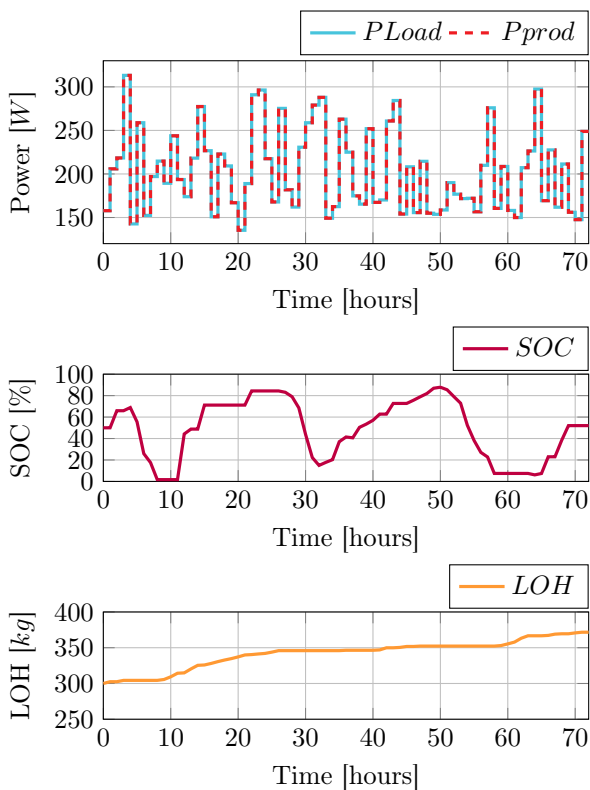


Figure 8 Source commitment results

7.4 Summary of the results

The results above suggest several interesting observations. First of all, the sizing of the electrical sources is very important as well as the values of the initial state of storage. They allow a good running of the programs. Otherwise, the management tool can provide an unfeasible model.

The MILP that matches with a given profile depends extremely of the relaxation factor. Sometimes, given the storage state at the moment of the negotiation and the energy production, the management tool provide an unfeasible model and is not capable to answer to the demand. The negotiation take action here and send a second profile with a different relaxation factor.

The execution time of the algorithms is at the scale of seconds which is compatible with the negotiation process as it's a synchronous negotiation.

The PDM is an efficient management tool of all energy sources (wind turbine, photovoltaics, batteries, fuel cells, electrolyzers) that is able to provide data center demand with 100% renewable energy.

Before concluding, we can mention that two negotiations in two different periods of the year converge to the same power profile to meet for supplying the data center. The two solutions, given after solving the two PDM power source commitment problems, have no reason to be the same. Indeed, these solutions do not only depend on the input power profile to address but also on the storage state and the target level of hydrogen at the end of the period.

8 Conclusion

In this paper, we presented (1) an analysis of the main trade offs involved in powering data centers with hybrid renewable energy system and the ANR DATAZERO project that aims to completely provide a data center with only renewable energy (2) a model of HRES composed of wind turbines, photovoltaic panels, batteries and hydrogen system (3) the problem statement defined by powering the demand of the data center with only renewable energy and the constraint satisfaction problem due to it (4) the linearization of the constraints in order to get a convenient usage of the sources and the mixed linear program which is used in the PDM (5) the power decision module which is a management tool able to manage a hybrid renewable energy system presenting four optimization problems depending on the stage of the negotiation. Additional constraints are also written to allow us to find appropriate solutions. These problems have been illustrated by several simulation. As the computation time is very short (less than 60 s) considering the complexity of the problem, a negotiation step can be launched as soon as the power system notes a significant deviation from storage. We show that our optimal models are convenient to address the power commitment of a 100% renewable energy data center, since the resolution is obtained within few seconds. As

future works, we plan to consider the aging of power sources in order to play maintenance scenarios similar to the real life one. For instance, one can manage in various manner one wind turbine or one battery depending on its degradation level so as to improve the sustainability of the power platform.

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Appendices

The range of the variables used in the four following MILPs are defined as follow:

- $Pch_k, Pdch_k, Pez_k, Pch'_k, Pdch'_k, Pez'_k, Qez_k, Qfc_k, Qez'_k, Qfc'_k, Pfc_k, Pez_k$ are defined $\forall k \in \llbracket 0, K-1 \rrbracket$,
- x_k, y_k, z_k, u_k, v_k are defined $\forall k \in \llbracket 0, K-1 \rrbracket$,
- SOC_k, LOH_k are defined $\forall k \in \llbracket 0, K \rrbracket$.

A Providing a constant power profile

The obtained model used to provide a constant power profile as a first proposition for the negotiation is:

$$\begin{aligned}
 & \text{maximize } Pprod \\
 & \text{s.t. :} \\
 & Pprod \leq Pwt_k + Ppv_k + (Pfc_k + Pdch_k)\eta_{inv} \\
 & \quad - (Pez_k + Pch_k)\eta_{inv} \\
 & SOC_k = SOC_{k-1}(1 - \sigma) \\
 & \quad + \frac{Pch_{k-1}\Delta t \times \eta_{ch} - Pdch_{k-1}\Delta t / \eta_{ach}}{Cbat} \\
 & SOC_K = SOC_0 = SOC_{init} \text{ if } K < (T = 24) \\
 & SOC_k = SOC_0 = SOC_{init} \text{ if } K \geq (T = 24) \ \& \ k \% 24 = 0 \\
 & LOH_K \geq LOH_{target_D} \\
 & Pez_k = HHVh_2 \times Qez_k / \eta_{ez} / \Delta t \\
 & Pfc_k = LHVh_2 \times Qfc_k \times \eta_{fc} / \Delta t \\
 & LOH_k = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1} / \eta_{tank} \\
 & Pch_k \leq x_k \times Pchmax \\
 & Pch_k \geq 0 \\
 & Pch_k \leq Pch'_k \\
 & Pch_k \geq Pch'_k - (1 - x_k)Pchmax \\
 & Pdch_k \leq (1 - x_k) \times Pdchmax \\
 & Pdch_k \geq 0 \\
 & Pdch_k \leq Pdch'_k \\
 & Pdch_k \geq Pdch'_k - x_k Pdchmax \\
 & Pez_k \leq Pez'_k \\
 & Pez_k \geq 0 \\
 & Pez_k \leq y_k \times Pezmax \\
 & Pez_k \geq Pez'_k - (1 - y_k)Pezmax \\
 & 0 \leq Pez'_k \leq Pezmax \\
 & Pez_k \geq y_k \times Pezmin \\
 & Qez_k \leq Qez'_k \\
 & Qez_k \geq 0 \\
 & Qez_k \leq z_k \times Qezmax \\
 & Qez_k \geq Qez'_k - (1 - z_k)Qezmax \\
 & 0 \leq Qez'_k \leq Qezmax \\
 & Qfc_k \leq Qfc'_k \\
 & Qfc_k \geq 0 \\
 & Qfc_k \leq (1 - z_k) \times Qfcmax \\
 & Qfc_k \geq Qfc'_k - z_k \times Qfcmax \\
 & 0 \leq Qfc'_k \leq Qfcmax \\
 & 0 \leq u_k + v_k - x_k - y_k \\
 & u_k \leq x_k \\
 & u_k \leq y_k \\
 & 0 \leq 1 - x_k - y_k + u_k \\
 & u_k \geq 0 \\
 & v_k \leq x_k \\
 & v_k \leq z_k \\
 & 0 \leq 1 - x_k - z_k + v_k \\
 & v_k \geq 0
 \end{aligned}$$

$$\begin{aligned}
 & \text{Range of } k & \text{Bounds:} \\
 & \forall k \in \llbracket 0, K-1 \rrbracket & Pfc_k \leq Pfcmax \\
 & \forall k \in \llbracket 0, K-1 \rrbracket & Pez_k \geq Pezmin \\
 & \forall k \in \llbracket 0, K \rrbracket & SOCmin \leq SOC_k \leq SOCmax \\
 & \forall k \in \llbracket 0, K \rrbracket & 0 \leq LOH_k \leq LOHmax \\
 & \forall k \in \llbracket 0, K-1 \rrbracket & Pch_k, Pdch_k, Pez_k, Pch'_k, Pdch'_k, Pez'_k \geq 0 \\
 & \forall k \in \llbracket 0, K-1 \rrbracket & Qez_k, Qfc_k, Qez'_k, Qfc'_k \geq 0 \\
 & \forall k \in \llbracket 0, K-1 \rrbracket & x_k, y_k, z_k, u_k, v_k \in \{0, 1\}
 \end{aligned}$$

B Providing a non constant power profile

The obtained model used to provide a non constant power profile as a proposition for the negotiation is:

$$\begin{aligned}
 & \text{maximize } \sum_{k=0}^{K-1} Pprod_k \\
 \text{s.t. :} & \\
 Pprod_k & \leq Pwt_k + Ppv_k + (Pfc_k + Pdch_k)\eta_{inv} \\
 & \quad - (Pez_k + Pch_k)\eta_{inv} \\
 SOC_k & = SOC_{k-1}(1 - \sigma) \\
 & \quad + \frac{Pch_{k-1}\Delta t \times \eta_{ch} - Pdch_{k-1}\Delta t / \eta_{dch}}{Cbat} \\
 SOC_K & = SOC_0 = SOC_{init} \text{ if } K < (T = 24) \\
 SOC_k & = SOC_0 = SOC_{init} \text{ if } K \geq (T = 24) \ \& \ k \% 24 = 0 \\
 LOH_K & \geq LOH_{target_D} \\
 Pez_k & = HHVh_2 \times Qez_k / \eta_{ez} / \Delta t \\
 Pfc_k & = LHVh_2 \times Qfc_k \times \eta_{fc} / \Delta t \\
 LOH_k & = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1} / \eta_{tank} \\
 Pch_k & \leq x_k \times Pchmax \\
 Pch_k & \geq 0 \\
 Pch_k & \leq Pch'_k \\
 Pch_k & \geq Pch'_k - (1 - x_k)Pchmax \\
 Pdch_k & \leq (1 - x_k) \times Pdchmax \\
 Pdch_k & \geq 0 \\
 Pdch_k & \leq Pdch'_k \\
 Pdch_k & \geq Pdch'_k - x_k Pdchmax \\
 Pez_k & \leq Pez'_k \\
 Pez_k & \geq 0 \\
 Pez_k & \leq y_k \times Pezmax \\
 Pez_k & \geq Pez'_k - (1 - y_k)Pezmax \\
 0 & \leq Pez'_k \leq Pezmax \\
 Pez_k & \geq y_k \times Pezmin \\
 Qez_k & \leq Qez'_k \\
 Qez_k & \geq 0 \\
 Qez_k & \leq z_k \times Qezmax \\
 Qez_k & \geq Qez'_k - (1 - z_k)Qezmax \\
 0 & \leq Qez'_k \leq Qezmax \\
 Qfc_k & \leq Qfc'_k \\
 Qfc_k & \geq 0 \\
 Qfc_k & \leq (1 - z_k) \times Qfcmax \\
 Qfc_k & \geq Qfc'_k - z_k \times Qfcmax \\
 0 & \leq Qfc'_k \leq Qfcmax \\
 0 & \leq u_k + v_k - x_k - y_k \\
 u_k & \leq x_k \\
 u_k & \leq y_k \\
 0 & \leq 1 - x_k - y_k + u_k \\
 u_k & \geq 0 \\
 v_k & \leq x_k \\
 v_k & \leq z_k \\
 0 & \leq 1 - x_k - z_k + v_k \\
 v_k & \geq 0
 \end{aligned}$$

$$\begin{aligned}
 \text{Range of } k & \quad \text{Bounds:} \\
 \forall k \in [0, K - 1] & \quad Pfc_k \leq Pfcmax \\
 \forall k \in [0, K - 1] & \quad Pez_k \geq Pezmin \\
 \forall k \in [0, K] & \quad SOCmin \leq SOC_k \leq SOCmax \\
 \forall k \in [0, K] & \quad 0 \leq LOH_k \leq LOHmax \\
 \forall k \in [0, K - 1] & \quad Pch_k, Pdch_k, Pez_k, Pch'_k, Pdch'_k, Pez'_k \geq 0 \\
 \forall k \in [0, K - 1] & \quad Qez_k, Qfc_k, Qez'_k, Qfc'_k \geq 0 \\
 \forall k \in [0, K - 1] & \quad x_k, y_k, z_k, u_k, v_k \in \{0, 1\}
 \end{aligned}$$

C Matching with a requested profile

The model used to provide a power profile that can match with a profile received from the negotiation is:

$$\begin{aligned}
 & \text{minimize } \alpha \\
 \text{s.t. :} & \\
 Pprod_k & \leq Pre_k \eta_{inv} + (Pfc_k + Pdch_k)\eta_{inv} - (Pez_k + Pch_k)\eta_{inv} \\
 Pre_k & = Pwt_k + Ppv_k \\
 SOC_k & = SOC_{k-1}(1 - \sigma) \\
 & \quad + \frac{Pch_{k-1}\Delta t \times \eta_{ch} - Pdch_{k-1}\Delta t / \eta_{dch}}{Cbat} \\
 SOC_K & = SOC_0 = SOC_{init} \text{ if } K < (T = 24) \\
 SOC_k & = SOC_0 = SOC_{init} \text{ if } K \geq (T = 24) \ \& \ k \% 24 = 0 \\
 Pprod_k & \geq (1 - \alpha) \times Pload_k \\
 Pez_k & = HHVh_2 \times Qez_k / \eta_{ez} / \Delta t \\
 Pfc_k & = LHVh_2 \times Qfc_k \times \eta_{fc} / \Delta t \\
 LOH_k & = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1} / \eta_{tank} \\
 LOH_K & \geq LOH_{target_D} \\
 Pch_k & \leq x_k \times Pchmax \\
 Pch_k & \geq 0 \\
 Pch_k & \leq Pch'_k \\
 Pch_k & \geq Pch'_k - (1 - x_k)Pchmax \\
 Pdch_k & \leq (1 - x_k) \times Pdchmax \\
 Pdch_k & \geq 0 \\
 Pdch_k & \leq Pdch'_k \\
 Pdch_k & \geq Pdch'_k - x_k Pdchmax \\
 Pez_k & \leq Pez'_k \\
 Pez_k & \geq 0 \\
 Pez_k & \leq y_k \times Pezmax \\
 Pez_k & \geq Pez'_k - (1 - y_k)Pezmax \\
 0 & \leq Pez'_k \leq Pezmax \\
 Pez_k & \geq y_k \times Pezmin \\
 Qez_k & \leq Qez'_k \\
 Qez_k & \geq 0 \\
 Qez_k & \leq z_k \times Qezmax \\
 Qez_k & \geq Qez'_k - (1 - z_k)Qezmax \\
 0 & \leq Qez'_k \leq Qezmax \\
 Qfc_k & \leq Qfc'_k \\
 Qfc_k & \geq 0 \\
 Qfc_k & \leq (1 - z_k) \times Qfcmax \\
 Qfc_k & \geq Qfc'_k - z_k \times Qfcmax \\
 0 & \leq Qfc'_k \leq Qfcmax \\
 0 & \leq u_k + v_k - x_k - y_k \\
 u_k & \leq x_k \\
 u_k & \leq y_k \\
 0 & \leq 1 - x_k - y_k + u_k \\
 u_k & \geq 0 \\
 v_k & \leq x_k \\
 v_k & \leq z_k \\
 0 & \leq 1 - x_k - z_k + v_k \\
 v_k & \geq 0
 \end{aligned}$$

$$\begin{aligned}
 \text{Range of } k & \quad \text{Bounds:} \\
 \forall k \in [0, K - 1] & \quad Pfc_k \leq Pfcmax \\
 \forall k \in [0, K - 1] & \quad Pez_k \geq Pezmin \\
 \forall k \in [0, K] & \quad SOCmin \leq SOC_k \leq SOCmax \\
 \forall k \in [0, K] & \quad 0 \leq LOH_k \leq LOHmax \\
 \forall k \in [0, K - 1] & \quad Pch_k, Pdch_k, Pez_k, Pch'_k, Pdch'_k, Pez'_k \geq 0 \\
 \forall k \in [0, K - 1] & \quad Qez_k, Qfc_k, Qez'_k, Qfc'_k \geq 0 \\
 \forall k \in [0, K - 1] & \quad x_k, y_k, z_k, u_k, v_k \in \{0, 1\}
 \end{aligned}$$

D Source commitment

The obtained model used for the source commitment is defined as follow:

$$\left\{ \begin{array}{l}
 \text{maximize } LOH_K \\
 \text{s.t. :} \\
 Pprod_k = Pwt_k + Ppv_k + (Pfc_k + Pdch_k)\eta_{inv} - (Pez_k + Pch_k)\eta_{inv} \\
 Pload_k \leq Pprod_k \\
 SOC_k = SOC_{k-1}(1 - \sigma) \\
 \quad + \frac{Pch_{k-1}\Delta t \times \eta_{ch} - Pdch_{k-1}\Delta t/\eta_{dch}}{Cbat} \\
 SOC_K = SOC_0 = SOC_{init} \text{ if } K < (T = 24) \\
 SOC_k = SOC_0 = SOC_{init} \text{ if } K \geq (T = 24) \ \& \ k\%24 = 0 \\
 Pez_k = HHVh_2 \times Qez_k/\eta_{ez}/\Delta t \\
 Pfc_k = LHVh_2 \times Qfc_k \times \eta_{fc}/\Delta t \\
 LOH_k = LOH_{k-1} + Qez_{k-1} - Qfc_{k-1}/\eta_{tank} \\
 Pch_k \leq x_k \times Pchmax \\
 Pch_k \geq 0 \\
 Pch_k \leq Pch'_k \\
 Pch_k \geq Pch'_k - (1 - x_k)Pchmax \\
 Pdch_k \leq (1 - x_k) \times Pdchmax \\
 Pdch_k \geq 0 \\
 Pdch_k \leq Pdch'_k \\
 Pdch_k \geq Pdch'_k - x_k Pdchmax \\
 Pez_k \leq Pez'_k \\
 Pez_k \geq 0 \\
 Pez_k \leq y_k \times Pezmax \\
 Pez_k \geq Pez'_k - (1 - y_k)Pezmax \\
 0 \leq Pez'_k \leq Pezmax \\
 Pez_k \geq y_k \times Pezmin \\
 Qez_k \leq Qez'_k \\
 Qez_k \geq 0 \\
 Qez_k \leq z_k \times Qezmax \\
 Qez_k \geq Qez'_k - (1 - z_k)Qezmax \\
 0 \leq Qez'_k \leq Qezmax \\
 Qfc_k \leq Qfc'_k \\
 Qfc_k \geq 0 \\
 Qfc_k \leq (1 - z_k) \times Qfcmax \\
 Qfc_k \geq Qfc'_k - z_k \times Qfcmax \\
 0 \leq Qfc'_k \leq Qfcmax \\
 0 \leq u_k + v_k - x_k - y_k \\
 u_k \leq x_k \\
 u_k \leq y_k \\
 0 \leq 1 - x_k - y_k + u_k \\
 u_k \geq 0 \\
 v_k \leq x_k \\
 v_k \leq z_k \\
 0 \leq 1 - x_k - z_k + v_k \\
 v_k \geq 0
 \end{array} \right.$$

$$\left\{ \begin{array}{ll}
 \text{Range of } k & \text{Bounds:} \\
 \forall k \in [0, K - 1] & Pfc_k \leq Pfcmax \\
 \forall k \in [0, K - 1] & Pez_k \geq Pezmin \\
 \forall k \in [0, K] & SOCmin \leq SOC_k \leq SOCmax \\
 \forall k \in [0, K] & 0 \leq LOH_k \leq LOHmax \\
 \forall k \in [0, K - 1] & Pch_k, Pdch_k, Pez_k, Pch'_k, Pdch'_k, Pez'_k \geq 0 \\
 \forall k \in [0, K - 1] & Qez_k, Qfc_k, Qez'_k, Qfc'_k \geq 0 \\
 \forall k \in [0, K - 1] & x_k, y_k, z_k, u_k, v_k \in \{0, 1\}
 \end{array} \right.$$