

1 Caustics of the Axially Symmetric Vortex 2 Beams: Analysis and Engineering

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9 **Abstract:** We demonstrate that our theoretical scheme developed in the previous study on the
10 caustics of the abruptly autofocusing vortex beams [Xiao *et al.*, Opt. Express **29** (13): 19975
11 (2021)] is universal for all the *axially symmetric vortex beams*. Further analyses based on this
12 method show the complex compositions of the vortex caustics in real space. Fine features of
13 the global caustics are well reproduced, including their deviations from the trajectories of the
14 host beams. Besides, we also show the possibility of tailoring the vortex caustics in paraxial
15 optics based on our theory. The excellent agreements of our theoretical results with both
16 numerical and experimental results confirm the validity of this scheme.

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19 1. Introduction

20 Vortex beams are structured light fields with doughnut-shaped spatial profiles and phase
21 singularities. Their distinctive feature is the presence of the helical phase fronts described as
22 $\exp(i l \theta)$, where l is the so-called topological charge and θ is the azimuthal angle [1]. Among
23 the vortex beams, the spiral vortex beams are shown to be strong in terms of the structural
24 stability [2,3]. Due to these notable properties, vortex beams have attracted widespread interests
25 and play critical roles in various applications, like particle micromanipulation [4,5], microscopy
26 [6], material processing [7-9], and optical communication [10,11]. By superimposing the
27 helical phase on the axially symmetric phases of different host beams like the Gaussian beam,
28 the Bessel beam and the abruptly autofocusing beam, a series of axially symmetric vortex
29 beams (ASVBs) are investigated [12-15]. In this way, vortex beams can be adapted with diverse
30 intensity tubes in focusing, diverging and non-diffracting shapes.

31 Two major schemes are basically implemented to interpret and engineer the light fields.
32 The integral-based scheme is the mostly-used method, involving with the diffraction integral
33 using the stationary phase method [16-19]. In some cases, the use of this method induces
34 “singular points” whose intensity tends to infinity [20]. Various asymptotic methods have also
35 been discussed to analyze the field around the irremovable singular points [20-23]. As the
36 approximation is indispensable to simplify the diffraction integral, error estimates as well as
37 complex algebra are required. In parallel, the differentiation-based scheme is also developed in
38 the realm of the geometric optics. In this scheme, vortex light fields can be decomposed into
39 families of rays emerging from any cross-section along propagation [24,25]. And the envelope
40 of the ensemble of rays constitutes the framework of the caustics [24, 26]. In this way, a
41 relatively simple and efficient method without further approximation is available to interpret
42 the caustics of ASVBs and to predict the focusing properties in real space [27]. However, some
43 clarifications of the compositions of caustics in real space have not been discussed. In addition,
44 for applications like microscopy, laser ablation and fabrication of two-photon polymerization,
45 tailoring the caustics have also been an increasing interest in recent years [28-32]. With a

46 comprehensive understanding of the caustics, engineering the caustics of the ASVBs is also an
 47 issue of fundamental importance in applications.

48 In this paper, we show a developed approach to classify the caustics of different ASVBs. In
 49 Section 2, we firstly introduce the theoretical results as a set of concise expressions developed
 50 for reproducing the caustics of the ASVBs. Comparing with the existing results, these
 51 expressions are obtained without any mathematical approximation. Then, the third Section
 52 compares our theories with the numerical simulations and the experimental results for several
 53 exemplary beams, illustrating the geometries of the vortex caustics. In particular, finer features
 54 can be well outlined in more intuitive physical images as shown in the discussion of the Bessel
 55 vortex beam and the abruptly autofocusing vortex beam, which are absent in previous studies.
 56 Furthermore, we also developed a method to engineer vortex beams with tailored novel tubular
 57 caustics based on our results. Our theoretical results are in excellent agreement with both
 58 numerical simulations and experimental results.

59 2. The caustics of the ASVBs

60 2.1 Analytical results

61 From a given *axially symmetric* host beam with the phase profile $\phi_{\text{host}}(r)$, the vortex version
 62 can be synthesized by combining the spiral phase $\phi_{\text{vortex}}(\theta) = l\theta$ with $\phi_{\text{host}}(r)$ in any cross-
 63 section along propagation [27]:

$$64 \quad \phi(r, \theta) = \phi_{\text{host}}(r) + \phi_{\text{vortex}}(\theta) = \phi_{\text{host}}(r) + l\theta \quad (1)$$

65 In geometrical optics, the corresponding radial components of the k vector can be defined as
 66 $k \cdot \sin \gamma(r) \equiv -\partial \phi(r, \theta) / \partial r = -\partial \phi_{\text{host}} / \partial r$, where $k = 2\pi/\lambda$ is the wave number depending on the
 67 wavelength λ [27]. Note that this angle is only related to the host beam. With the parameters N
 68 and V defined as:

$$69 \quad \begin{aligned} N(r) &= \sqrt{\sin^2 \gamma + l^2 / (kr)^2} \\ V(r) &= \sqrt{N^2 - 1} \end{aligned} \quad (2)$$

70 we found that the rays emerging from the ring of a specific radius r in the initial transverse
 71 plane $z = 0$ lie on the hyperboloid [Fig. 1(a)] specified as:

$$72 \quad \begin{aligned} \frac{\rho^2}{R^2} - \frac{(z - z_w)^2}{L^2} &= 1 \quad \rho^2 = x^2 + y^2 \\ R &= \frac{|l|/k}{N}, \quad L = RV, \quad z_w = \frac{V}{N} \sqrt{r^2 N^2 - \frac{l^2}{k^2}} \end{aligned} \quad (3)$$

73 where R , L and z_w are all dependent on r for a given topological charge l . Moreover, the whole
 74 light field can be represented in geometrical optics as the superposition of ray families lying on
 75 different hyperboloids [Fig. 1(b)], leading to their envelope defined as the caustic of the
 76 synthesized vortex beam from the host field. Here we postulate the existence of the caustic, and
 77 we found that the z positions of the *constituent* points on the caustic (or the *characteristic* points
 78 in [27]) are simply the solutions to the equation:

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$$A(z - z_w)^2 + B(z - z_w) + C = 0$$

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$$A = (LVN)^{-2} \frac{R'}{R}, \quad B = \frac{z_w'}{L^2}, \quad C = -\frac{R'}{R} \quad (4)$$

$$\Delta \equiv \sqrt{B^2 - 4AC}$$

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where the prime denotes a derivative with r . Since the Eq. (4) is quadratic, there are two sets of constituent points $(\rho(z_1), z_1)$ and $(\rho(z_2), z_2)$ for each given parameter r :

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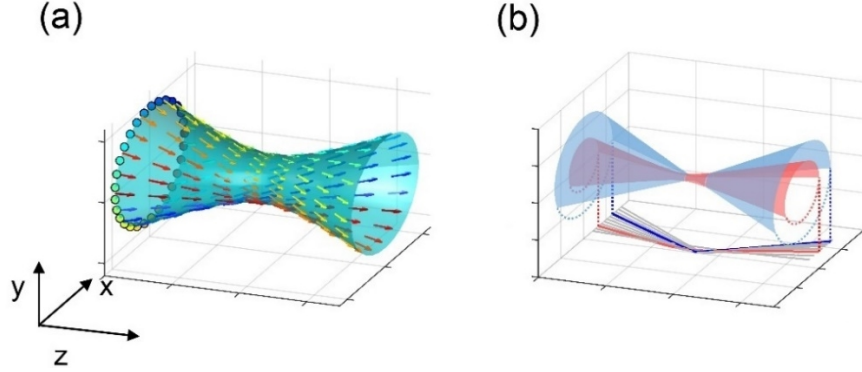
$$z_1 = z_w - \frac{B - \Delta}{2A}$$

$$z_2 = z_w - \frac{B + \Delta}{2A} \quad (5)$$

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Note that the host phase $\phi_{\text{host}}(r)$ is represented by the specific distribution of $\sin \gamma(r)$ through differentiation. And the introduction of the parameters N and V in Eq. (2) can further facilitate the understanding on the geometrical image of the vortex beams. One can easily calculate the complex caustic by substituting (N, V) of a specific host phase into Eqs. (3) - (5). Since no integral is involved in this procedure, our differentiation-based method is very friendly to implement without further approximations.

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Fig. 1. Schematics of the axially symmetric vortex beams (ASVBs) in geometrical optics: (a) a single hyperboloid formed by rays emerging from a specific ring in the transverse plane $z=0$; (b) Two different hyperboloids formed by the corresponding families of rays from the plane $z=0$ (the blue and red half tubes), with their intersections with $y=0$ plane (blue and red solid curves) projected into the bottom plane. The intersections between other hyperboloids and $y=0$ plane are also superimposed (gray solid curves). The whole beam propagates in the z direction.

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2.2 Discussions on the topology of the caustics

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In this work, we focus on the caustics in *real* space of an optical setup ($z > 0$) since the beam is usually generated in such ways. In general, the constituent points of the global caustics of the ASVBs can be rather complex: either a single set of $\{z_1\}$ (or $\{z_2\}$) or both sets of $\{z_1\}$ and $\{z_2\}$ can get involved in constituting the caustic in real space (as will be shown in Section 3.2). After some algebra, we find that the expression below can well distinguish the above two general cases in terms of z_w :

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$$\text{Both sets: } z_w > \frac{B + \Delta \cdot \text{sgn}(R')}{2A}, \quad z_1 > 0, z_2 > 0 \quad (6)$$

$$\text{Single set: } z_w < \frac{B + \Delta \cdot \text{sgn}(R')}{2A}, \quad z_2 < 0 < z_1 \text{ (or } z_1 < 0 < z_2)$$

105 where $\text{sgn}(R')$ is the sign function. Besides, the relative locations of z_1 and z_2 for a specific host
106 beam are determined by R' . More details of the cases are summarized in Table 1.

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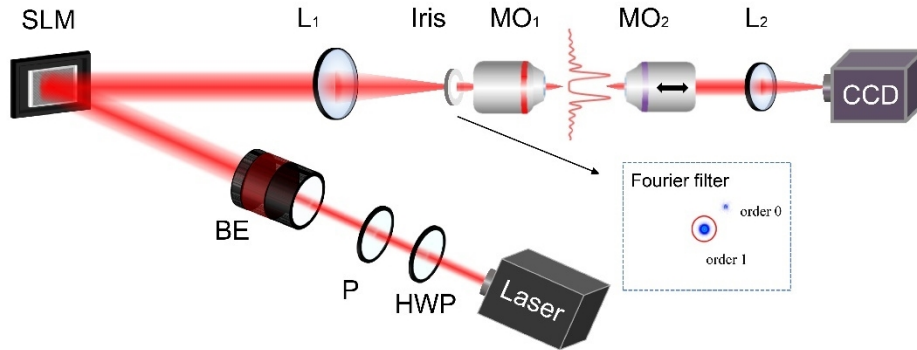
Table 1. Constituent points in real space ($z > 0$)

No. of solution sets	Two sets: $\{z_1\}$ and $\{z_2\}$	A single set: $\{z_1\}$ (or $\{z_2\}$)
Sign of R'		
+	$0 < z_2 < z_1$	$z_2 < 0 < z_1$
-	$0 < z_1 < z_2$	$z_1 < 0 < z_2$

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110 3. Numerical and experimental demonstration of the caustics of different 111 ASBVs

112 3.1 Setup



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Fig. 2. Schematic of the experimental setup. HWP: half-wave plate; P: polarizer; BE: beam expander; SLM: spatial light modulator; L: lenses; MO1 and MO2: microscope objectives.

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We use the same setup as in [27] to demonstrate our analytical results in section 2. As shown in Fig. 2, the Gaussian beam centered at 1065nm from a home-made ultrafast fiber laser is firstly injected into a beam expander. The output collimated beam with an expanded width of ~8mm is then incident upon a phase-only spatial light modulator (Holoeye SLM-Pluto, 1920×1080 pixels). The exposed power is controlled by adjusting the half-wave plate before a polarizer. With the phases of the synthesized vortex beams in Table 2 encoded on the SLM together with an additional grating phase, ASBVs can be generated right after SLM in the first order. Then a telescope is used to shrink the ASBVs down to the micron-scale. The telescope is built with a lens (focal length = 1m) and a microscope objective (50×, NA = 0.8). An iris is installed close to MO₁ to block the undesired orders, retaining the first order of the diffraction lights as shown in the inset of Fig. 2. An imaging system made of another identical microscope objective (MO₂) followed by a lens (focal length = 0.5m) is used to capture the intensity profiles at each z position along beam propagation. The 2D side views of the intensity profiles are then

129 extracted from the stacked data. Careful alignments only introduce weak perturbation in the
 130 setup. This guarantees that the vortex beams appear with negligible deviation from the ideal
 131 caustics.
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133 3.2 Experimental demonstrations

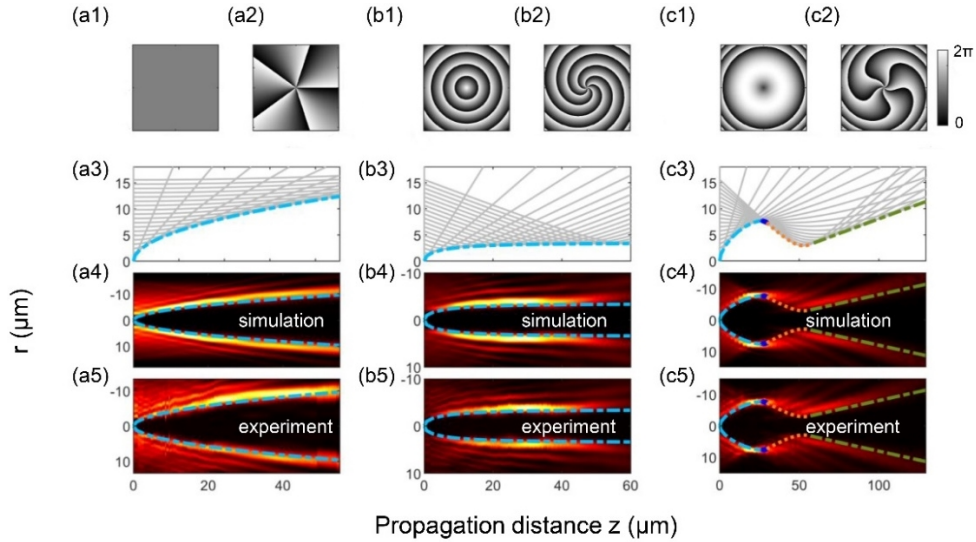
134 In our previous study on vortex beams hosted by the abruptly autofocusing beams [27], it is
 135 proved that the caustics of their central tube can be well described by the set of constituent
 136 points determined by Eq. (3)-(5). To further demonstrate the universality of our formulae for
 137 the whole family of axially symmetric vortex beams (ASVBs), vortex beams with four
 138 additional host beams, such as Gaussian beams, Bessel beams, Bessel-like beams [33] and
 139 parabolic toroidal lens beams [34] are generated in this work. Table 2 lists their phases and the
 140 corresponding $\sin \gamma(r)$.

141 **Table 2. Phases of four vortex beams synthesized from specific host beams**

Specific ASVBs	Applied phase and their $\sin \gamma(r)$: caustics of two simplest cases are given in the parentheses
Gaussian vortex beam	$\phi(r, \theta) = l\theta$ $\sin \gamma(r) = 0 \quad \left(z = \frac{\rho^2 - (l/k)^2}{2 l/k } \right)$
Bessel vortex beam	$\phi(r, \theta) = -k \sin \gamma \cdot r + l\theta$ $\sin \gamma(r) = \text{constant} \quad \left(z = \frac{\rho^2 \sin \gamma}{ l/k } \sqrt{\frac{\rho^2 - (l/k)^2}{(l/k)^2 - \rho^2 \sin^2 \gamma}} \right)$
Bessel-like vortex beam [33]	$\phi(r, \theta) = -k(ar^n + br^m) + l\theta$ $\sin \gamma(r) = nar^{n-1} + mbr^{m-1}$
Parabolic vortex toroidal lens [34]	$\phi(r, \theta) = -k(r^2 - 2r_0 r)/2f + l\theta$ $\sin \gamma(r) \equiv (r - r_0)/f$

142 According to section 2, the caustics of the ASVBs with a given topological charge l are only
 143 related to the corresponding host phases. Without loss of generality, the topological charge l is
 144 chosen to be $l = 5$ for this section. Based on the angular spectrum method [35], we also
 145 numerically simulate different ASVBs with parameters corresponding to the setup in Fig. 2.
 146 The simulated and experimental results are shown in Fig. 3, where the measured 2D intensity
 147 profiles are extracted from the 3D data acquired with our setup. For Gaussian vortex beams,
 148 the phase of the host Gaussian beam as well as the corresponding total phase of the ASVB are
 149 shown in Fig. 3(a1) - (a2). The flat phase of the host Gaussian beam results in $z_w = 0$ and $B = 0$
 150 for any r , which gives $z_2 = -z_1$ with $z_1 > 0$. According to Table 1, the caustic in real space is
 151 determined only by the single set of z_1 , shown by the blue dash-dotted line in Fig. 3(a3) - (a5).
 152 In the second example, the phases of the host Bessel beam with $\sin \gamma(r) \equiv 8.87 \times 10^{-4}$ and the
 153 corresponding vortex beam are shown in Fig. 3(b1) - (b2). As Bessel vortex beam determines
 154 that $R'(r) > 0$ and $z_w < (B + \Delta)/2A$, the sign of z_1 and z_2 can be solved as $z_1 > 0$ and $z_2 < 0$. In this
 155 way, the caustic in real space is also determined by the single set of z_1 as shown in Fig. 3(b3) -
 156 (b5) with the blue dash-dotted line. Besides, the set of $(\rho(z_1), z_1)$ can be well approximated by
 157 the set of $(R(r), z_w(r))$ for Bessel vortex beams. Comparing with the cylindrical caustic expected
 158 for Bessel vortex beams [23], our solution in Table 2 can well outline the finer features of the
 159 transitionally-expanding tube caustic as shown in [25]. The cylindrical caustic is the special
 160 case where the approximation $l/(kr) \ll \sin \gamma$ is applied in the expression $R(r)$ in Eq. (3). We
 161 stress here that the analytical results in this paper also address the puzzling correspondence
 162 between the ensemble of the hyperboloidal waists and the central tube caustics of Bessel vortex
 163 beams in our previous study [25].

164 A family of perfect optical vortices (POVs) are recently designed by integrating the spiral
165 phase into the phase of the parabolic toroidal lens [34]. This POV with a large range of
166 topological charge l has a quasi-static focal ring radius r_0 at a focal length f . The set of equations
167 determining the caustics of these beams are too complex in [34], resulting in analytical
168 estimates in two special cases. Since our analytical results are deduced for any axially
169 symmetric vortex beam without any further estimate, we also generate one of such beams to
170 demonstrate the validity of our method. The corresponding beam parameters after the telescope
171 in Table 2 are selected as $f = 30\mu\text{m}$ and $r_0 = 7\mu\text{m}$. After some algebra, we found the caustic of
172 this specific POV can be decomposed into multiple sections. When a given r is small enough
173 that $z_w(r) < [B + \Delta \cdot \text{sgn}(R')] / 2A$ and $R' > 0$, the single set of $z_l(r)$ define the most front section of
174 the caustic [the blue dash-dotted line in Fig. 3(c3)–(c5)]. As r grows until $z_w(r) > [B + \Delta \cdot \text{sgn}(R')] / 2A$,
175 both the solution sets in Eq. (5) are involved in forming the caustic: $\{(\rho(z_1), z_1(r))\}$ define
176 a tiny part of the caustic very close to the original focal plane of the host beam [dark blue lines
177 in Fig. 3(c3)–(c5)]; $\{(\rho(z_2), z_2(r))\}$ determine the long opening tube behind, as shown by the
178 green dash-dotted line in Fig. 3(c3)–(c5). The intermediate caustic section [orange dots] in the
179 range of $[z_1(r_{\max}), z_2(r_{\max})]$ between the short dark blue line and the green line is composed by
180 part of the hyperboloid formed by the rays emerging from the edge of the effective aperture.
181 Besides, when the vortex order is increased, the section $\{(\rho(z_1), z_1(r))\}$ before the focus remains
182 quasi-static and the section $\{(\rho(z_2), z_2(r))\}$ after the focus is shorter. In short, the complex global
183 caustics can be well analyzed with our method. Our analytical results are in excellent agreement
184 with both numerical simulation and experimental results.

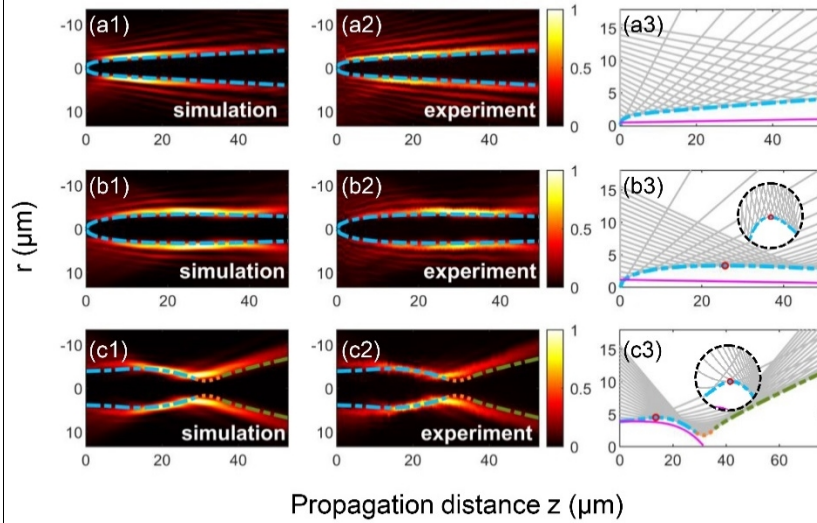


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Fig. 3. The results of different ASVBs with topological charge $l = 5$. (1)-(2): The phases of the host beams and the corresponding ASVBs. (3)-(5): The theoretical, numerical and experimental results for (a) Gaussian vortex beam, (b) Bessel vortex beam and (c) perfect optical vortex beam generated by parabolic vortex toroidal lens. Light blue dash-dot lines together with dark blue short lines represent the caustic defined by $(\rho(z_1), z_1)$. Green dash-dot lines represent the caustic defined by $(\rho(z_2), z_2)$. Orange dot lines represent part of the caustic formed by part of the hyperboloidal surface between $(\rho(z_1), z_1)$ and $(\rho(z_2), z_2)$ occurred in the perfect optical vortex.

193 In addition, our results can well reproduce the deviation of the propagating behavior of the
194 synthesized vortex beam from that of the corresponding host beam with specific parameters.
195 The topological charge l is also chosen to be $l = 5$. Here, we firstly selected the Bessel-like
196 beam in [33], *i.e.* a family of shape invariant beams, as the host beam. For specific Bessel-like
197 beams with a linearly ramped central lobe along propagation, the parameters are selected as n
198 $= 2, m = 1$ in Table 2. As for the Bessel-like beams featuring the linearly diverging central lobe,

199 the parameters are chosen as $a = -0.17 \text{ m}^{-1}$, $b = 0.0018$. With $R' > 0$ and $z_w < (B+\Delta)/2A$, z_2 is
200 negative. Therefore, the global caustic is also defined by the single set of z_1 , shown as the blue
201 dash-dot lines in Fig. 4(a). For comparison, the central lobe profile of the Bessel-like beam
202 without the spiral phase is superimposed as the purple line in Fig. 4(a3). It is evident that the
203 spiral phase further accelerates the divergence along propagation. In the second Bessel-like
204 beam [shown in Fig. 4(b)], we select the parameters as $a = 0.056 \text{ m}^{-1}$ and $b = 0.0006$ without
205 changing n and m . Instead, this Bessel-like host beam has a linearly-tapered central lobe along
206 propagation, presented by the purple line in Fig. 4(b3). Interestingly, the corresponding ASVB
207 has an extremum on the ring caustic [shown by the single red circle in Fig. 4(b3)] determined
208 by $R'(r_{\text{extrema}}) = 0$. This behavior is totally different from the monotonous tapering of central
209 lobe in the host beam along propagation. In fact, this deviation was also observed in our early
210 work on abruptly autofocusing vortex (AAFV) beams hosted by the polynomial phase [27]. For
211 such AAFV beams with specific parameters (for instance, $n = 4$, $a = 0.3 \times 10^{-4} \text{ m}^{-3}$ and $r_0 = 1.08$
212 mm as in [27]), the sets of z_1 and z_2 are both involved in constituting the global caustics. Besides
213 the significant deviation of the vortex caustics from the host polynomial trajectories [shown by
214 the purple line in Fig. 4(c3)], the introduction of the spiral phase into the host beam also brings
215 the interesting feature: once the local maximum in the waist distribution $R(r)$ exists, an
216 extremum occurs accordingly on the global caustic despite of the original trajectory of the host
217 beam as shown in Fig. 4. In short, the analyses based on our method can exactly reproduce the
218 fine features of the caustic shape. This further demonstrates the validity of our analytical results,
219 serving as a powerful tool for analyzing the vortex beams.



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Fig. 4. Propagating behavior deviation of the ASVBs ($l = 5$) from their host beams. Bessel-like vortex beam with parameters: (a) $a = -0.17 \text{ m}^{-1}$, $b = 0.0018$ and (b) $a = 0.056 \text{ m}^{-1}$, $b = 0.0006$; (c) Abruptly autofocusing vortex beams with: $n = 4$, $a = 0.3 \times 10^{-4} \text{ m}^{-3}$ and $r_0 = 1.08$ mm. Purple lines in (a3) and (b3) show the central lobe size of the host Bessel-like beam without the spiral phase, and the purple line in (c3) represents the host polynomial trajectory. Blue dash-dot lines represent the caustic defined by $(\rho(z_1), z_1)$ and green dash-dot lines represent the caustic defined by $(\rho(z_2), z_2)$. Orange dot lines in (c1) - (c3) represent part of the caustic formed by part of the hyperboloidal surface between $(\rho(z_1), z_1)$ and $(\rho(z_2), z_2)$ like the perfect optical vortex. Insets of (b3) and (c3) show zoomed extrema points.

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4. Engineering the caustics of the ASVBs in the paraxial optics

Previous sections show how to calculate the caustics of the ASVBs from their phases $\phi(r, \theta)$. With the help of the caustic expressions, we also demonstrate that the propagation behavior of

233 the ASVBs can deviate significantly from that of the corresponding host beams due to the spiral
 234 phase. Therefore, a challenge arises here that the host beams cannot always well *predict* the
 235 tube shape of their vortex “brother” beams.

236 In fact, the inverse problem of *tailoring* the caustic by an engineered host phase is more
 237 interesting. The target profile $\rho(z) = c(z)$ can be engineered by solving the host phase $\phi_{\text{host}}(r)$
 238 from $z_{\text{caustic}}(r) = c^{-1}(z)$ based on Eq. (4) and (5). However, this usually involves a mathematical
 239 challenge. Here, we clarify a fundamental limit and show the possibility of tailoring the tube
 240 shape based on our results with two preconditions. Since travelling waves are generated in
 241 numerous applications, this leads to a fundamental requirement that the topological charge l
 242 should not be very large within the radial contents of the beam, i.e. $|l| \leq kr |\cos \gamma(r)|$. In practice,
 243 paraxial optics are adopted in most cases, requiring that $\tan \gamma(r) \approx \sin \gamma(r)$. If we further focus
 244 on the ASVBs with the azimuthal components of k vector much smaller than the corresponding
 245 radial components, we found $r \gg |l / \phi'(r, \theta)|$ and $\sin^2 \gamma(r) + [l / (kr)]^2 \approx \sin^2 \gamma(r)$. With these
 246 preconditions implemented in Eqs. (4) and (5), the tubular caustic can be well approximated
 247 as:

$$248 \quad z \approx r / \tan \gamma \approx r / \sin \gamma = -kr / \phi'_{\text{host}}(r) \quad (7)$$

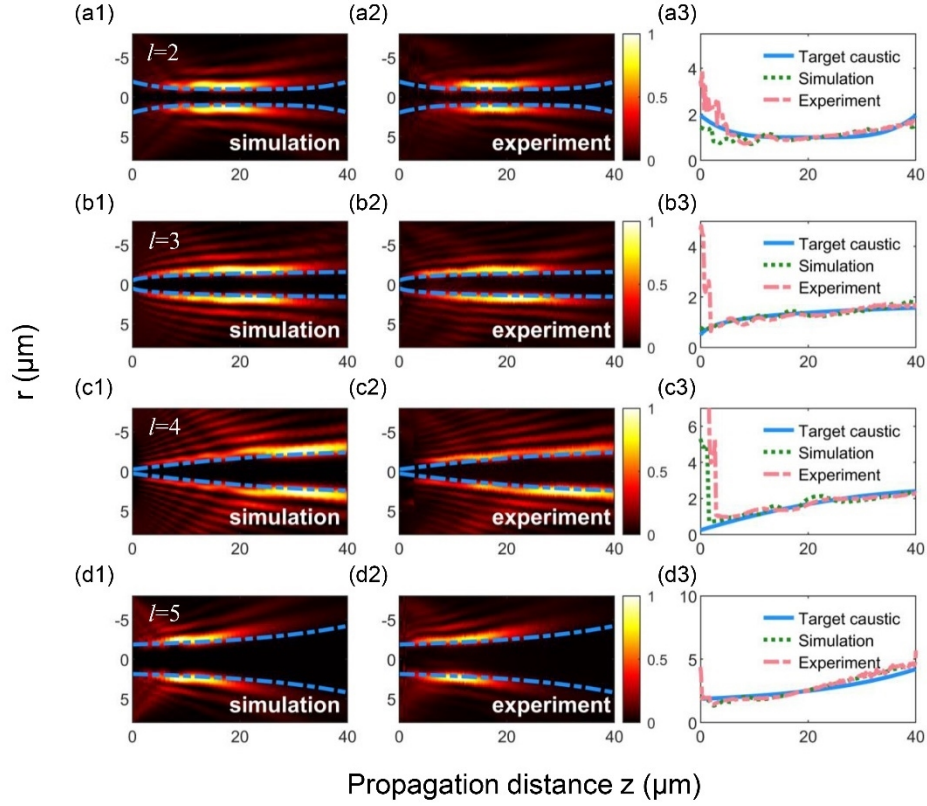
$$\rho = -|l| / \phi'_{\text{host}}(r)$$

249 The $\phi_{\text{host}}(r)$ can be solved by substituting the target caustic profiles $\rho(z) = c(z)$ into Eq. (7) with
 250 the help of the computer. To demonstrate the validity of our method, several exemplary ASVBs
 251 with tailored tubular profiles after the telescope can be generated in our setup. The target
 252 profiles and the specific parameters of these beams are listed in Table 3. All the measured
 253 caustics present excellent agreements with the corresponding tailored profiles as shown in Fig.
 254 5.

255 **Table 3. Target profiles $\rho(z) = c(z)$ of different shapes**

Types of profiles	The target profiles and parameters after the telescope
Quartic	$\rho(z) = a(z - z_0)^4 + b$ $a = 6 \times 10^{12} \text{ m}^{-3}, \quad z_0 = 20 \mu\text{m}, \quad b = 1 \mu\text{m}$
Logarithmic	$\rho(z) = a \log_2(z + b) + c$ $a = 0.2, \quad b = 1 \mu\text{m}, \quad c = 0.5 \mu\text{m}$
Parabolic	$\rho(z) = a(z - z_0)^2 + b$ $a = -9 \times 10^2 \text{ m}^{-1}, \quad z_0 = 50 \mu\text{m}, \quad b = 2.5 \mu\text{m}$
Exponential	$\rho(z) = a \exp[b(z - z_0)] + c$ $a = 1, \quad z_0 = 20 \mu\text{m}, \quad b = 5 \times 10^4 \text{ m}^{-1}, \quad c = 1.5 \mu\text{m}$

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Fig. 5. Synthesized vortex beams of different vortex orders with: (a) quartic, (b) logarithmic, (c) parabolic and (d) exponential tubular profiles and tailored parameters listed in Table 3. The blue dash dotted lines s represent the pre-engineered target caustics. The caustic profiles extracted from the simulation and experiments shown in the third column are all defined as in [27].

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In addition, two exemplary ASVBs with $l = 6$ are pre-engineered and shown in Fig. 6, presenting one beam carrying an opening central tube profile $\rho(z) = a + bz$ with $a = 2\mu\text{m}$, $b = 0.058$ [Fig. 6(a)] and the other with a tapered central tube profile $\rho(z) = a - bz$ with $a = 5\mu\text{m}$, $b = 0.058$ [Fig. 6(b)]. By inserting Eq. (7) into the above target tube profiles, the engineered phase can be readily obtained as $\phi_{\text{host}}(r) = -(l/a)r \pm r^2bk/(2a)$. The blue solid lines represent the pre-determined caustics $\rho(z)$. Fig. 6(a3) and Fig. 6(b3) also present the simulated and measured tube profiles. The discrepancies from the target tapered profile in Fig. 6(b) mainly originate from the limited active aperture on the SLM ($8.64\text{mm} \times 8.64\text{mm}$). This is proved by simulating the same beam with SLMs of different areas, where the larger active area ($12\text{mm} \times 12\text{mm}$) allows a better agreement with the predefined geometry [Fig. 6(b5)]. Despite that such a large SLM is unavailable in our experiment, this distortion can be corrected in tailored caustics with a smaller initial ring and a less steep taper ($a = 4\mu\text{m}$, $b = 0.038$) as shown in Fig. 6(c).

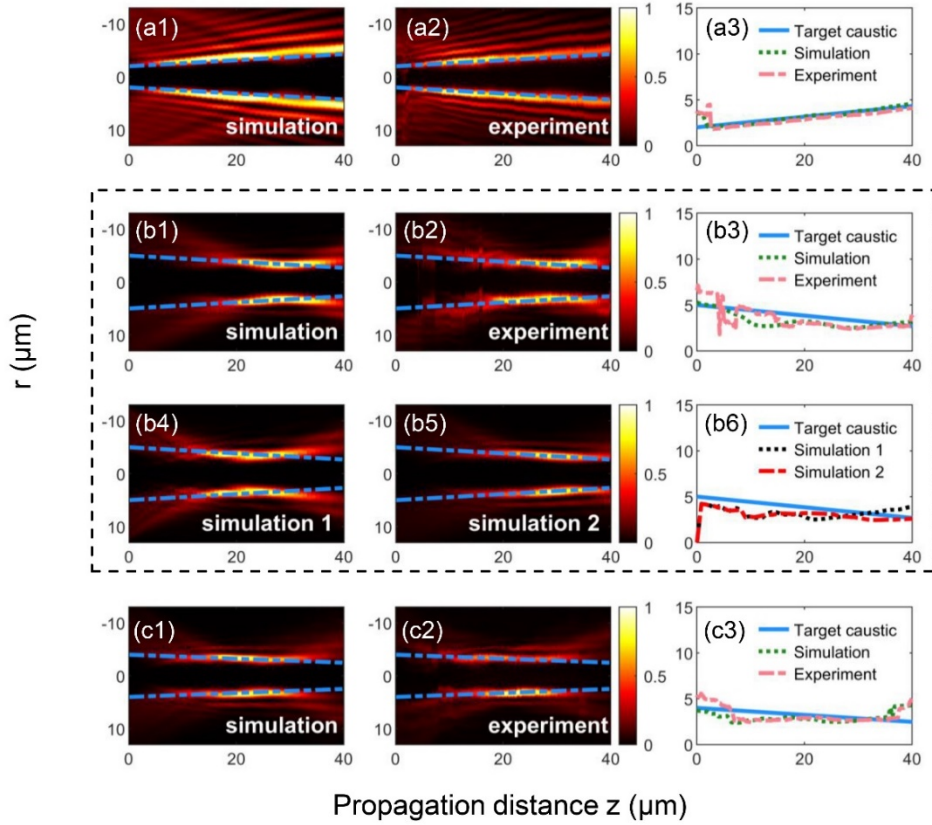


Fig. 6. Numerical simulations and experimental results of several particular examples with the tunable hollow core radius. (a) $\rho = a + bz$ with $a = 2\mu\text{m}$, $b = 0.058$; (b) $\rho = a - bz$ with $a = 5\mu\text{m}$, $b = 0.058$ and (c) $\rho = a - bz$ with $a = 4\mu\text{m}$, $b = 0.038$. SLMs with a smaller ($7\text{mm} \times 7\text{mm}$) and a larger ($12\text{mm} \times 12\text{mm}$) area are adopted in the simulation in (b4) and (b5), respectively. The blue dash dotted lines represent the pre-engineered target caustics. The caustic profiles extracted from the simulation and experiments shown in the third column are all defined as in [27].

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282 5. Conclusion

283 In this paper, we demonstrate that the set of analytical equations developed in our previous
284 study on the caustics of the abruptly autofocusing vortex beams [27] have a wider universality
285 to well reproduce the caustics of the axially symmetric vortex beams. Based on a couple of
286 vortex beams synthesized from different host beams, the universality is proved by the excellent
287 agreements of our theory with the numerical and experimental results. Features of the vortex
288 caustics can also be well addressed with our theoretical methods, including the components of
289 the global caustics and the deviation of the vortex caustics from the host caustics. Besides, we
290 have also shown that it is possible to pre-engineer the vortex caustics based on our theory in
291 the paraxial regime where the polarization components can be decoupled. Interesting
292 opportunities also arise for extending our work to the nonparaxial regime. We expect that these
293 results will promote the development of numerous applications, such as material processing,
294 microscopy, particle micromanipulation and synthesis of novel electro-magnetic wavepackets
295 [36, 37]. Also, the structural stability of the different solutions in the nonlinear regime can
296 represent interesting future work.

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303 **Data availability.** Data underlying the results presented in this paper are not publicly available at this time but may
304 be obtained from the authors upon reasonable request.

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