

LES MÉTAUX AMORPHES, UNE INNOVATION DE RUPTURE DANS LE DOMAINE DES MATÉRIAUX ET DE LA FATIGUE

*Guillaume COLAS,
Stani Carbillet,
Pierre-Henri Cornuault*

*Alexis Lenain,
Léna Verchère*

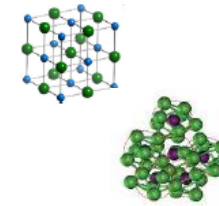
*Laurent Cadiergues,
Pascal Durand*



BULK METALLIC GLASSES

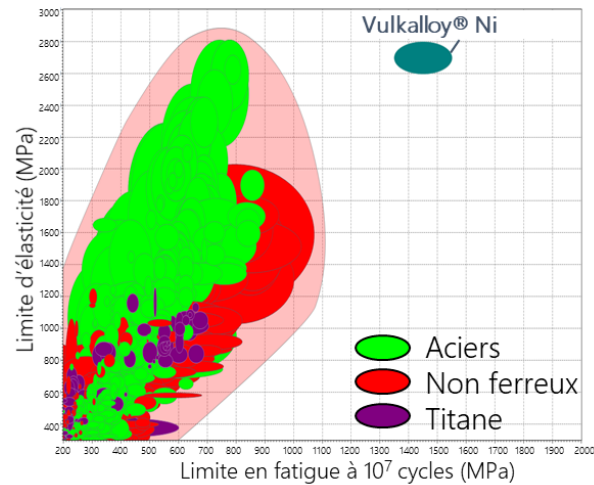
Microstructure

- Common alloys ► crystalline microstructure
- Bulk Metallic Glass ► amorphous microstructure

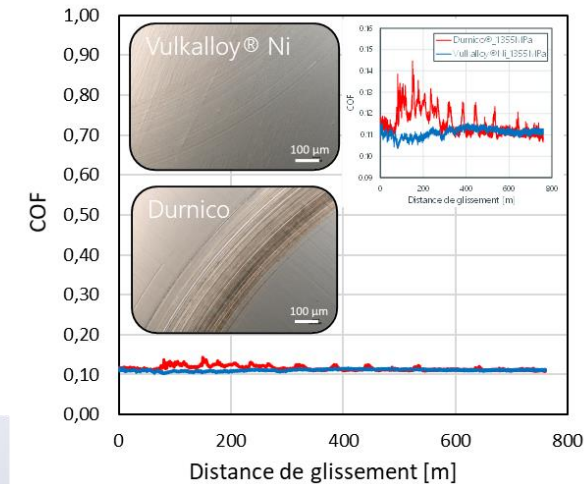
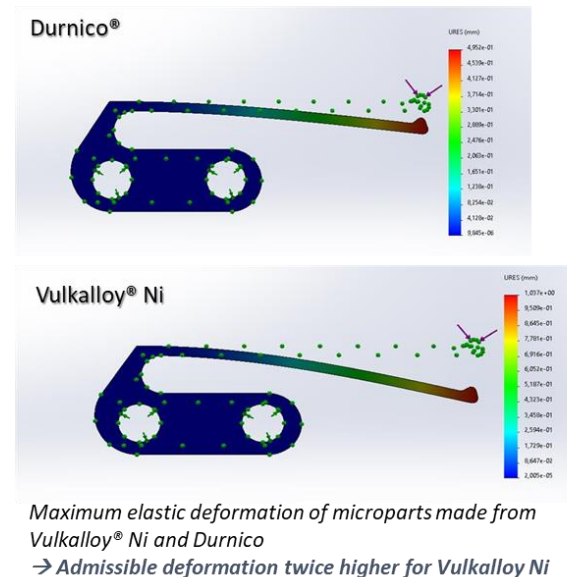
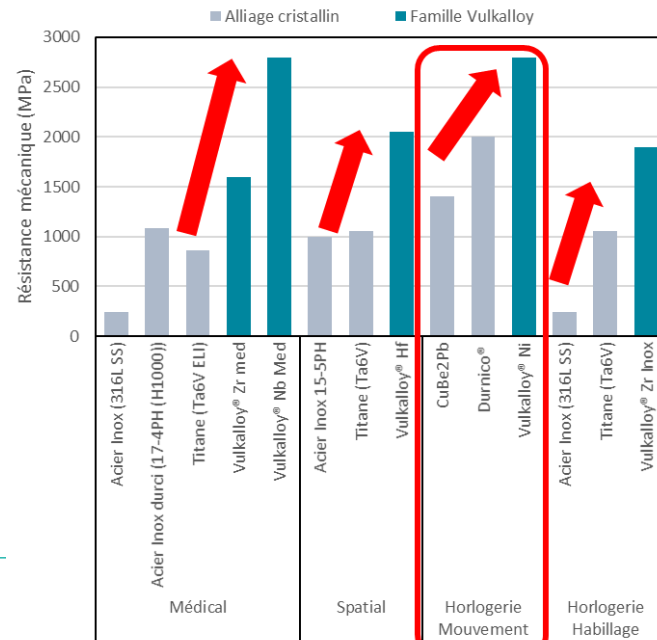


Mechanical and physical properties

- High elastic limit, High reversible deformation range
- High strength, High fatigue resistance
- High corrosion resistance
- High hardness, ...



+ elongation of 1.8% !!

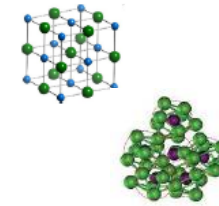


Friction and wear of Vulkalloy® Ni vs Durnico sliding against CuBe @ 1350MPa
→ Very low wear and very stable friction, almost no wear for Vulkalloy® Ni

BULK METALLIC GLASSES

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- High hardness, ...

Pure Metals

1. Automated batch melting



Materials pellets



2. Automated Molding



Parts in Vulkalloys®



Thermomouldage Net shape



Thermomouldage Near Net shape



Thermomouldage 2D + Laser



Micromouldage 3D

Extremely good molding properties

⇒ near netshape molding
⇒ Machining
⇒ Laser processing
⇒ ...

Recycling
= optimized ressources management

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LIMITED COMPONENT SIZE DEPENDING ON THE COMPONENTS

1. Micro-components

- 0,2 à 10 mm³
- Tolerances < 2μm / Ra < 0,1

2. Miniature-components

- 10 à 250 mm³
- Tolerances ± 0,015 mm / Ra < 0,35

3. Millimeter size components

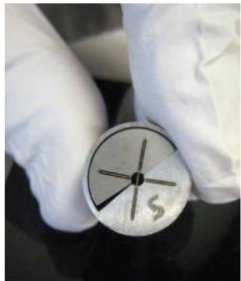
- 250 à 1000 mm³
- Tolerances ± 0,02 mm / Ra < 0,35

OBJECTIVE OF THE STUDY

- Explore the potential of the BMG in flexure and rolling/sliding micro/mini applications

❑ Flexural Pivot / Bearing

stroke increase wrt **endurance** limit



❑ Micro Gears

Lifetime increase wrt **tribology**

Torque capability increase wrt **yield strength**

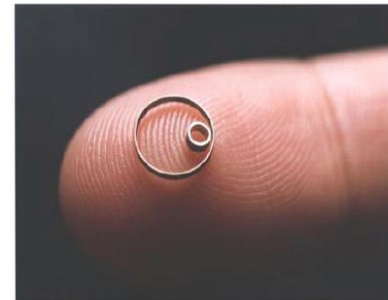


Fig. 5 Gear wheels in Nickel-Iron alloy

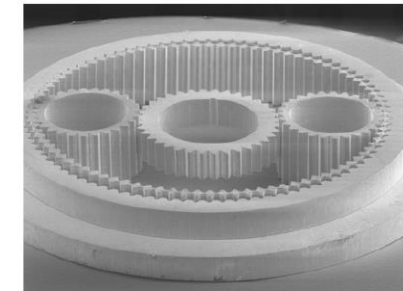


Fig. 6 Micro Harmonic Drive® gear component set

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MATERIAL CHOICE FOR THE STUDY

- Flexure materials, Harmonic drive (flexspline), gears
 - High to moderate E (160 GPa ideal for flexspline)
 - High strength and rupture strength
 - Good fatigue endurance
 - High tenacity
- Good corrosion résistance
- Low outgassing
- Low vapor pressure
- Low thermal expansion
- Good wear resistance for tribological applications

		Vulkalloy Base Zr	Vulkalloy Base Cu	Vulkalloy Base Ni	TA6V	15-5PH H1025	440C
Dureté	(HRC)	42	48	63	41	35	59
Déformation élastique	(%)	2	2	1,8	0,7	0,5	1
Module d'Young	(GPa)	80	95	150	115	200	200
Limite d'élasticité	(MPa)	1660	1900	2800	860	1000	1900

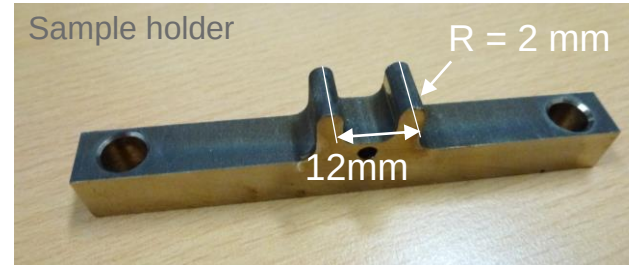
- BMGs meeting all requirements (in general) are Ni-based and Cu-Zr-based
 - Ni-based offers the best corrosion resistance than Cu-Zr
 - NI-based offer better corrosion resistance than 17-4 PH (acier utilisé aussi dans les engrenages *(Hampson 2015)*)
 - Ni-base equal 15-5PH
- Additionnal advantage of BMG: surface roughness

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FATIGUE TESTS – QUASI STATIC 3 POINT BENDING

➤ Samples

- Dimensions : 20*4,8*0,48 mm en AMA Ni1
- From 2 batches
- Polished to $R_a < 0.2$



➤ 3 different tests

➤ Quasi-static

- 5 repetitions
- Load @ 1mm/min
- Until rupture

➤ Whöler curves

- 10^6 cycle
- 30 Hz
- $R = 0.1$
- 13 tests

➤ Fatigue endurance tests

- Staircase method ISO 12107/2012
- 10^7 Cycle
- 30 Hz
- $R = 0.1$
- Step of 50 Mpa
- 15 tests

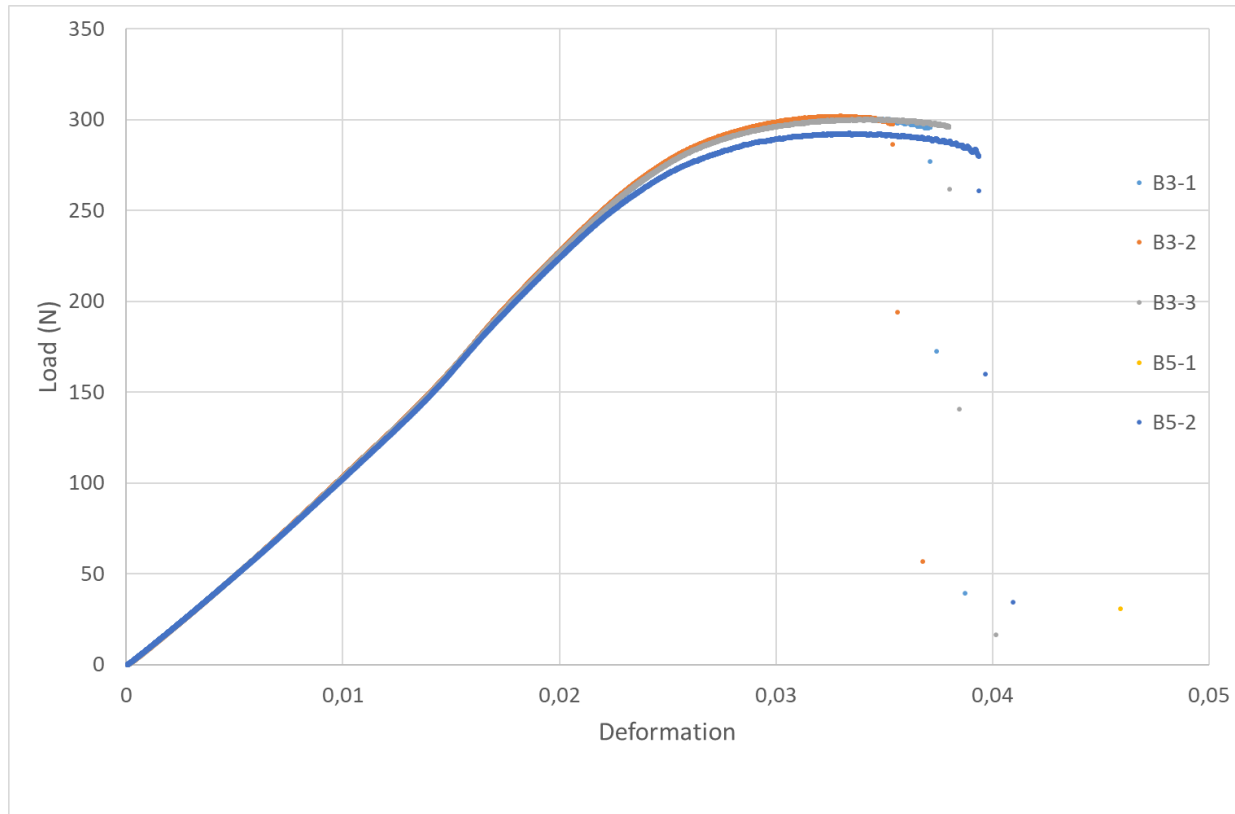
- Instron ELECTROPULS E10 000
- Load cell of 1 KN



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FATIGUE TESTS – QUASI STATIC 3 POINT BENDING

➤ Load vs deformation

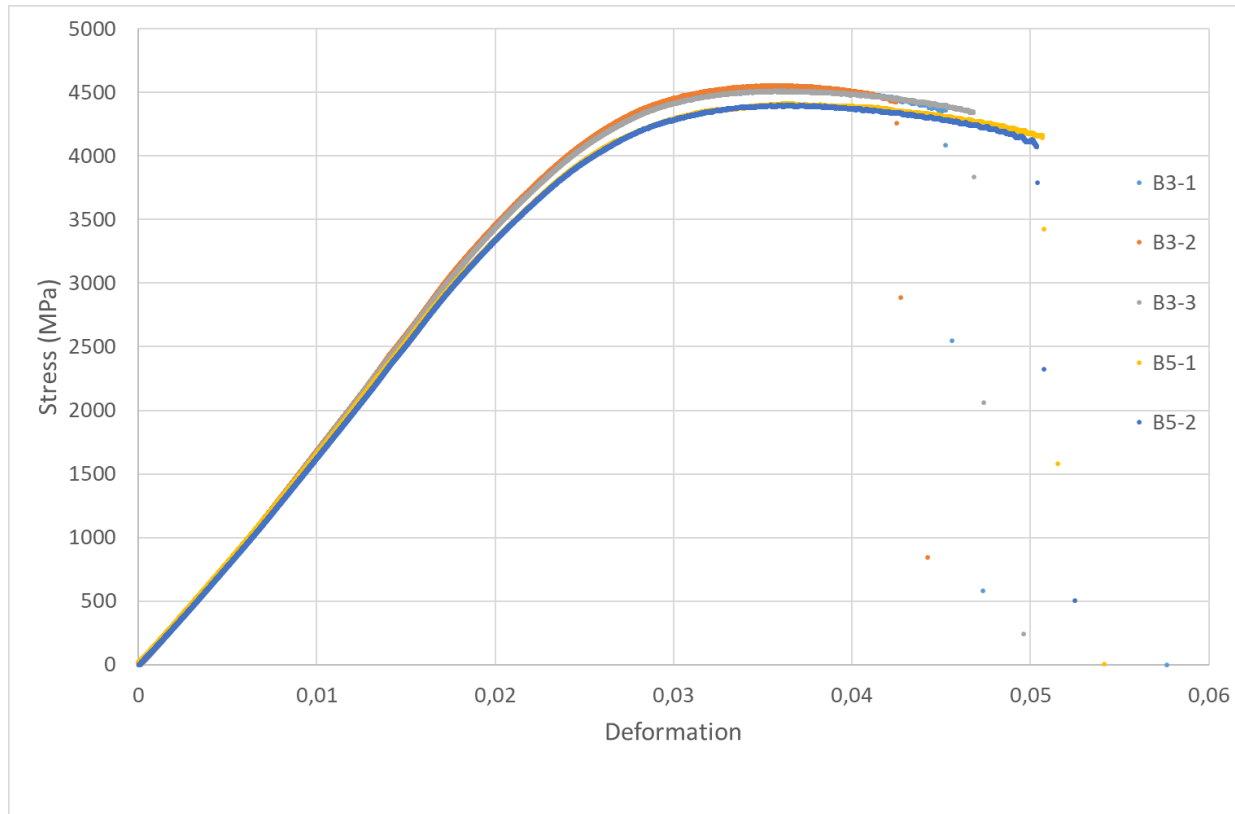


- 2 mm deflection @ rupture !
 - Need to take it into account in the deformation calculation
- Highly reproducible

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FATIGUE TESTS – QUASI STATIC 3 POINT BENDING

- Stress vs deformation => corrected data



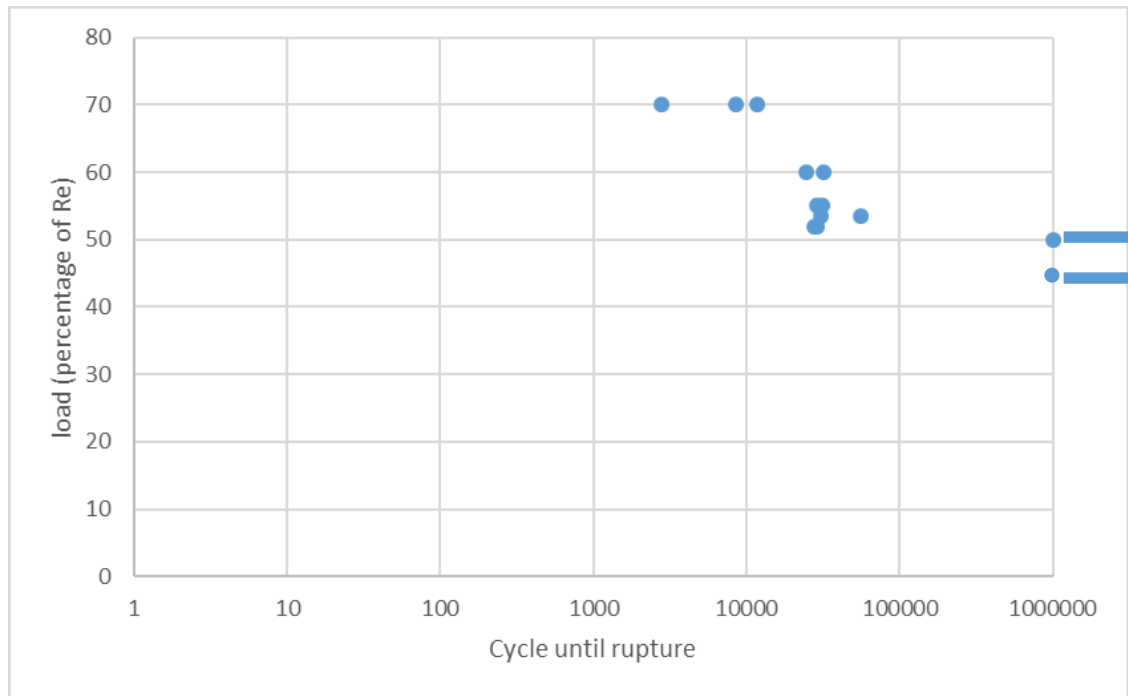
- 2 mm deflection @ rupture !
 - Need to take it into account in the deformation calculation
- Highly reproducible
- Rupture due to local plasticization of the loading points
- Deformation at rupture not relevant due to traction and compression stresses over the sample thickness

	Re (MPa)	Rm (MPa)	Rupture Stress (MPa)
B3-1	2850	4560	4362
B3-2	2840	4557	4255
B3-3	2845	4555	4344
B5-1	2838	4402	4146
B5-2	2835	4408	4076
Moyenne	2841,6	4496,4	4236,6
Ecart-type	5,31	74,67	110,99

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FATIGUE TESTS – 3 POINT BENDING – WÖHLER CURVE

- Load applied calculated based on each sample geometry
- Reminder :
 - 10^6 cycle unless rupture ; 30 Hz ; $R = 0.1$



Percentage of elastic limit	Cycle to rupture	Batch N°
70	2 759	B5
70	8 561	B3
70	11 811	B5
50	1 000 000	B3
50	1 000 000	5
45	1 000 000	B3
60	24 652	B5
60	31 954	B3
55	31 153	B3
55	28 893	B5
52	29 079	B5
52	43 894	B5
52	27 432	B3

BULK METALLIC GLASSES

FATIGUE TESTS – 3 POINT BENDING – STAIRCASE

- Load applied calculated based on each sample geometry
- Reminder :
 - 10^7 cycle unless rupture ; 30 Hz ; $R = 0.1$

O : sample passed
X : sample failed

	Test number														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
	Batch number														
Stress (Mpa)	B5	B3	B3	B3	B3	B3	B5	B3	B3	B5	B3	B5	B3	B3	B5
1550			X				X								
1500		O		X		O		X		X					
1450	O					O			O		X		X		
1400												O		X	
1350															O
Cycle @ rupture			30 690	27 432			55 715	18 936		43 894	26 298		33 487	38 740	

BULK METALLIC GLASSES

FATIGUE TESTS – 3 POINT BENDING – STAIRCASE

- Load applied calculated based on each sample geometry
- Reminder :
 - 10^7 cycle unless rupture ; 30 Hz ; $R = 0.1$

With samples that failed the test

contraintes Mpa	15 éprouvettes 8 rompues			
	i	ni	i*ni	i ² *ni
1550	4	0	0	0
1500	3	2	6	18
1450	2	3	6	12
1400	1	1	1	1
1350	0	1	0	0
Pas p (Mpa)	50			
Coeff N	7			
Coeff A	13			
Coeff B	31			
σ_0 (Mpa)	1350			
Résistance en fatigue σ_D (Mpa)	1468			
Condition de validité écart-type	0,98			
Ecart-type s (Mpa)	82			

With samples that passed the test

contraintes Mpa	15 éprouvettes 7 non rompues			
	i	ni	i*ni	i ² *ni
1550	4	2	8	32
1500	3	3	9	27
1450	2	2	4	8
1400	1	1	1	1
1350	0	0	0	0
Pas p (Mpa)	50			
Coeff N	8			
Coeff A	22			
Coeff B	68			
σ_0 (Mpa)	1350			
Résistance en fatigue σ_D (Mpa)	1463			
Condition de validité écart-type	0,98			
Ecart-type s (Mpa)	78			

Endurance Limit ($R=0.1$, 50%) = 1460MPa

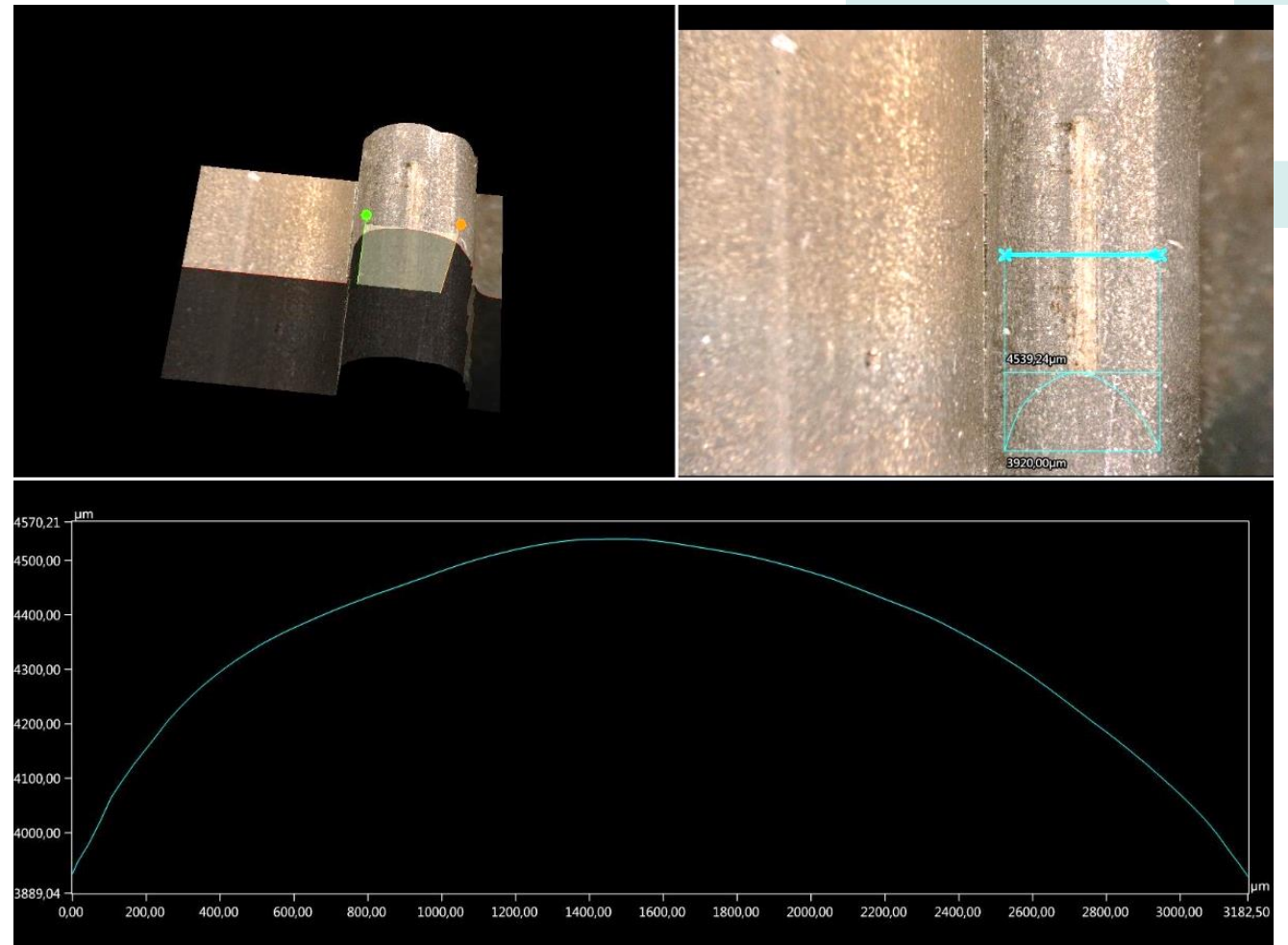
Standard Deviation : 5,6% (< typical 8% for standard alloys)

Endurance Limit with 99.9% reliability ($R=0.1$, 99,9%) = 1190MPa

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FATIGUE TESTS – 3 POINT BENDING

- Sample holder post test verification

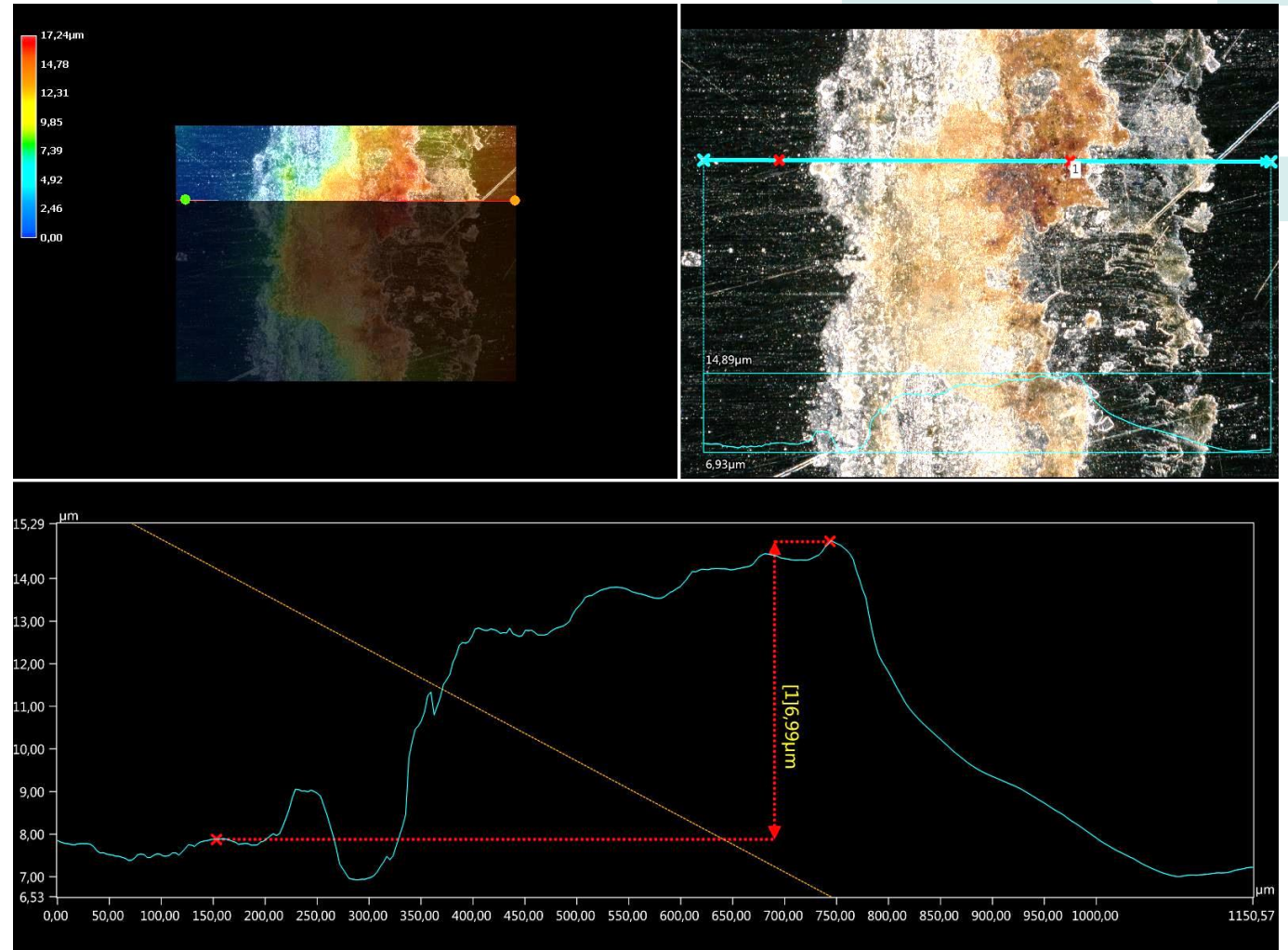
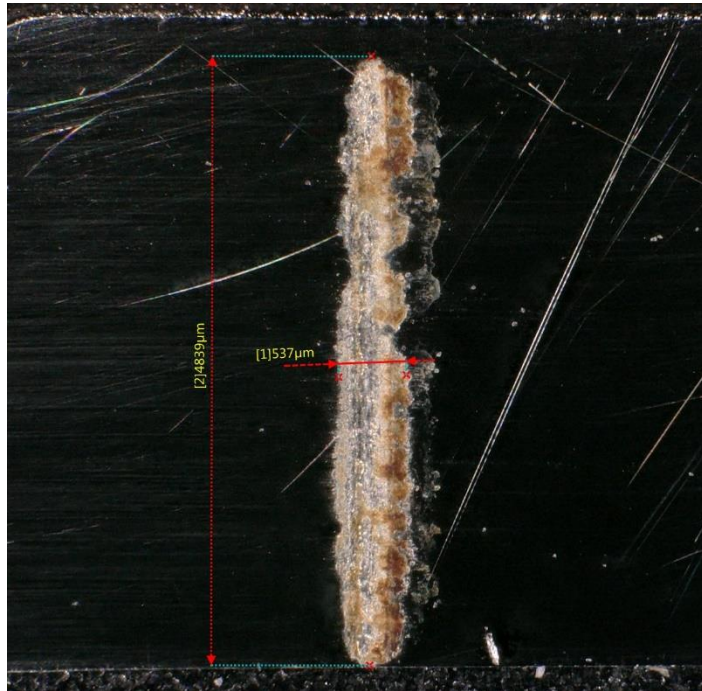


- Wear marks located at the contact points between BMG sample and sample holder
 - No significant damages detected => geometry not impacted

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FATIGUE TESTS – 3 POINT BENDING

- Sample post test verification



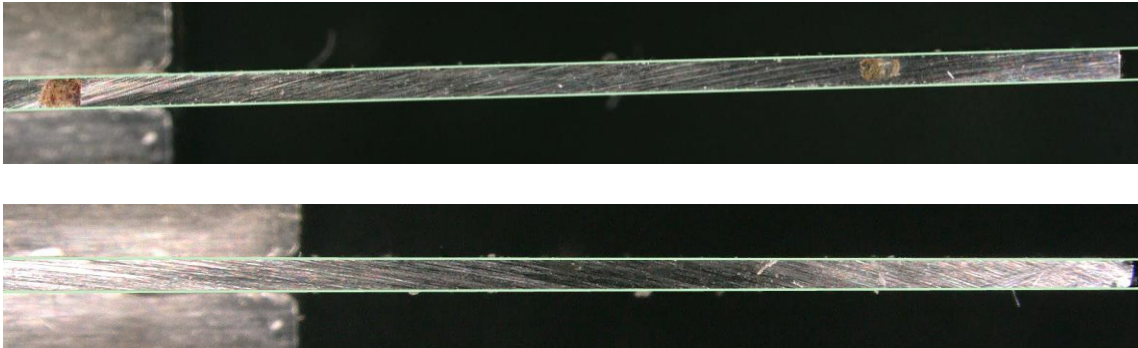
- Wear marks located at the contact points between BMG sample and sample holder
 - Transferred material from the holder

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FATIGUE TESTS – 3 POINT BENDING

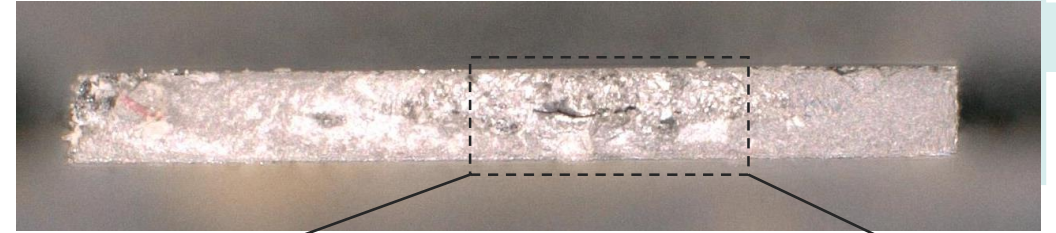
- Sample post test verification

Geometry of successful samples



- Samples that passed the endurance tests are not showing any deformation after test.

Rupture surface



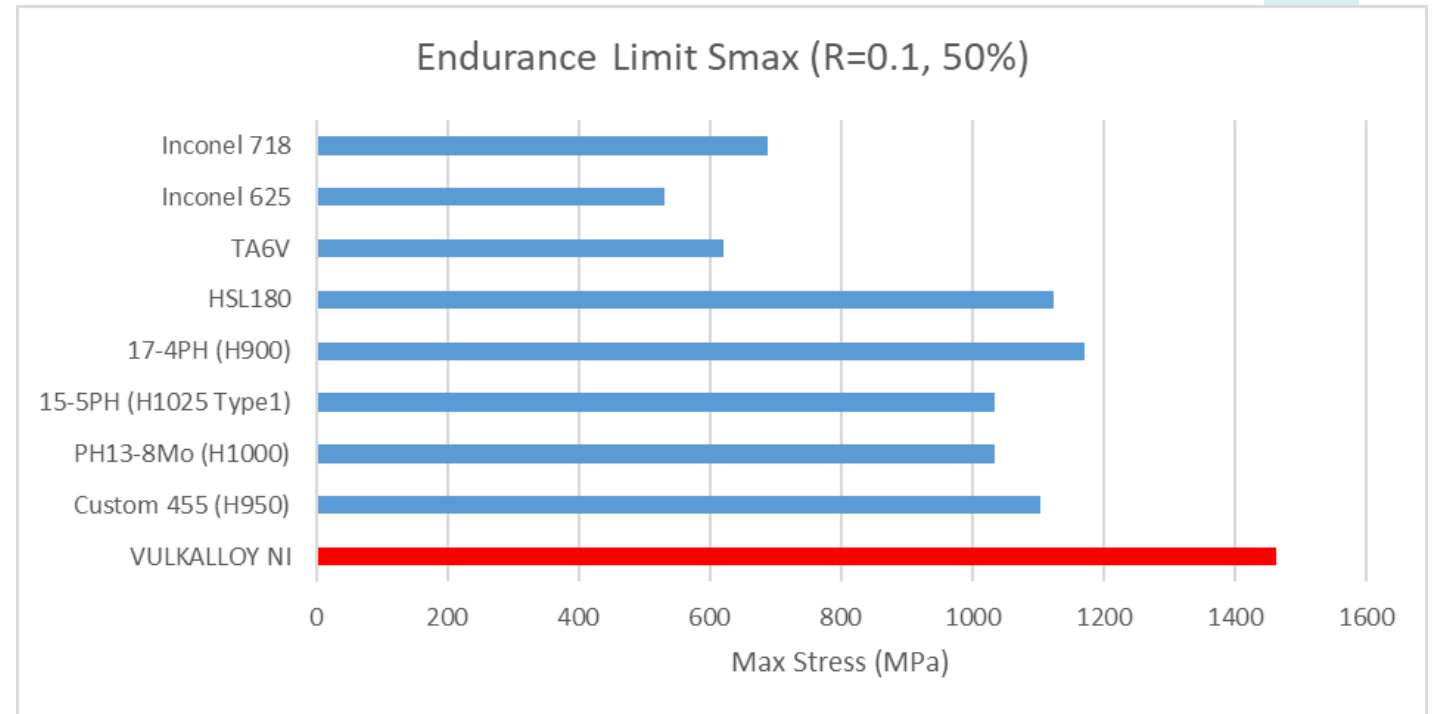
- Cracks visible in the rupture section, mostly at the neutral fiber
- Normal features and morphologies of the section for a BMG sample

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FATIGUE TESTS – RESULTS SYNTHESIS + COMPARISON WITH COMMON MATERIALS

Property	Unit	Vulkalloy Ni
Typical Thickness	mm	<1
Density	kg.mm3	8800
CTE	ppm/K	11
Hardness	HRC	63
Young Modulus	GPa	151
Yield Stress	MPa	2840
Endurance limit (R0.1, 50%)	MPa	1460
Endurance limit standard deviation	MPa	85

- Standard Deviation : 5,6% (< typical 8% for standard alloys)
- Endurance Limit with 99.9% reliability (R=0.1, 99,9%) = 1190MPa

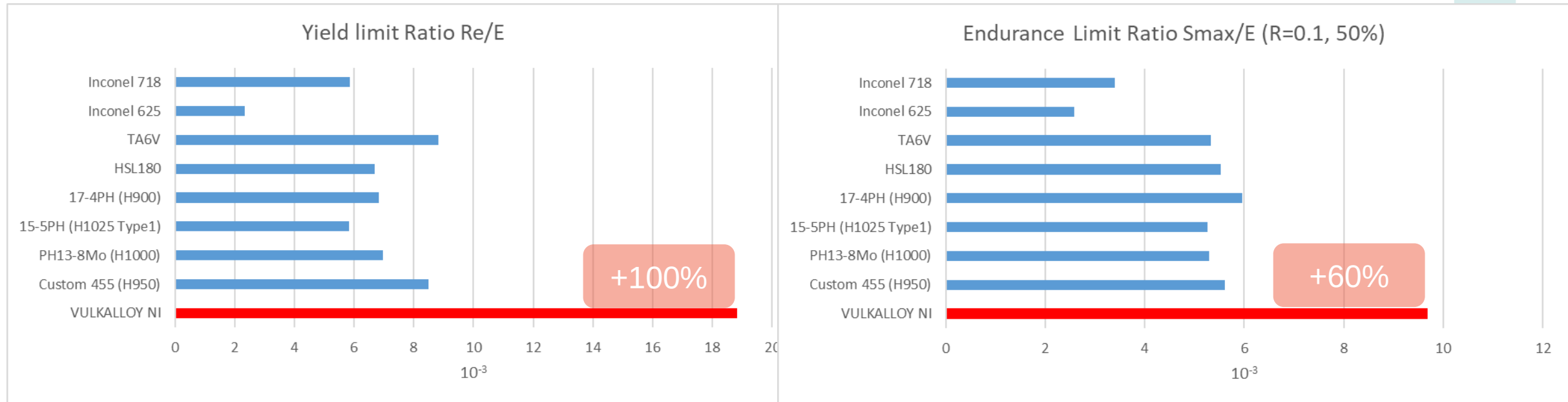


Common Alloys Data Source : MMPDS

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FATIGUE TESTS – COMPARISON WITH COMMON MATERIALS

Strain capability proportional to Stress to Modulus ratio



➤ VulkalloyNi surpasses all the reference materials

➤ Extremely promising material for flexure applications

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FATIGUE TESTS – CONCLUSION

- **Vulkalloy Ni surpasses all the reference materials**
- **Extremely promising material for flexure applications**
 - Accept larger deformation ranges than crystalline material
 - No needs for specific design rules
- **For Harmonic Drive flexspline**
 - Flexspline displacement is fixed => for a fixed loading, stress imposed will be lower if Young's modulus is lower
 - ISO geometry => Vulkalloy Ni will induce lower stress
 - Higher propensity for low wear
- **Industrial scale manufacturing process (plates, rods, finished and semifinished parts)**
 - Includes formulation, molding, machining, etc...

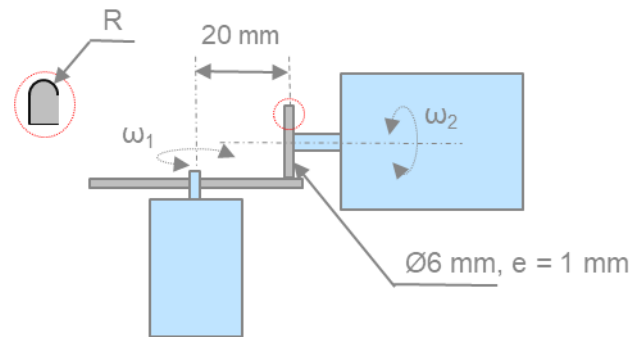
Ready to be used

*Call for
application case*

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NEXT STEP : TRIBOLOGICAL TESTS

- Rolling with sliding study for HD and gear applications
- Main contact conditions
 - Vacuum: $5.10e-7$ mbar, and Air 50%HR
 - Sliding to Roll Ratio (SRR) = 30%,
 - 1.2 GPa contact pressure
 - 3 types of contacts :
 - BMG / BMG
 - BMG / 15-5PH 1075
 - 15-5PH 1075 / 15-5PH 1075
 - 3 tests per contact types per environments



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THANKS FOR YOUR ATTENTION

Thanks to CNES for supporting the study

See you next time for the rolling with sliding test results...



guillaume.colas@femto-st.fr



alexis.lenain@vulkam.com



Laurent.Cadiergues@cnes.fr

