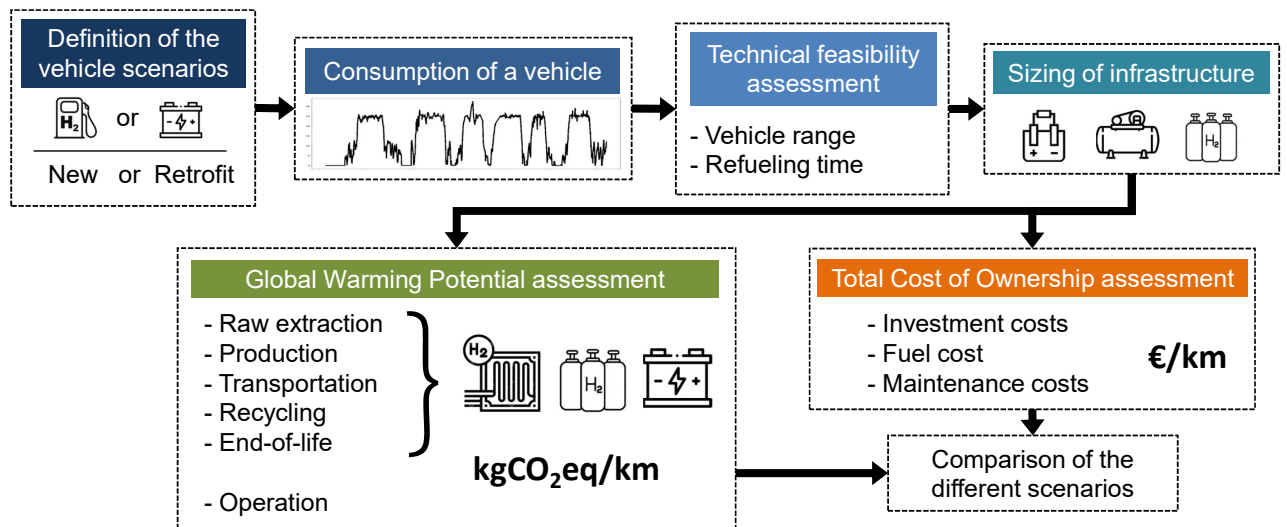


Graphical Abstract

Investigating the use of hydrogen and battery electric vehicles for public transport: a technical, economical and environmental assessment

Agnès François, Robin Roche, Dominique Grondin, Nastasya Winckel, Michel Benne



Highlights

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- GWP depends mainly on operation phase, the least on the transport of the technologies
- With marked relief, range and recharging time are a limit of battery coaches
- A battery and fuel cell coach mix results in an economic and environmental optimum
- Improvements in eco-driving and vehicle weight reduce costs and environmental impact

Investigating the use of hydrogen and battery electric vehicles for public transport: a technical, economical and environmental assessment

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Abstract

More and more territories are looking at alternatives to diesel for their public transport to decarbonise their energy mix. Electricity and hydrogen, among the most popular alternatives, are analysed in this article on the basis of various technical, economic and environmental criteria. The consumption of these vehicles is first estimated and the feasibility of their implementation validated in terms of range and recharging time. The economic criterion then evaluated is the total cost of ownership (TCO) of the vehicle fleet, and the environmental criterion is the global warming potential (GWP) of a vehicle, taking into account the life cycle of the main technologies that compose

Abbreviations: EoL, end-of-life; FC, Fuel Cell; GWP, Global Warming Potential; H₂, Hydrogen; ICE, Internal Combustion Engine; LFP, Lithium-iron Phosphate; NMC, Nickel Manganese Cobalt; PV, Photovoltaics; TCO, Total Cost of Ownership

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it as well as the vehicle's operating phase. Here, coaches are analysed for the case study of Reunion Island. If the technical feasibility concludes that it is impossible to use a fleet entirely composed of electric vehicles, a fleet composed only of hydrogen vehicles would involve high TCO and GWP. A balance must be struck and improvements in vehicle consumption can be made to reduce the overall impact.

Keywords: energy transition, total cost of ownership, global warming potential, fuel cell vehicles, heavy mobility, Reunion Island

1. Introduction

Given the increasingly visible effects of climate change on the Earth, new solutions are being considered all over the world to reduce our dependence on fossil fuels. In particular, the mobility sector is at the heart of both debates and research. Indeed, it was responsible for the emission of nearly 8 gigatonnes of CO₂ worldwide in 2022 [1]. Over 73 % of these emissions come from the road sector, and 44 % from individual vehicles alone (3.53 gigatonnes of CO₂ in 2022 [2]). With their particular energy situation, combining dependence on climatic events, limited space and heavy reliance on private cars, island territories are particularly dependent on fossil imports for their mobility. Decarbonising the transportation sector is therefore a major challenge for these territories. The development of public transport is one of the plans to do so. For example, in the global transport sector in 2022, buses emitted less than 8 % of CO₂ emissions (0.45 gigatonnes of CO₂ [3]). In order to reduce global emissions, these means of transport need to be developed even further, and use low-carbon energy where this is not already the case.

17 The public transport sector, composed of buses and coaches, is often
18 studied in the scientific literature for an optimal decarbonisation. While
19 the former operate mainly in cities, with routes interspersed with numerous
20 stops and carrying more passengers, the latter are mainly used for inter-city
21 routes, which are longer and have fewer stops. As buses are the most com-
22 monly studied vehicles, the main solutions for decarbonising the sector in-
23 clude hybrid diesel-electric buses, natural gas buses, battery-electric buses or
24 hydrogen fuel-cell buses. As a solution that has not yet been fully developed
25 for this application sector, hydrogen-powered buses with internal combustion
26 engines (ICE) are not widely discussed in the literature. The choice between
27 one technology or another often depends on the application, and can be based
28 on various technical, economic or environmental criteria. In [4], the authors
29 analyse the total cost of ownership (TCO) of electric and hydrogen buses in
30 public transport in a small to medium-sized city and its surrounding area
31 in 2020 and in 2030. The same economic parameter is assessed in [5], but
32 this time for diesel, gas, hybrid and hydrogen technologies in Australia. This
33 criteria is also calculated in [6], centered on diesel, electric and fuel cell buses
34 comparison, and providing an assessment of CO₂ emissions over the lifespan
35 of the buses, and in [7], where diesel, compressed natural gas, fuel cell and
36 electric buses from a tropical urban area are compared, with an additional
37 criteria on bus pollutant emissions. Finally, this criteria can also be found in
38 studies without hydrogen, like in [8], where the authors focus on the detailed
39 comparison of two types of recharging for electric buses, depot charging or
40 opportunity charging at terminal stops, or in [9] with a complete economic
41 study involving the calculation of the net present value, the internal rate of

42 return and the payback period for diesel, compressed natural gas and electric
43 buses. Some studies do not consider an economic assessment and are inter-
44 ested in showing an environmental comparison, like in [10] where the carbon
45 footprint of different fossil buses in Taiwan is calculated, with the one of
46 electric and fuel cell buses. In [11] and in [12], a Life Cycle Assessment
47 of different types of buses is build, considering extraction of raw materials
48 through their utilization as fuel for the former, and total energy use by fuel
49 type, greenhouse gases emissions and criteria air pollutants for the latter.
50 In [13], the authors use a Life Cycle Assessment approach with a Life Cy-
51 cle Inventory analysis, through an environmental model developed to assess
52 the impact of energy carrier consumption and electricity origin on driving.
53 Various energy sources, including wind, solar, waste, and grid electricity, are
54 analyzed throughout the life cycles of the carriers and infrastructure. Finally,
55 some studies compare technologies on the basis of economic and environmen-
56 tal criteria, like in [14], where the lifecycle costs and CO₂ emissions of diesel,
57 natural gas, hybrid, fuel cell and electric buses are evaluated, or in [15], cen-
58 tered on the last two types of vehicle and assessing their emission reduction,
59 capital, maintenance and energy costs. Sometimes other additional criteria
60 can be studied, like noise pollution, sense of comfort or speed of traffic flow
61 [16].

62 One of the main limitations of all these studies is the lack of detail in the
63 sizing of the infrastructure required for refueling hydrogen vehicles, which
64 is sometimes overlooked in the environmental impact calculations. This has
65 been done in the literature, but the corresponding studies often focus on
66 hydrogen technology and therefore do not allow a comparison with other

67 technologies. This is the case of [17], which is investigating the sizing of the
 68 electrolyser to produce hydrogen for a bus fleet and its economic evaluation.
 69 In [18], the hydrogen fuel supply chain is optimised in order to minimise the
 70 levelized cost of hydrogen for fuel cell buses, but no environmental assessment
 71 is made. This is also the case in [19], which optimises hydrogen production
 72 in order to minimise its costs. Finally, [20] optimises the Levelized cost of
 73 driving and the Carbon Intensity of a diesel bus fleet, by optimising the pro-
 74 portion of vehicles converted to hydrogen, and [21] works on the configuration
 75 of the electricity supply system and the hydrogen production system to power
 76 a fleet of hydrogen-powered buses. This assessment is based on an energy,
 77 economic and environmental analysis. On the whole, economic studies offer
 78 consistent results. In the short term, they conclude that battery-powered
 79 vehicles are economically more advantageous than hydrogen-powered vehi-
 80 cles (still emerging sector, high costs and lack of infrastructure). In the long
 81 term, however, the conclusions are often reversed depending on the local sit-
 82 uation. Meanwhile, environmental studies regularly fail to take into account
 83 the impact of technologies outside the vehicle’s operational phase. This is
 84 often done for studies on individual vehicles, as in [22], but not for public
 85 transport. While the literature is often quite extensive concerning studies on
 86 buses, the present paper will focus on coaches, vehicles not studied in the
 87 literature. The technologies are similar, but the data may differ, as may the
 88 state of research and marketing, and the actual uses.

89 All these studies cover the techno-economic and life-cycle assessment as-
 90 pects of zero-emission vehicles. Overall, coaches have been largely overlooked
 91 in public transport studies, as has hydrogen combustion in the consideration

92 of new vehicle technologies. Moreover, very few studies take into account
93 real speed profiles when estimating vehicle consumption, or the appropriate
94 sizing of vehicle recharging technologies. Finally, there are very few articles
95 comparing electric and hydrogen vehicles on the basis of TCO and global
96 warming potential (GWP). Moreover, no literature article measures the im-
97 pact of the latter criterion on in-vehicle technologies (batteries, fuel cells,
98 hydrogen storage) for public transport.

99 In this way, the work proposed in the present article will address these
100 previous shortcomings by proposing a complete comparison of hydrogen and
101 battery electric coaches for public transport. This comparison will take into
102 account hydrogen production infrastructure and their sizing will be detailed
103 in the article. A technical, economic and environmental assessment of differ-
104 ent coach technologies will be made, by evaluating the total cost of ownership
105 and the global warming potential of these technologies. This last criterion
106 will take into account all the stages in the life cycle of the technologies used in
107 the vehicles and the operation phase of the vehicles. In particular, hydrogen
108 retrofitted coaches and new hydrogen coaches will be compared with electric
109 retrofitted coaches and new electric coaches. Vehicles with hydrogen ICE
110 will also be considered in the study. The TCO of coaches will be studied on
111 a real fleet over a period of 8 years (half the lifetime of the coaches studies).
112 The methodology presented, although replicable to other case studies, will
113 be applied to the local case of Reunion Island, a French island seeking to
114 move closer to energy self-sufficiency and currently considering hydrogen as
115 a solution to decarbonise its mobility. Considering an island territory as a
116 case study offers a number of specificities: for example, terrain and climatic

117 conditions may involve higher vehicle consumption than found in most of
118 the literature. In addition, it is possible to model the entire electricity net-
119 work and consider the impact of vehicles on it. Finally, as mentioned at the
120 beginning of the introduction, the transition of these territories is a major
121 challenge that needs to be studied. The work will enable the advantages and
122 disadvantages of the technologies studied to be presented in terms of differ-
123 ent criteria, so as to provide an overall view of each possible solution for the
124 area in question. The results obtained will therefore be specific to the case
125 study, and if one technological solution stands out, this may not be the case
126 elsewhere.

127 Following the introductive section, the methodology is presented in Sec-
128 tion 2. In this section, the modelling of vehicle consumption is described
129 as well as the sizing of hydrogen vehicle refueling infrastructures. The two
130 economic and environmental criteria assessed in the work, the TCO and the
131 GWP, are also presented. In Section 3, the case study is described, with
132 every local data and assumptions detailed. Finally, Section 4 presents the
133 obtained results and discusses them. This section starts with a subsection
134 on the technical feasibility of every scenario studied, then details the eco-
135 nomic and environmental assessment of the two criteria introduced above.
136 The article concludes in section 5.

137 **2. Methodology**

138 The objective of the present article is to compare different technologies
139 of public transportation, over different criteria. In particular, different tech-
140 nologies of coaches will be studied: electric ones, composed of a battery and

141 refueled by electricity, hybrid ones, composed of a battery and a fuel cell
142 and refueled by hydrogen, and hydrogen ones, composed of a battery and a
143 combustion engine, and refueled by hydrogen. Scenarios involving retrofits
144 and investment in new vehicles will be considered.

145 The first aspect to assess is the technical feasibility of the different mod-
146 elled scenarios compared to local characteristics. In particular, local energy
147 production, range of the vehicles and refueling time will be studied. To do
148 so, the consumption and the distances traveled by the different vehicles are
149 required. Then, the size of the infrastructure required to supply them are
150 investigated, before starting the comparison over economic and environmen-
151 tal points of view. The total cost of ownership (TCO) in euros per kilometre
152 for a whole fleet are first calculated to make an economic comparison of the
153 technologies. Then, the global warming potential (GWP) is assessed to make
154 an environmental comparison. If the final results obtained are contradictory
155 in the case of the economic assessment and in the case of the environmental
156 one, the choice of one technology over another can be made in relation to
157 other criteria (water consumption, consumers acceptance, etc.). A summary
158 of the followed methodology can be seen in Figure 1.

159 *2.1. Energy consumption estimation*

160 The first step before assessing the technical feasibility of the different
161 modelled vehicles is the estimation of their average energy consumption. To
162 do so, the power consumption of a vehicle at each timestep of its journey
163 is studied, and one or more speed and elevation data profiles are required.
164 These can be taken from real data or simulated, but are necessary to estimate
165 the fuel consumption of the vehicle at best. The different forces applied to

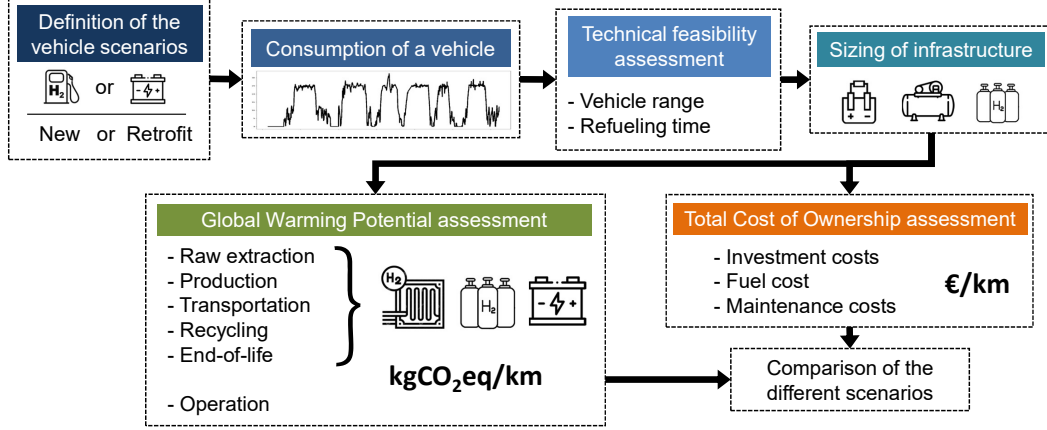


Figure 1: Methodology of the present study.

the vehicle are calculated at each timestep [23]:

$$F_a(t) = \frac{1}{2} \times \rho \times A \times C_x \times v(t)^2 \quad (1)$$

$$F_r(t) = m \times C_r \times g \times \cos \alpha(t) \quad (2)$$

$$F_g(t) = m \times g \times \sin \alpha(t) \quad (3)$$

with F_a the aerodynamic resistance (N), F_r the rolling resistance (N), F_g the climbing resistance (N), ρ the air density taken at 1.21 kg/m^3 [24], g the gravitational acceleration taken at 9.81 m/s^2 and m the mass of the vehicle (kg). A stands for the vehicle frontal area (m^2), C_x the vehicle drag coefficient and C_r the rolling resistance coefficient, three parameters specific to the modelled vehicle. Finally, v the speed (m/s) and α the slope (radians) are two variables changing at each timestep. To obtain power at the wheels P_{wheels} (W), all the forces introduced previously are summed [25]:

$$P_{wheels}(t) = v(t) \times \left(m \frac{dv(t)}{dt} + F_a(t) + F_r(t) + F_g(t) \right) \quad (4)$$

175 The instantaneous power $P_{traction}$ (W) is then calculated [8]:

$$P_{traction}(t) = P_{AC} + \begin{cases} \frac{P_{wheels}(t)}{\eta}, & \text{if } P_{wheels}(t) \geq 0 \\ P_{wheels}(t) \times \eta \times r, & \text{if } P_{wheels}(t) < 0 \end{cases} \quad (5)$$

176 with P_{AC} the additional power required for the air conditioning or heating
 177 in the vehicle (in W, assumed constant during the journey), η the drivetrain
 178 efficiency taken at 0.8 [23] and r the percentage of energy recovered during
 179 downhill. Finally, the energy consumed in kWh during the journey of the
 180 vehicle is obtained by integrating the power profile:

$$E_{elec} = \int P_{traction}(t) dt \quad (6)$$

181 For a comparison between electricity-powered vehicles and hydrogen-
 182 powered ones, the hydrogen consumption is obtained from the global energy
 183 consumption:

$$E_{hydrogen_FC} = \frac{E_{elec} \times 3.6}{LHV \times \eta_{FC}} \quad \text{or} \quad E_{hydrogen_ICE} = \frac{E_{elec} \times 3.6}{LHV \times \eta_{H2ICE}}, \quad (7)$$

184 depending if the hydrogen is used to power an electric motor or a combustion
 185 engine. In Eq. 7, LHV is the low heating value of hydrogen taken at 120.1
 186 MJ/kg [23], η_{FC} is the efficiency of the fuel cell taken at 0.47 [24] and η_{H2ICE}
 187 is the efficiency of the combustion engine taken at 0.40 [26]. Both efficiencies
 188 were considered constant for the consumption estimates of this work. The
 189 3.6 factor is used to convert E_{elec} from kWh to MJ. To simplify estimates, the
 190 operation of the battery in hydrogen-powered vehicles has not been modelled.
 191 Hydrogen consumption results will therefore be slightly overestimated.

192 Once an average consumption obtained, it is possible to first assess the
 193 technical feasibility of the different scenarios, considering the range of the

194 vehicles, their refueling time and the average distances traveled every day.
 195 For hydrogen-powered vehicles, considering a normal refuelling rate at 3.6
 196 kgH₂/min [27] and one or more tanks onboard for a total between 25 and
 197 73 kgH₂ [28], the refueling time of one coach will not exceed 20 minutes,
 198 thus not constituting a strong constraint on the feasibility of the technology.
 199 Daily demand can then be generated, using a profile from [20] and adapt-
 200 ing it according to local constraints (working hours mostly). However, for
 201 electricity-powered vehicles, the charging time will depend on the charging
 202 power chosen, influencing directly power demand on the grid and lifetime of
 203 the embedded batteries [29]. To deal with this specific constraint, the net-
 204 work considered must be studied more precisely, in order to establish whether
 205 several charging per day are necessary, and if so whether fast charging is nec-
 206 essary.

207 Once the technical feasibility is confirmed, it is possible to model a de-
 208 mand profile for one year, in order to simulate the operation of the whole
 209 electricity grid with an additional consumption for the mobility, and to size
 210 the refueling infrastructures at the same time. Indeed, these data will be
 211 required for the economic and environmental comparison.

212 *2.2. Infrastructure modeling*

213 To assess the impact of hydrogen mobility on the case study, it is essen-
 214 tial to consider the entire hydrogen production process. In this section, the
 215 modelling used to size the infrastructure (electrolyser, compressor, station-
 216 ary hydrogen storage) is detailed. For electric scenarios, there is no charging
 217 infrastructure that needs to be sized, as the vehicles are powered directly
 218 from the grid and the charging power will be fixed considering the required

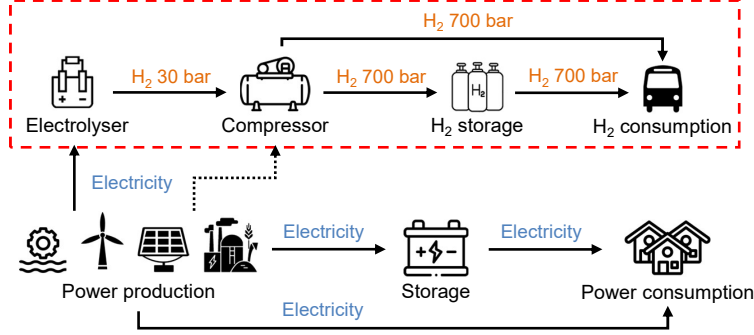


Figure 2: Modelling of a substation of the grid with a hydrogen refueling station framed in dots.

charging time.

The hydrogen necessary to refuel the coaches is produced locally by electrolysis of water, using electricity from the grid. Each refueling station is linked to a substation of the grid, as can be seen in Figure 2. Several refueling stations can be considered and placed near substations with high installed power generation capacities [30].

It is therefore important to take an interest in the grid and consider the energies that will make it up. The whole electrical system is modeled with PyPSA [31], which will allow the sizing of the refueling infrastructures. Moreover, line reinforcement is investigated with the model, as well as additional batteries at every substation, necessary to allow the operation of an electrical system with a high percentage of renewables, which is the aim of many territories in the coming years. The following notations are adopted: n for the different substations of the grid, k for the different refueling stations, s for the different technologies installed at the same station and t for the timesteps (every hour of the year simulated). The optimization of the sizing

235 of refueling infrastructure is made with a minimization of the investment and
 236 operating costs, as defined in the objective function below:

$$\begin{aligned} \min \sum_n c_{n,bat} \bar{e}_n + \sum_{k,s} [c_{k,s} \bar{g}h_{k,s} + c_{k,h2} \bar{e}h_k] + \sum_l c_l F_l \\ + \sum_t \sum_{n,s} [o_{n,s,t} g_{n,s,t} + o_{n,bat,t} h_{n,t}] + \sum_t \sum_{k,s} [o_{k,s,t} gh_{k,s,t} + o_{k,h2,t} hh_{k,t}] \quad (8) \end{aligned}$$

237 with $c_{n,s}$ the investment costs of a new technology, $\bar{e}_n$ the size of new batteries
 238 at every substation (MWh), $\bar{g}h_{k,s}$ the nominal power of electrolyzers and
 239 compressors (MW), $\bar{e}h_k$ the size of stationary hydrogen storages (MWh), c_l
 240 the costs of electrical line reinforcement, F_l the line reinforcements (MVA),
 241 $o_{n,s,t}$, the operation costs of the technologies, $g_{n,s,t}$ the operation of electricity
 242 production technologies, $h_{n,t}$ the operation of batteries, $gh_{k,s,t}$ the operation
 243 of electrolyzers and compressors and $hh_{k,t}$ the operation of hydrogen tanks,
 244 all in MW. Even if line reinforcement and additional batteries are included in
 245 the objective function, they will not be considered in the following economic
 246 assessment. Indeed, some previous study showed that line reinforcement and
 247 additional batteries are required in the medium term in order to aim for a
 248 more self-sufficient electricity grid [32]. Their sizing obtained in the present
 249 optimisation is thus not directly related to the presence of hydrogen vehicles
 250 and their impact will not be considered for the present study, focusing on
 251 the implementation of hydrogen refueling stations and the corresponding
 252 technologies.

253 The main constraints of the optimisation problem is the satisfaction of

254 both electric (Eq. (9)) and hydrogen (Eq. (10)) demands:

$$\sum_s g_{n,s,t} + h_{n,t} - \sum_l K_{nl} f_{l,t} = d_{n,t} + gh_{n,ely,t} + gh_{n,comp,t} \cdot \beta_{comp}. \quad (9)$$

$$gh_{k,ely,t} \cdot \eta_{ely} + hh_{k,t} = dh_{k,t} \quad (10)$$

255 with η_{ely} the efficiency of the electrolyser, taken at 50 kWh/kgH₂ [33], β_{comp} .
 256 the electric consumption of the compressors, taken at 1.68 kWh/kgH₂ [34],
 257 $d_{n,t}$ the electrical demand at a substation and $dh_{k,t}$ the hydrogen demand at
 258 a refueling station. The operation rate of electrolyzers and compressors is
 259 imposed over the year with Eq. (11):

$$\sum_t gh_{k,s,t} \geq \sum_t 1 \times CF \times \bar{gh}_{k,s} \quad (11)$$

260 with CF a capacity factor taken at 0.9. Removing this constraint would lead
 261 to the electrolyzers and compressors being oversized for economic optimum,
 262 and to highly intermittent operation, mainly at full power for less than ten
 263 hours a day. Decreasing the value of the capacity factor will also mean an in-
 264 crease in the size of the technologies and a more intermittent operation. The
 265 operation of hydrogen storage units is defined with the following equations:

$$eh_{k,t} = eh_{k,t-1} - hh_{k,t} \quad (12)$$

$$eh_{k,tinitial} \times (1 - 10\%) \leq eh_{k,tfinal} \leq eh_{k,tinitial} \times (1 + 10\%) \quad (13)$$

$$\bar{eh}_{k,s} \geq \max \sum_{24h} dh_{k,t} \quad (14)$$

$$eh_{k,s,t} \geq \max \sum_{24h} dh_{k,t} \quad (15)$$

266 Eq. (12) determines the stored energy with standing loss considered at zero
 267 and Eq. (13) defines a soft cyclical operation of the storage over the simulated

268 period. Eq. (14) enforces a minimum size for every hydrogen storage $e\bar{h}_k$.
 269 At each station, these must be large enough to cover the maximum hydrogen
 270 demand $dh_{k,t}$ for a whole day. This one-day demand is not identical over the
 271 year, and can vary between a working day and a public holiday. Moreover,
 272 Eq. (15) enforces the state-of-charge of these storages to be at least equal
 273 to this same demand. This measure reinforces the previous constraint, and
 274 makes it possible to locally store the demand for a full day for the whole
 275 fleet, to minimize the risk of not being able to run the fleet due to an issue
 276 on the electrolyser or the compressor [35]. This constraint directly influences
 277 the size of optimized storage.

278 The main results obtained from this optimisation are the size of the
 279 electrolysers, compressors and hydrogen storages, as well as the quantity
 280 of electricity produced used for the hydrogen refueling of the coaches and
 281 the composition of the electricity mix. The installed capacities of electricity
 282 generation technologies are not optimisation variables, but parameters of the
 283 optimisation problem. In addition, electricity production models for inter-
 284 mittent energy sources (photovoltaics and wind), have been determined on
 285 the basis of historical production and meteorological data, and the result-
 286 ing hourly production is therefore not directly optimised. Once the results
 287 collected, the economical and environmental comparison of the different sce-
 288 narios can be implemented.

289 *2.3. TCO calculation*

290 To start with the economic comparison of the technologies, their total
 291 cost of ownership will first be calculated. This criterion groups together all
 292 the direct and indirect costs involved for a fleet of vehicles, and is expressed

as a function of the travelled distance [36]. It is often used in the literature and therefore enables different technologies, different models or different case studies to be compared. The TCO of a scenario j (kind of coach technology) is calculated as follows:

$$TCO_j = \frac{(IC_j + II_j) \times CRF_j - RV_j + FC_j + MC_j + MI_j}{KM} \quad (16)$$

with IC_j the investment costs for the vehicle, II_j the investment costs for new infrastructure, RV_j the residual value of the vehicles if the end of their lifetime has not been reached at the end of the simulated period, FC_j the fuel costs for a year of operation, MC_j the vehicle annual maintenance cost and MI_j the infrastructure annual maintenance cost. Finally, KM stands for the number of kilometres travelled during a year by the whole fleet. CRF_j stands for the capital recovery factor, calculated as follows:

$$CRF_j = \frac{i \times (1 + i)^{n_j}}{(1 + i)^{n_j} - 1} \quad (17)$$

with i the discount rate taken at 4.5 % [37] and n_j the lifetime of the technology.

A few assumptions were taken for the calculations. Fuel cost is determined with electricity cost, as well as operation cost of electrolyser for hydrogen-powered coaches. If one scenario includes a retrofitting operation, no residual value has been considered for the old elements. Vehicle insurance and labour costs are not included in the calculations, because of a lack of data and an assumption of a small influence in the comparison. No national purchase aid was considered, whether for the retrofitting, the purchase of a new coach or the installation of new infrastructure. The obtained results can therefore be considered as an upper bound compared with costs that can be found in

Parameter	Value	Unit	Reference
Hydrogen retrofit cost	400	k€	Manufacturer
Hydrogen coach	620	k€	[20]
Electric retrofit cost	300	k€	[40]
Electric coach	440	k€	[38]
Maintenance cost of coaches	0.11	€/km	[4]

Table 1: TCO parameters for coaches.

return on experience reports. As electricity-powered coaches have a smaller range than hydrogen-powered ones [37, 38, 39], the possibility of fast charging at the terminus will be considered, with a comparison with a full charging at a charging station a few times a day. Data that can be used generically are detailed in Tables 1 and 2. Case-specific data will be detailed in section 3. It is assumed that a hydrogen station is based on an electric station, with some cost requirements for the depot charging station, the grid connection, the planning and the transformer.

2.4. GWP calculation

After the presentation of the criterion used for the economic assessment, the calculation of the global warming potential can be presented for the environmental comparison of the vehicles. This criterion, expressed in kgCO₂eq or kgCO₂eq/km, represents the impact of a single unit of greenhouse gas on the greenhouse effect, and allows to take into account CO₂ but also other greenhouse gases, converted into their equivalents in terms of carbon dioxide. In the present study, this criterion is calculated for the fuel cells, hydrogen

Parameter	Value	Unit	Reference
Electrolyser	410	€/kW	[41]
Electrolyser operation	0.154	€/kWh	[33]
Electrolyser maintenance	2	% of investment / year	[41]
Compressor	550	€/kW	[41]
Compressor maintenance	4	% of investment / year	[41]
Hydrogen tank	1350	€/kgH ₂	[27]
Hydrogen tank maintenance	3	% of investment / year	[4]
Hydrogen dispenser	65	k€	[20]
Hydrogen dispenser maintenance	3	% of investment / year	[20]
Electric station (depot charging station, grid connection, planning, transformer)	34	k€	[4]
Electric dispenser	35	k€	[38]
Electric dispenser maintenance and operation	0.14	€/kWh	[4]
Fast charging station (with coupling system and transformer)	515.5	k€	[4]
Fast charging station maintenance	5	k€/year	[4]

Table 2: TCO parameters for infrastructure.

Technology	GWP from raw material extraction, production and EoL	GWP with recycling	Reference
LFP battery	227.72 kgCO ₂ eq/kWh	127.45 kgCO ₂ eq/kWh	[43]
NMC battery	160.85 kgCO ₂ eq/kWh	128.48 kgCO ₂ eq/kWh	[43]
Fuel cell	42.94 kgCO ₂ eq/kW	29.47 kgCO ₂ eq/kW	[42]
Hydrogen tank	8.49 kgCO ₂ eq/kWh	x	[42]

Table 3: GWP data.

tanks and batteries of the different vehicles. This is done on different life cycle steps: raw materials extraction, production, transportation, recycling and end-of-life (EoL). The recycling phase will have an impact on the extraction and production of raw materials, thereby reducing emissions from the corresponding stages. This step is however not considered for the hydrogen tanks, as it is not possible yet to recycle them because of their high carbon fibre content [42]. Data used for all life cycle steps except transportation can be found in Table 3. Impacts of infrastructure, like electrolyzers, compressors or dispensers are not considered as the assessment of the GWP focuses on the technologies inside the vehicles.

For the transportation step of the assessed technologies, it is possible to consider different countries of origin and different ways of transport. Methodology from [44] is followed and Eq. (18) from [43] is used to calculate the GWP of this step:

$$GWP_{transport,s} = \frac{1}{E_s} \times \sum_i F_i D_i \quad (18)$$

with E_s the specific energy or power of a technology (data used are sum-

Technology	Value	Reference
LFP battery	151.3 Wh/kg	[43]
NMC battery	207.4 Wh/kg	[43]
Fuel cell	650.0 W/kg	[45]
Hydrogen tank	1400.0 Wh/kg	[46]

Table 4: Specific energy and power densities data.

Transportation mode	Value (gCO ₂ eq/t.km)
Truck (26 tons)	161.00
Truck (40 tons)*	94.00
Container ship	10.70
Electric train in France	1.55
Diesel train	28.10

* Used when main mode of transport is container ship

Table 5: Emission factor data from [43] for transportation mode.

346 marised in Table 4), F_i the emission factor of a mean of transportation per
 347 ton transported and per kilometre travelled (in gCO₂eq/t.km, data used are
 348 summarised in Table 5) and D_i the distance travelled by this mean of trans-
 349 portation in km. Different scenarios can then be simulated, with different
 350 transportation modes and different countries of origin when the exact place
 351 of origin of the technology was not given by the manufacturer. As this step
 352 has usually a small impact over the whole GWP, the worst case can be taken
 353 for each technology; for the transportation mode, a transport by truck is
 354 often the most impactful. For the scenarios with a retrofitting operation, it

Technology	Value (gCO ₂ eq/kWh)
Onshore wind	14.1
Photovoltaics	43.9
Hydroelectricity	6.0
Biomass	228.3
Biogas	342.4
Fossil	730

Table 6: Emission factor data for electricity generation facilities used, from [47].

is assumed that all elements have to stop at the place where the company selling the kit is located.

Finally, the emissions generated by the operation of vehicles are the last component of the GWP. Data used to estimate the impact of the electricity mix can be seen in Table 6.

3. Case study

The present article focuses on the case study of Reunion Island, a French overseas department located near Madagascar. With a population of nearly 900 000 inhabitants, the territory must import most of its energy, either for electricity production or mobility. In 2021, Reunion Island was dependent at 88.2 % on fossil fuel imports for its primary energy consumption [48]. In particular, the mobility sector represents a major challenge. Indeed, of all the fossil fuels imported each year, almost half are allocated to the transport sector, of which 70 % are for the road sector only. This represented 450 ktOE in 2021 [48]. This amount has been increasing every year since 2000, and

370 one of the main causes is the inhabitants' heavy dependence on private cars.
371 Traffic jams on the island's various roads are a daily occurrence, and the
372 private car fleet numbered almost 400,000 vehicles at the end of 2019, i.e.
373 almost one car for every two inhabitants [48]. With the aim of the territory to
374 reach energy self-sufficiency by 2030 [49], public transport, already present
375 on the island, will need to be further developed in order to reduce fossil
376 fuel imports in the years to come. Moreover, new technologies will need to
377 be considered, such as electric or hydrogen vehicles, in order to achieve a
378 complete decarbonisation of the road sector.

379 The present study focuses on the coaches of the island's regional bus
380 network. A project for several hydrogen-powered coaches is currently being
381 studied for this network; hydrogen can be seen as a solution for replacing fossil
382 fuels in buses, allowing a better range and a shorter refueling time than with
383 an electric vehicle. In France today, at least four cities are already equipped
384 with hydrogen-powered buses [50]. In the present case, the studied vehicles
385 are coaches, and not buses, more used for long distances and for inter-city
386 travel. For hydrogen vehicles, fuel cell ones (with retrofitting operation or
387 not) will be considered here, as well as vehicles with internal combustion
388 engine, even if nothing is currently available on the market. Also part of the
389 comparison, electricity-powered coaches (with retrofitting operation or not)
390 will be studied.

391 The present work will compare the different technologies installed in the
392 considered vehicles. These are detailed in Table 7. The chemistry of the bat-
393 teries used is detailed because of their differing impact on the environment;
394 the acronym NMC stands for Nickel Manganese Cobalt, while LFP stands

395 for Lithium-iron Phosphate.

396 To estimate the hydrogen demand of the coaches of the regional network,
397 a scenario with a higher daily bus mileage than today is proposed: a 12 %
398 increase in annual mileage, from almost 8 Mkm to almost 9 Mkm [30]. The
399 same number of coaches composing the fleet as today is considered, assuming
400 that they travel more kilometres per day (about a hundred vehicles). Then,
401 three different speed and elevation profiles were recovered, for three different
402 lines of the studied network: two for two regular lines, travelling along the
403 coast, and one for a line with a more marked relief. These data are visible
404 on Figure 3. Speed, latitude and longitude data were collected with the GPS
405 logger application inside one coach during its journey. Elevation data were
406 obtained with GPS Visualizer [52]. In order to deal with measurement errors,
407 the data recorded per second were averaged every 5 seconds. Data with too
408 high elevation differences per second were also corrected. Finally, to estimate
409 energy consumption of the vehicles, data specific to the case study from Table
410 8 were used. The percentage of recovery on downhill sections was taken to be
411 lower than what is used in the literature, because the roads travelled included
412 a large number of curves, making brake use high and recovery low.

413 To produce the energy that will power the coaches, a 100 % renewable
414 electricity mix is simulated. Given the strong political will to reduce car-
415 bon emissions, this objective could be achieved in the years to come. The
416 electricity mix is composed of photovoltaics, hydroelectricity, wind turbines,
417 biomass and biogas. Installed capacities were determined considering current
418 local projects, potential studies and existing planning decisions [32]. Two
419 other short-term scenarios (named Scenario 2 and 3) were simulated in order

Technology	Fuel cell	Hydrogen tanks	Batteries	Reference	Refueling infrastructure
Hydrogen retrofit	150 kW	36 kgH ₂	84 kWh (NMC)	[51]	Electrolyser, compressor, hydrogen stationary storage
Hydrogen coach	180 kW	72.8 kgH ₂	160 kWh (NMC)	[28]	Electrolyser, compressor, hydrogen stationary storage
Electric retrofit	x	x	192 kWh (LFP)	[28]	Slow charging at depots, fast charging at main stops
Electric coach	x	x	375 kWh (LFP)	[28]	Slow charging at depots, fast charging at main stops

Table 7: Data on technologies used in the vehicles.

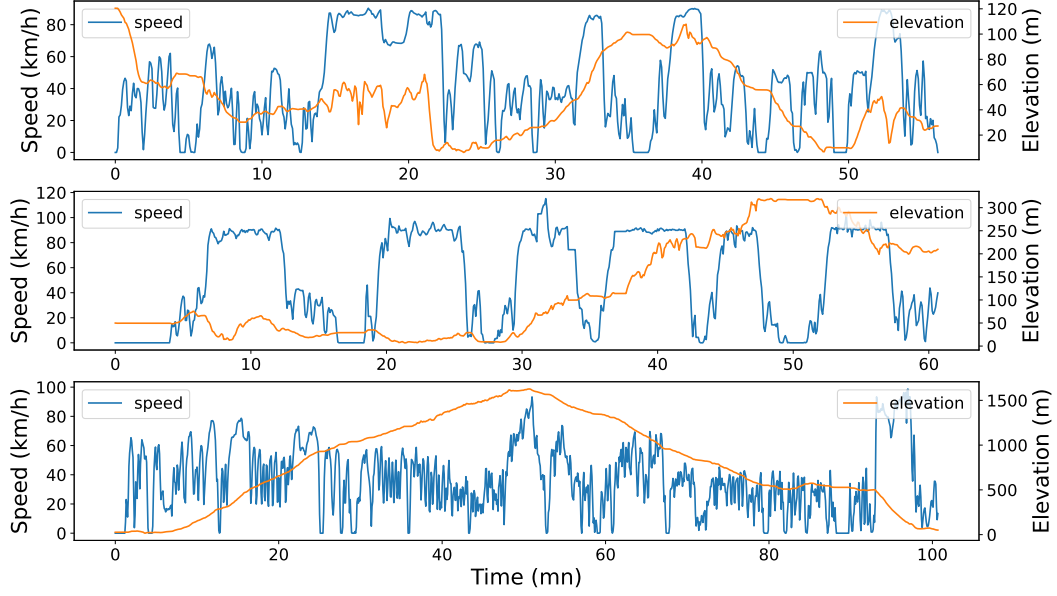


Figure 3: Speed and elevation profiles for three lines of the studied coach network. First line will be called "Regular line 1" in the following, second line "Regular line 2" and third line "Line with marked relief".

Parameter	Symbol	Value	Unit	Reference
Full vehicle mass	m	23	tons	[53]
Frontal area	A	8.59	m ²	[53]
Drag coefficient	C_x	0.66	-	[54]
Rolling resistance coefficient	C_r	0.0075	-	[8]
Air conditioning power	P_{AC}	6 800	W	[55]
Energy recovery	r	20	%	Assumption

Table 8: Parameters used for the estimation of energy consumption.

420 to quantify the impacts of electricity mix on results. Details of these scenar-
421 ios (installed capacity and electricity mix resulting from the simulations) are
422 shown in Table 9.

423 In parallel, for the modelling of the whole electrical system, the base elec-
424 tricity consumption consists of the Energy Efficiency (EE) scenario from [32].
425 This scenario assumes a rather small increase and non-trend consumption in
426 electricity compared to current and historical data, assuming better demand
427 management and energy performance. Moreover, the electricity consumption
428 of individual electric vehicles was not considered as the focus of the paper
429 is on public transport, and the greening of other bus networks' fleets of Re-
430 union Island was not studied as the focus is on the regional lines. Concerning
431 the sizing of the hydrogen infrastructure, two refueling stations with three
432 dispensers each are considered for the modeling of the hydrogen-powered
433 coaches scenario, to be able to charge in coaches in the North and South
434 areas of the island.

435 The fact that the average age of the vehicles in the current fleet of the
436 regional network is less than seven years was obtained from the network
437 operator. Considering that the lifetime of a coach is sixteen years [37], the two
438 economic and environmental criteria will be calculated in the present study
439 for a period of eight years, from year 8 to year 16, following the methodology
440 of [56]. The different scenarios compared are the following:

- 441 • hydrogen retrofit with an electric motor of the diesel coaches (after
442 eight years of operation),
- 443 • scrapping of the diesel coaches (after eight years of operation) and
444 purchase of new hydrogen coaches of a sixteen years lifetime,

- 445 • electric retrofit of the diesel coaches (after eight years of operation),
- 446 • scrapping of the diesel coaches (after eight years of operation) and
- 447 purchase of new electric coaches of a sixteen years lifetime.

448 The only cost needed that is specific to the case study is electricity price,
449 which is taken at 0.1166 €/kWh as current average electricity price excluding
450 taxes in Reunion Island for local authorities with a contract power of more
451 than 250kVA. This choice was made because this price is common to all
452 French territories and its evolution over time is difficult to predict. The
453 impact of the 100 % renewable electricity mix is taken at 123.3 gCO₂eq/kWh,
454 calculated with the average electricity mix resulting from the simulations,
455 visible in Table 9. The other two electricity mix scenarios give impacts of
456 124.7 and 126.2 gCO₂eq/kWh. Scenario 2 represents the island's current
457 situation, with a final combustion turbine using fuel oil. As this turbine
458 only is used for peak demand or when other means of power generation are
459 shut down, the carbon impact of the electricity mix is barely affected. The
460 difference in consumption from one coach integration scenario to another only
461 affects the production of biomass and biogas plants, because of intermittent
462 resources depending on weather conditions, and hydropower resources being
463 often used to the maximum because of its low cost. With data from Table 6,
464 it can be seen that the calculated carbon impact is deteriorated by the high
465 use of biomass and biogas resources on Reunion Island. The emissions on
466 the operation step will be calculated over eight years.

467 Regarding scenarios with electricity-powered vehicles, some additional
468 assumptions were made. Following the data used in [57], it will be assumed
469 that the batteries of the electric vehicles cannot be discharged below 20 %,

Technology	Scenario 1	Scenario 2	Scenario 3
Onshore wind	50 MW	50 MW	91.5 MW
	153 GWh	153 GWh	280 GWh
Photovoltaics	600 MW	600 MW	470 MW
	780 GWh	780 GWh	600 GWh
Hydroelectricity	150 MW	150 MW	146 MW
	800 GWh	800 GWh	778 GWh
Biomass	429 MW	429 MW	429 MW
	1 200 GWh	1 200 GWh	1 300 GWh
Biogas	48 MW	48 MW	48 MW
	210 GWh	210 GWh	210 GWh
Fossil	0 MW	80 MW	0 MW
	0 GWh	10 GWh	0 GWh

Table 9: Details of the installed capacity and average electricity mix resulting from power system simulations.

Scenario	Regular line 1	Regular line 2	Line with marked relief
Electricity consumption	152.1 kWh/100km	176.7 kWh/100km	206.7 kWh/100km
Hydrogen consumption (FC)	9.7 kgH ₂ /100km	11.3 kgH ₂ /100km	13.2 kgH ₂ /100km
Hydrogen consumption (ICE)	11.4 kgH ₂ /100km	13.2 kgH ₂ /100km	15.5 kgH ₂ /100km

Table 10: Results of the consumption study.

nor charged above 80 %, this to preserve their lifetime. Moreover, to estimate the number of fast charging stations required, it will be assumed that the maximum power charging at these stations is 300 kW per dispenser [57].

4. Results and discussion

The technical comparison of the vehicles will first be detailed, with the results of the estimation of their consumption and the sizing of the refueling infrastructures. The calculated TCO and GWP will then be presented.

4.1. Technical comparison

Following the study of the consumption of different types of vehicles, different results were obtained. These are visible in Table 10. In the case of a regular line, it can be seen that the obtained results are close to the data usually used in the literature, whether for electric [58] or fuel cell [11] vehicles. A sensitivity analysis was carried out to assess the uncertainty surrounding the various parameters used to calculate consumption, the results of which

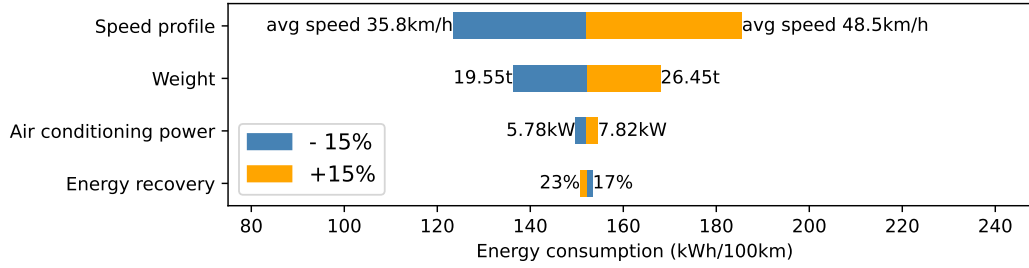


Figure 4: Tornado chart on Regular line 1 consumption showing a $\pm 15\%$ sensitivity analysis on energy consumption of a vehicle.

are visible in Figure 4. If this validates the importance of using a real speed profile and the impact of the mass of the vehicle, it also shows that the uncertainties on the consumption of the air conditioning and the energy recovered in downhill are small. Finally, the results obtained in the case of a line with marked relief show the impact of it on the consumption of the vehicle, with an increase of 36 % of the latter. With regard to the fuel consumption of hydrogen-powered vehicles, a 15 % improvement in the efficiency of the fuel cell (0.54) and the thermal engine (0.46) would lead to fuel consumption of 8.4 kgH₂/100km and 9.9 kgH₂/100km respectively (-13 %) for Regular line 1. It is important to first remember that the operation of the battery inside the hydrogen vehicles has not been simulated and to then specify that the obtained results allow us to estimate an average consumption, but would not be sufficient in the case of sizing on-board technologies. To do that, a more precise study should be carried out.

With this consumption data, the range of the vehicles can be assessed. According to the network operator, some vehicles travel around 400 km per day. In the present study, it is assumed that all the coaches travel an average

Scenario	Electrolysers	Compressors	Hydrogen tanks
FC coaches	3.09 MW / station	2.04 MW / station	2.23 tH ₂ / station
	Total: 6.18 MW	Total: 4.08 MW	Total: 4.46 tH ₂
ICE coaches	3.58 MW / station	2.39 MW / station	2.61 tH ₂ / station
	Total: 7.16 MW	Total: 4.77 MW	Total: 5.22 tH ₂

Table 11: Results of the hydrogen infrastructures sizing. The electricity mix used for the simulation does not have an impact.

of 400 km per day. By grouping the results of Tables 7 and 10, the following conclusions can be drawn. First, if the coaches were all equipped with fuel cells, around two refuelings per day would be required (range of around 300 km). In the case of a vehicle with large on-board storage, such as a new hydrogen coach or one with a combustion engine (without on-board fuel cells, there is more space for storage), two refuelings for three days of operation would be necessary (range of more than 600 km). The results of the hydrogen station refueling infrastructure sizing are shown in Table 11. These data are necessary to evaluate the TCO and GWP of the entire hydrogen chain. It is important to note that the size of the technologies is directly proportional to the total demand for hydrogen on the island. For the same number of stations, if demand is halved, then the size of the technologies will be halved. However, if the number of stations were to change (e.g. 3 stations installed or 4), the total installed hydrogen storage would vary slightly, as shown in [30].

It can be seen that in both scenario a hydrogen storage capacity of more than two tons of hydrogen would be required. This would involve cumber-

518 some administrative procedures in France, as such project must be subject
519 to authorization. Thus, it could be more beneficial to install more refueling
520 stations to spread consumption and reduce administrative procedures. An-
521 other solution could be the removal of the constraint minimizing the size of
522 the storages in order to ensure a minimum supply (Eq. 14 and 15). Finally,
523 a last solution could be the evolution of current regulations, taking the ex-
524 ample of Germany, where hydrogen storage can reach 3 tons on the same site
525 before undergoing heavier procedures [59].

526 For electricity-powered vehicles, the problem is addressed from another
527 side. It is assumed that batteries cannot be discharged below 10 %, nor
528 charged above 95 % [8]. This constraint directly impacts the range of the
529 vehicles considered. Thus, for a retrofitted vehicle, the range will be around
530 117 km for a regular line and around 93 km for a line with marked relief.
531 For a new electric coach, the range will be around 228 km for a regular line
532 and around 181 km for a line with marked relief. Regarding the vehicles
533 recharging time, it is assumed for the case study that a vehicle should not
534 have to stop for more than 5 minutes during a race to charge its battery. This
535 would mean that a maximum of only 25 kWh could be charged with a power
536 of 300 kW. With the consumption data obtained in Table 10, this corresponds
537 to 15 km on a route with little relief. Considering the lengths of the different
538 lines composing the network and although the consumption of the vehicles
539 was overestimated by taking a full coach and a high consumption of air
540 conditioning, it seems technically difficult to consider vehicles with electric
541 retrofit for the entire studied network (longest journey is 110 km long and
542 has very few stops). Indeed, if it is assumed that a vehicle cannot be fully

recharged during the day (because of charging time, availability of operators, impacts on the grid or impacts on battery lifetime), the use of retrofitted electric coaches is not possible. The implementation of new electric coaches could be possible with the use of fast charging stations and with a reduction in the daily mileage of some vehicles, but seems difficult in the case of lines with marked relief. Therefore, from a technical point of view, it is better not to implement the transition of Reunion Island's coach network using only electric vehicles, as they are currently available on the market and with current charging technologies.

However, the optimal composition of the fleet between electric and hydrogen vehicles, as well as the daily mileage of each vehicle will not be studied here. This would require more data on the network, such as the number of vehicles per line or the location of depots and the distances travelled by the vehicles between their commercial journeys. In this way, the total cost of ownership of fleets composed of a single type of vehicle will be evaluated. This will enable to set limits on the TCO of an optimum fleet. The GWP of the different types of bus will then be evaluated.

4.2. TCO

For the assessment of the total cost of ownership, coaches burning hydrogen will not be considered because of missing data. The obtained results are visible in Table 13.

The calculated TCO shows a clear difference between a hydrogen technology and an electric one. As can be seen in Table 13, in the case of the modelled coach fleet, a hydrogen fleet would have a TCO in euros per kilometre around 2 times higher than the one of an electric fleet. This result

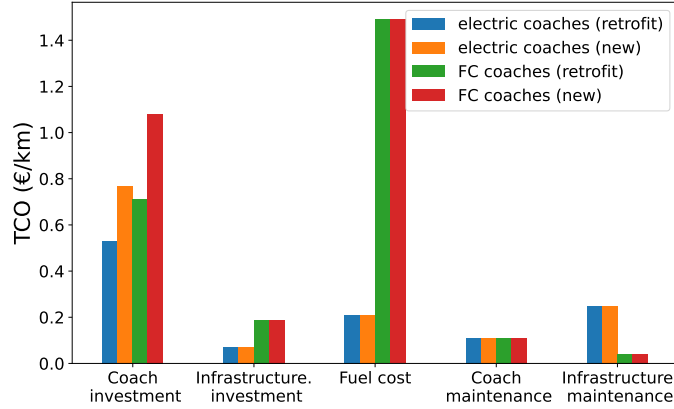


Figure 5: Details of the breakdown of the TCO. The electricity mix used for the simulation does not have an impact.

568 validates the economic optimality of having a fleet made up of both battery
 569 and fuel cell vehicles, so as to reduce the TCO of a fleet made up exclusively
 570 of the latter. Details of these costs are shown in Figure 5. The main differ-
 571 ence between the two technologies lies in the cost of powering the vehicles.
 572 Indeed, powering hydrogen coaches requires more electricity, and the oper-
 573 ating cost of the electrolyzers as well as the electricity consumption of the
 574 compressors have to be taken into account. Finally, it is important to note
 575 that, as this TCO criterion depends on the kilometres travelled, the obtained
 576 results will vary according to the configuration of the network and the lines.

577 Given the large difference in TCO for hydrogen coaches, a sensitivity
 578 analysis was carried out to identify the parameters with the greatest influ-
 579 ence on this criterion, and thus study the possible evolution of the obtained
 580 results in the coming years. Knowing that half of the TCO comes from fuel
 581 supply, this analysis is carried out on coach consumption (a parameter that
 582 also influences infrastructure sizing), electricity cost and operating cost of

583 the electrolyser. Another parameter is also studied as source of uncertainty
 584 in the modelling: the investment cost of the retrofit, as well as that of the
 585 electrolyser, compressor and hydrogen tank technologies. The results of the
 586 sensitivity analysis are shown in Figure 6. As expected, the average con-
 587 sumption of the hydrogen coaches is the parameter with the highest impact
 588 on the TCO. To have a TCO lower than the one of electric vehicles, if only
 589 the consumption of hydrogen coaches varied, it would take a 66 % reduc-
 590 tion in consumption, namely a consumption of 3.7 kgH₂/100km. As seen
 591 above, consumption can be decreased, but probably not at such a level. To
 592 have a competitive TCO, all costs for hydrogen technologies should decrease.
 593 However, while the cost of hydrogen seems set to fall [41, 60], the price of
 594 electricity could rise in the years ahead. The price of electricity in households
 595 has been rising steadily since 2007 [61], with an increasing rate of 41.8 % be-
 596 tween January 2018 and January 2024. If the price of electricity were to rise
 597 in the same way between now and 2030, it could reach 0.1653 €/kWh ex-
 598 cluding taxes in the medium term for local authorities with a contract power
 599 of more than 250 kVA. This would imply an increase in the TCO of 10.6 %
 600 (2.81 €/km) and 9.6 % (3.19 €/km) respectively for a hydrogen retrofit sce-
 601 nario and the purchase of new hydrogen coaches. For fully electric vehicles,
 602 the increase in the TCO would be 7.5 % (1.25 €/km) in the case of a retrofit,
 603 and 6 % (1.48 €/km) in the case of a new fleet.

604 Finally, the choice of calculating the TCO over an 8-year period may be
 605 questioned. This choice was made in order to compare both retrofit opera-
 606 tions and new vehicle purchases. In the case of a longer-term study, more
 607 data would be needed, such as the replacement of technologies in vehicles

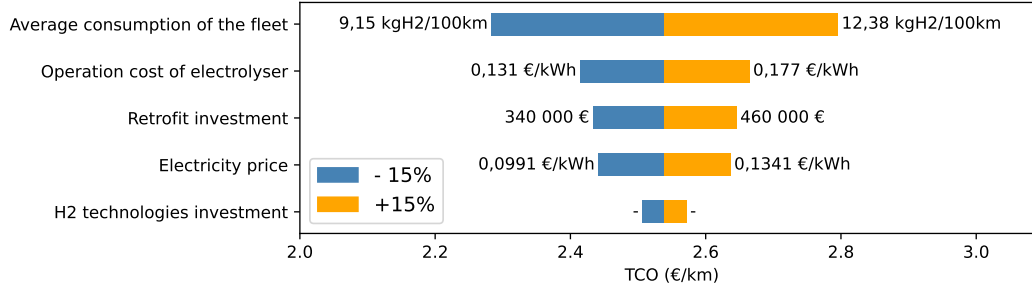


Figure 6: Tornado chart for the hydrogen coaches showing a $\pm 15\%$ sensitivity analysis on TCO. The low values of investment of electrolyzers, compressors and hydrogen tanks are respectively 348.5 €/kW, 467.5 €/kW and 1 147.5 €/kgH₂. Their high values are respectively 471.5 €/kW, 632.5 €/kW and 1 552.5 €/kgH₂.

(battery, fuel cell). However, the obtained results are consistent with those of [6], which compares electric buses (TCO of 1.45 €/km) and fuel cell buses (TCO of 2.7 €/km) with the same methodology. Other electric/hydrogen comparison studies show quite different results for hydrogen like [4] (TCO around 0.9 €/km for electric buses and around 1.4 €/km for fuel cell buses). This could be due to the lower fuel consumption of hydrogen vehicles (taken at 8 kgH₂/100km), but other parameters could influence, explaining the difference in ratio between hydrogen/ electric vehicle types (56% in the article, 89% in the present study).

4.3. GWP

Concerning the calculation of the GWP, the impacts obtained for the transport phase of the technologies are first presented in Table 12. It is assumed that all elements of new hydrogen coaches have to stop in Portugal, place where the vehicles considered in the present study are manufactured. As expected, this step has a small impact over the whole GWP.

Technology	Application	Country of origin	GWP from transportation
LFP battery	New electric coach	China	1.962 kgCO ₂ eq/kWh
LFP battery	Electric retrofit	France	0.886 kgCO ₂ eq/kWh
NMC battery	Hydrogen retrofit	Mainland France	0.717 kgCO ₂ eq/kWh
NMC battery	New hydrogen coach	Turkey	4.418 kgCO ₂ eq/kWh
Fuel cell	Hydrogen retrofit	Mainland France	0.269 kgCO ₂ eq/kW
Fuel cell	New hydrogen coach	Japan	3.426 kgCO ₂ eq/kW
Hydrogen tank	Hydrogen retrofit	South Korea	0.270 kgCO ₂ eq/kWh
Hydrogen tank	New hydrogen coach	Japan	1.590 kgCO ₂ eq/kWh

Table 12: GWP data from the transportation step.

Then, the results obtained by calculating the GWP are presented. In each case, results presented are for one coach, not for the whole fleet, and only take into account the impact of the batteries, fuel cells or hydrogen tanks inside the vehicle, as well as the operation of the vehicle. The obtained results are visible in Table 13. As can be seen, the impact of the operation phase for eight years is far greater than the impact of the other steps: up to 17 times larger in the case of a hydrogen retrofit (with a 100 % renewable and local electricity mix in Reunion Island). This can be seen in Figure 7, where the composition of the GWP of all scenarios is detailed.

Regarding the vehicle with hydrogen retrofit, its GWP is lower than the one of a new electric vehicle, by considering only the technologies composing it, but becomes significantly superior by taking into account the operation phase over eight years. These results show the importance of having a decarbonated electricity mix, a low consumption of the coaches and a high

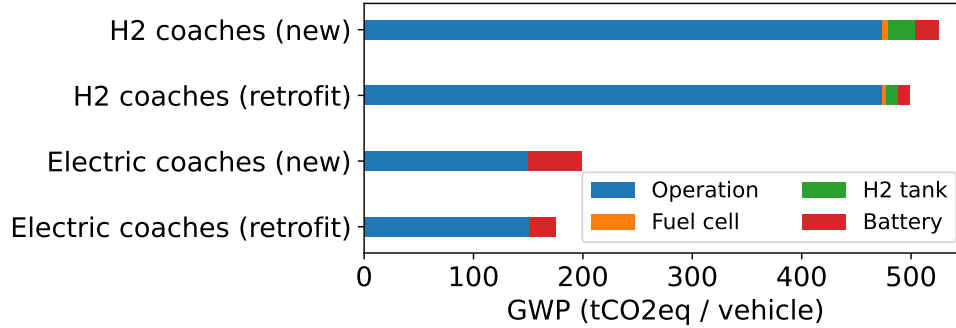


Figure 7: Details of the breakdown of the GWP with a simulation with Scenario 1 electricity mix.

637 efficiency of the hydrogen production chain. Indeed, all these parameters are
 638 the reason of the higher impact of the hydrogen vehicles on the operation
 639 stage; if the electricity mix used had a carbon impact of 10 gCO₂eq/kWh, the
 640 overall GWP of the two vehicles (hydrogen retrofit and new electric) would
 641 be equivalent. Scenario 2, with a slightly more carbon-intensive mix, implies
 642 a 1 % increase in GWP, while Scenario 3 implies a 2 % increase in GWP due
 643 to a greater use of biomass.

644 If no recycling step was considered in every scenario, the GWP of the tech-
 645 nologies in the retrofit hydrogen scenario would be 30.6 tCO₂eq, 59.3 tCO₂eq
 646 in the new hydrogen coach scenario, 43.9 tCO₂eq in the electric retrofit sce-
 647 nario and 86.1 tCO₂eq in the new electric coach scenario. This shows the
 648 importance of considering battery recycling when studying the installation
 649 of new vehicles. As a reminder, the recycling phase will have an impact on
 650 the extraction and production of raw materials, by using recycled materials.

651 The obtained results can be compared with those of [13]. In the arti-
 652 cle, the authors propose several scenarios, considering different vehicle con-

sumption and different electric mix. A scenario in particular is similar to the present study, with consumption of vehicles close (120 kWh/100km and 9 kgH₂/100km), and also a composition of electric mix close (half solar - half waste-energy with carbon capture). In this scenario, the GWP is equal to 26.9 kgCO₂eq/100km for electric vehicles, and has a value of 99.2 kgCO₂eq/100km for fuel cell vehicles.

If a similar study were to be conducted in a few years, the results would probably be different. Indeed, certain resources used in one technology or another could become scarce. This could be due to a number of factors: scarcity of raw materials [62], monopolies held by one country over part or all of a sector [63], diplomatic or armed conflicts that could lead to disruption of the sector or embargoes, pandemics, etc. However, these topics are difficult to predict.

4.4. Other impacts

Other environmental impacts like pollutant emissions of nitrogen oxide, carbon oxide, hydrocarbons or fine particles could have been assessed. Regarding the operation phase of the vehicles, all these emissions would be 0 in the case of a vehicle with an electric motor [58]. However, if hydrogen were to be burned in an ICE, these emissions would not be null. Indirect costs would also be generated, for example on the healthcare system [64].

As a common subject for interrogation, water consumption of hydrogen-powered coaches was evaluated. With a data of 11 liters of water required to produce 1 kg of hydrogen [65], 10 621 m³ would be required for one year to power the whole hydrogen coaches fleet. This represents around 0.7 % of the island's daily requirements (drinking water supply, irrigation, industry)

678 [66]. This criterion can therefore be neglected. As a comparison, it would
679 take $12\,423\text{ m}^3$ to fuel hydrogen-powered vehicles in an ICE (0.8% daily re-
680 quirements).

681 It is also important to have an idea of consumers attitude toward new
682 technologies in mobility. Indeed, if collective transport using different tech-
683 nologies basically offers the same service at the same price, consumption
684 choice then deals mostly with technology acceptance. In general, the liter-
685 ature on hydrogen technologies seems to show a high acceptance, but also
686 that a large part of the population lack knowledge and have a volatile posi-
687 tioning toward hydrogen [67, 68]. Moreover, some papers study the positive
688 willingness to pay for the air pollution reduction associated with hydrogen
689 buses [69]. Finally, it has been shown in the literature that decision to adopt
690 alternative fuel vehicles for public transportation does not really depend on
691 end users. However, it would seem that the barrier for alternative fuel public
692 transportation was more related to entrepreneurs and companies' choices [70]
693 as they mostly consider operating and acquisition costs.

694 5. Conclusion

695 The aim of the presented work was to carry out a comparison of the
696 technical, economic and environmental aspects of different means of electric
697 and hydrogen public transport, applied to Reunion Island. In particular,
698 one type of vehicle were studied, coaches. The study began by estimating
699 the energy consumption of the vehicles with real-data profiles, in order to
700 not have a study with underestimated consumptions. Then, the range and
701 recharging time of the vehicles was estimated. The first conclusions ruled out

Scenario	Vehicle consumption (average)	Range (km)	Annual electricity consumption	Infrastructure required	TCO (€/km)	GWP without operation phase (tCO ₂ eq)	GWP with operation phase (tCO ₂ eq)
Electric coaches (retrofit)	178.5 kWh/100km	108	16 GWh	2 stations	1.16	24.6	175.1
				6 fast-charging stations			(28.4
				6 dispensers			kgCO ₂ eq/100km)
				2 stations			199.0
Electric coaches (new)	178.5 kWh/100km	210	16 GWh	6 fast-charging stations	1.39	48.5	(32.3
				6 dispensers			kgCO ₂ eq/100km)
				5.6 MW electrolyser			499.1
				4.1 MW compressor			(81.1
FC coaches (retrofit)	11.4 kgH ₂ /100km	316	45.5 GWh	4.5 tH ₂ tank	2.54	25.8	kgCO ₂ eq/100km)
				2 stations			
				6 dispensers			
				5.6 MW electrolyser			
FC coaches (new)	11.4 kgH ₂ /100km	639	45.5 GWh	4.1 MW compressor	2.91	51.6	524.9
				4.5 tH ₂ tank			(85.3
				2 stations			kgCO ₂ eq/100km)
				6 dispensers			
ICE coaches	13.4 kgH ₂ /100km	~540	53.2 GWh	6.5 MW electrolyser	unknown	[25, 50]	[525, 550]
				4.8 MW compressor			
				5.2 tH ₂ tank			
				2 stations			
				6 dispensers			

Table 13: Results of the assessment of the different scenarios.

702 electrical retrofitting operations on the vehicles of the current fleet, as well as
703 the exclusive use of new electric coaches considering current range required
704 for the network. The use of hydrogen-powered vehicles would make it possi-
705 ble to overcome the problems of both range and recharging time. Thus, the
706 infrastructure required for hydrogen production were looked at, a step which
707 is sometimes overlooked in the literature, yet essential if all the impacts of a
708 hydrogen vehicle are to be taken into account. Once this sizing was carried
709 out, it was possible to compare the electricity consumption of the vehicles,
710 their total cost of ownership and their global warming potential. From an
711 economic point of view, the obtained results are consistent with those in the
712 literature, which conclude that hydrogen vehicles are more expensive today
713 than battery-powered ones. If a fleet made up of different types of vehicles
714 were to be optimised, it would be economically more interesting to have more
715 electric vehicles than hydrogen ones. Then, from an environmental point of
716 view, the comparison between the vehicles was made by considering the dif-
717 ferent stages in the life cycle of the technologies present in the vehicles, as
718 well as the operation phase of the latter. This distinction was not neces-
719 sarily relevant, given the current overwhelming impact of vehicle operation.
720 As a result, with a lower electricity consumption, the comparison of envi-
721 ronmental impact comes down in favour of electric vehicles. Finally, if both
722 technologies provide the same quality of service to users, the social impact of
723 manufacturing technologies or installing refueling stations was not assessed
724 in the study.

725 In the article, the use of internal combustion engines burning hydrogen
726 was compared to the other solutions in the majority of criteria. The ad-

727 vantages of such a solution lie mainly in the fact that it does not use rare
728 materials (compared to fuel cell vehicles), is tolerant of the use of less pure
729 hydrogen and is faster to deploy [71]. This first point has been partially
730 evaluated with the GWP, the fuel cell being the least impacting technology
731 compared with battery and hydrogen tanks. As hydrogen is only produced
732 from water electrolysis in this study, the second point is not a major con-
733 straint on the deployment of hydrogen-powered mobility. Finally, as this
734 solution is not yet deployed on the market, unlike fuel cell solutions, the last
735 point cannot be verified. However, if this were to be the case, it is possi-
736 ble that it would be more attractive to deploy hydrogen ICE engines, for
737 environmental and economic reasons.

738 As mentioned in the development, the transport networks scheduling has
739 not been optimised, due to too much uncertainty about the future place that
740 will be allocated to public transport on Reunion Island. Once this has been
741 done, it will be possible to re-apply the methodology presented in this paper,
742 optimise recharging times [72] and compare the new obtained results. The
743 number of buses in the network and their routes can also be optimised to
744 favour one type of vehicle over another. In the case studied here, it has been
745 shown that electric vehicles alone cannot be deployed locally, because of the
746 local topography and the daily distance covered by vehicles, and that a tech-
747 nological mix can be considered for economic and environmental reasons.
748 Indeed, as discussed in [7] battery and hydrogen technologies are comple-
749 mentary, and can coexist in the same territory. In a future study, other fuels
750 could be considered for the study case [73, 74].

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757 **CRedit authorship contribution statement**

758 **Agnès François:** Conceptualization, Methodology, Investigation, Soft-
759 ware, Formal analysis, Writing - Original Draft. **Robin Roche:** Conceptu-
760 alization, Supervision, Project administration, Writing - Review and Edit-
761 ing. **Dominique Grondin:** Conceptualization, Supervision, Writing - Re-
762 view and Editing. **Nastasya Winckel:** Investigation, Writing - Review and
763 Editing. **Michel Benne:** Conceptualization, Supervision.

764 **Declaration of competing interest**

765 The authors declare that they have no known competing financial inter-
766 ests or personal relationships that could have appeared to influence the work
767 reported in this paper.

768 **Data availability**

769 Data will be made available on request.

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