1	Correlation between structural and optical properties of WO <sub>3</sub> thin films sputter
2	deposited by glancing angle deposition
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4	Cédric CHARLES <sup>a</sup> , Nicolas MARTIN <sup>a, 1</sup> , Michel DEVEL <sup>a</sup> , Julien OLLITRAULT <sup>a</sup> ,
5	Alain BILLARD <sup>b</sup>
6	
7	<sup>a</sup> Institut FEMTO-ST, UMR 6174 CNRS, Université de Franche-Comté, ENSMM, UTBM
8	32, Avenue de l'observatoire, 25044 BESANCON Cedex, France
9	
10	<sup>b</sup> LERMPS, UTBM, Site de Montbéliard, 90010 BELFORT Cedex, France

<sup>&</sup>lt;sup>1</sup> Author to whom correspondence should be addressed: Tel.: +33 (0)3 81 85 39 69; Fax: +33 (0)3 81 85 39 98; Email: nicolas.martin@femto-st.fr

# 11 Abstract

Tungsten oxide WO<sub>3</sub> thin films are prepared by dc reactive sputtering. The GLancing Angle 12 Deposition method (GLAD) is implemented to produce inclined columnar structures. The incident 13 angle  $\alpha$  between the particle flux and the normal to the substrate is systematically changed from 0 14 to 80°. For incident angles higher than 50°, a typical inclined columnar architecture is clearly 15 produced with column angles  $\beta$  well correlated with the incident angle  $\alpha$  according to conventional 16 relationships determined from geometrical models. For each film, the refractive index and 17 extinction coefficient are calculated from optical transmittance spectra of the films measured in the 18 19 visible region. The refractive index at 589 nm drops from  $n_{589} = 2.18$  down to 1.90 as  $\alpha$  rises from 0 to 80°, whereas the extinction coefficient reaches  $k_{589} = 4.27 \times 10^{-3}$  for an incident angle  $\alpha = 80^{\circ}$ , 20 which indicates that the films produced at a grazing incident angle become more absorbent. Such 21 changes of the optical behaviours are correlated with changes of the microstructure, especially a 22 porous architecture, which is favoured for incident angles higher than 50°. Optical band gap  $E_{g}$ , 23 Urbach energy  $E_u$  and birefringence  $\Delta n_{617}$ , determined from optical transmittance measurements, 24 are also influenced by the orientation of the columns and their trend are discussed taking into 25 account the disorder produced by the inclined particle flux. 26

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## 28 Keywords

WO<sub>3</sub> films, GLAD, inclined columns, refractive index, porosity, optical band gap, Urbach energy,
birefringence.

# 31 **1. Introduction**

Transition metal oxides represent a very attracting class of materials because of the wide range of 32 physical and chemical properties that they exhibit. Among these oxide compounds, tungsten oxide 33 34 thin films have been extensively investigated due to their important applications as active layers for electrochromic window devices [1-4], sensors for toxic gases [5-8], optical coatings with high 35 refractive index [9, 10] or transparent and low resistive oxide materials [11, 12]. It is well known 36 that many chemical and physical characteristics of metal oxide thin films are strongly connected to 37 their chemical composition, especially the oxygen-to-metallic concentrations ratio, which can be 38 tuned in order to get a metallic, semi-conducting or insulating behaviour according to the metalloid 39 content in the film [13-16]. However, playing with the chemical composition is not the only 40 approach to tune the properties of metal oxide thin films. The structure at the sub-micrometric scale 41 can also influence the film performances for many applications [17]. So, the design and the growth 42 control of nanostructures in thin layers appear as important issues, e.g. in order to control the optical 43 properties by playing on structural features. To this aim, various strategies have been proposed for 44 45 the structuration of thin films [18].

In the last decade, the interest of nanostructuration by evaporation and/or sputtering techniques was 46 particularly boosted by the GLancing Angle Deposition (GLAD) method [19]. This method is based 47 on the preparation of thin films on fixed or mobile substrate, with an oblique incidence of the 48 incoming particle flux. Indeed, when the atomic vapour flow comes up at a non normal incident 49 angle  $\alpha$ , the nucleation sites intercept the flow of particles. This creates a shadowing effect and 50 there is a tilted grain growth of columnar shape leading to inclined columnar structures with an 51 angle  $\beta$  with respect to the normal of the substrate surface. Nature, crystallography, temperature and 52 surface conditions of the substrate, energy and interactions of the condensed particles with the 53 substrate, among other parameters, have a decisive role in the growth mode of the coating. As a 54 result, the GLAD technique can control the structure of thin films at the micro- and nanoscales. The 55 experimental setup has two degrees of freedom: a rotation axis at an angle  $\alpha$ , which allows to vary 56

the incident angle of the particle flux, and a rotary axis at an angle  $\phi$  (also called azimuth angle), 57 which modifies in an indirect way, the position of the particle source. The produced architectures 58 can be of type i) columnar and inclined; ii) chevron or zigzag by alternating periodically the 59 incident angle of particles from  $+\alpha$  to  $-\alpha$  maintaining constant  $\phi$  angle (azimuthal angle around the 60 substrate) or with a 180° rotation of  $\phi$  keeping constant  $\alpha$  angle; iii) spiral or helical thanks to a 61 continuous rotation of  $\phi$  at a constant incident angle  $\alpha$ . This latter type adds to the potential of the 62 GLAD technique. Morever, changing wisely  $\alpha$  and  $\phi$  angles as well as speeds of rotation, more 63 original structures can be obtained such as porous columnar structures with variable diameters [20] 64 or helical columns with squared sections [21]. In the end, the GLAD technique exploits the effects 65 of shadowing created by a tilted substrate relative to normal incidence and a change of the direction 66 of the particle flux through a rotation of the same substrate during the deposition. The two 67 68 combined can generate different forms of columns and varied architectures. For example, Robbie et al. [22, 23] or Van Popta et al. [24] have deposited by evaporation some structured films with 69 columnar architectures showing sinusoidal, helical and more complex forms. This variety allows 70 envisaging applications in many fields such as biomedical system [25], photonic devices [26], 71 microsensors [27], etc. Moreover thin films deposited by GLAD have high porosity and anisotropic 72 behaviours, which can be used as rugate filters [28], wavelength-selective polarizer [29], or 73 antireflection coating [30]. 74

The purpose of this article is to study the structural and optical properties of the sputter deposited 75 tungsten oxide WO<sub>3</sub> nanostructured thin films grown using various incident angles  $\alpha$  of the particle 76 flux from 0 to 80°. We systematically investigate how the structure and optical properties 77 (refractive index, extinction and absorption coefficients, optical band gap, birefringence) of such 78 oriented thin films can be tuned by changing the incident angle of the sputtered particles. The 79 evolution of the porous structure connected to the columnar orientation is especially analyzed in 80 81 order to discuss and understand some relationships between the architecture of the films and their resulting optical behaviours. 82

## 84 2. Experimental details

WO<sub>3</sub> films were sputter deposited by DC reactive magnetron sputtering using a home made system 85 86 [31, 32]. A tungsten target (5 cm diameter with purity 99.9 at. %) was powered at a constant current density J = 25.5 A.m<sup>-2</sup>, with an argon partial pressure  $P_{Ar} = 0.1$  Pa and an oxygen partial pressure 87  $P_{O2} = 0.08$  Pa. Substrates (grounded and kept at room temperature) were glass plates and (100) 88 silicon wafers. The distance between the target and the substrate was fixed at 60 mm. The growth of 89 the films was stopped at a thickness close to 1 µm thanks to the calibration of the deposition rate. A 90 systematic change of the incident angle from  $\alpha = 0$  to 80° with a 10° increment was performed to 91 92 tune the inclined columnar structure. Films deposited on glass substrates were characterized thanks to optical transmittance spectra measured with a Lambda 900 Perkin Elmer spectrophotometer in 93 the visible range from 1.55 to 3.10 eV (i.e. wavelength in-between 800 to 400 nm). Refractive 94 index, extinction coefficient and absorption coefficient were determined from interference fringes 95 obtained with experimental optical transmittance spectra using Swanepoel's method [32]. Films 96 97 prepared on (100) silicon wafers were cross-sectioned and observed by field effect scanning electron microscopy (SEM) using a JEOL 6400 F. WO<sub>3</sub> structures were also characterized by X-ray 98 diffraction (XRD). Measurements were carried out using a Bruker D8 focus diffractometer with a 99 cobalt X-ray tube (Co  $\lambda_{K\alpha}$  = 1.78897 Å) in a  $\theta/2\theta$  configuration. 100

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### 102 **3. Results and discussion**

# 103 **3.1 Structural characterization**

Tungsten oxide thin films prepared with an incident angle  $\alpha$  lower than 50° do not exhibit a clear inclined columnar structure. A densely packed feature is rather observed with a smooth surface topography. However, a further increase of the incident angle ( $\alpha$  higher than 50°) leads to a rougher film/air interface and a more defined columnar growth. Observations by SEM of surfaces and crosssections of WO<sub>3</sub> thin films sputter deposited with an incident angle  $\alpha$  of 70 and 80° are shown in

figure 1. It is worth of noting that the top of the columns has a rather sharp appearance (Fig. 1a), 109 which is even more emphasized for  $\alpha = 80^{\circ}$  (surface state becomes irregular and more voided as 110 illustrated in figure 1c). Such increase of the surface roughness versus incident angle of the 111 sputtered particles is in agreement with previous investigations focused on metal oxide coatings 112 produced by GLAD [33, 34]. It is mainly attributed to the shadowing effect at the atomic scale, 113 which prevails over the surface diffusion of adatoms as the incident angle rises. The structural 114 anisotropy (formation of growth islands connected to each other by chains perpendicular to the 115 plane of incidence) previously claimed by Tait et al. [35], is slightly marked for sputtered tungsten 116 oxide films. The top of the columns appears more or less connected to each other according to the x 117 direction and perpendicular to the particle flux (Fig. 1a and 1c). 118

Inspection of the cross-sectional view ensures that the GLAD WO<sub>3</sub> films are composed of slanted 119 columns and inter-columnar voids (Fig. 1b and 1d). The columns are inclined towards the direction 120 of the incoming vapour flux. The column angle  $\beta$ , defined as the angle between the substrate surface 121 normal and the long axis of the slanted columns, is measured from the cross-section SEM images. 122 For incident angle  $\alpha$  lower than 50°, the column angle  $\beta$  can not be accurately determined since no 123 clear columnar growth has been produced but a densely packed structure. For higher angles of 124 incidence ( $\alpha > 50^{\circ}$ ), SEM images exhibit morphologies composed by columns and inter-columnar 125 gaps. The columns become increasingly separated and can easily be distinguished at an incident 126 angle  $\alpha$  of 70° and even more at 80°. The resulting column angles  $\beta$  are 50 and 54° for incident 127 angles  $\alpha$  of 70 and 80°, respectively. Such column angles deviate from the empirical tangent rule 128 [36], which predicts 53 and 70°, respectively. This rule provides a first order approximation of the 129 expected  $\beta$  angles. Since the growth can be disturbed by many parameters (temperature, particle 130 energy, pressure), the tangent rule fails to well describe experimental column angles, especially for 131 grazing incident angles. This is indeed relevant for thin films deposited by the sputtering process. 132 where column angles are often lower than those calculated with various ballistic rules [37, 38]. 133 However, our produced WO<sub>3</sub> column angles are in good agreement with relationships proposed by 134

Tait et al. [39]. The sputtering pressure required to maintain the glow discharge restricts the mean 135 free path of the sputtered particles and thus, reduces the shadowing effect. As a result, the 136 theoretical column inclinations predicted by the simple tangent rule is systematically overestimated. 137 138 Since tungsten oxide thin films have been deposited at room temperature (substrate temperature is lower than 0.3 times the melting point of WO<sub>3</sub> compound), one could expect a poorly crystallized 139 material. However, XRD analyses exhibit diffracted signals (Fig. 2). Peaks corresponding to the 140 WO<sub>3</sub> monoclinic structure are clearly identified for incident angles included between  $\alpha = 0$  and 80°. 141 For normal incidence ( $\alpha = 0^{\circ}$ ), as-deposited films are weakly crystallized since the major diffracted 142 peaks exhibit low intensity and the average crystallite size calculated from the Scherrer equation is 143 smaller than 15 nm. An increase of the incident angle  $\alpha$  up to 40° leads to more intense peaks for all 144 crystallographic planes, without any preferential orientation. In addition, the crystallite size reaches 145 30 nm for  $\alpha = 40^{\circ}$  and the diffracted patterns (peaks position, intensity or full-width-at-half-146 maximum) do not evolve as the incident angle  $\alpha$  increases up to 80°. This improved crystallinity as 147 148 a function of the incident angle has also been observed for other ceramic thin films produced by GLAD [40, 41]. In addition, a reverse effect has been observed by others for some materials [42], 149 showing a reduction of the long range order up to an amorphous structure as the incident angle  $\alpha$ 150 rises. As a result, the dependence of crystallinity on the deposition angle has to be considered on a 151 case by case basis and still remains an open question. Nevertheless, it can be correlated with the 152 surface diffusion phenomenon of the sputtered particles. This phenomenon preferentially takes 153 place in the direction of the particle flux, particularly for grazing incident angles. During initial 154 growth and as the incident angle  $\alpha$  increases, the formed islands start collecting more adatoms. 155 They will grow faster and tend to capture more incoming vapour flux, reinforcing the growth of 156 large crystallites at the expense of other grains that are consumed during the process. This possible 157 explanation of the long range crystalline order is in agreement with the increase of the crystallite 158 size reported from XRD measurements since grain size rises from 15 to 30 nm as the incident angle 159  $\alpha$  changes from 0 to 40°, and finally 80°. 160

# 162 **3.2 Optical characterization**

Optical transmittance spectra of tungsten oxide films deposited on glass substrates have been 163 measured in the visible region for various incident angles  $\alpha$  of the particle flux (Fig. 3). As expected 164 for WO<sub>3</sub> compound, typical interference fringes are observed. The films deposited by conventional 165 process ( $\alpha = 0^{\circ}$ ) exhibit the highest amplitudes. For a given wavelength (e.g. 600 nm) the envelop 166 curve is below 70 % for the minimum of transmittance  $(T_{min})$ , whereas it is higher than 91 % for the 167 maximum of transmittance ( $T_{Max}$ ). Amplitude of the fringes is slightly reduced up to an increasing 168 169 incident angle  $\alpha = 40^{\circ}$ . The amplitudes reduction becomes more significant for grazing incident angles, especially for  $\alpha = 80^{\circ}$  since  $T_{min}$  is close to 77 % and  $T_{Max}$  is 88 % at 600 nm. For this high 170 incident angle of 80°, it is also worth of noting that fringes tend to disappear as the wavelength 171 comes closer to the absorption edge (i.e. between 400 and 500 nm), which can be attributed to the 172 enhancement of the light diffusion. This later is not solely due to structural modification in the film 173 (columns are more inclined), but it also comes from an increased surface roughness for incident 174 angles higher than 40°, as previously observed from SEM analyses (Fig. 1) and in agreement with 175 other theoretical and experimental investigations [43]. 176

From optical transmittance measurements of the WO<sub>3</sub> films deposited on glass substrate, refractive 177 178 index n (Fig. 4) and extinction coefficient k (Fig. 5) have been calculated as a function of the wavelength in the visible region using the Swanepoel's method [44]. The refractive index and 179 extinction coefficient dispersion curves of WO<sub>3</sub> films deposited at various incident angles are all 180 fitted by using the Cauchy dispersion equation in the range of wavelengths 400 to 800 nm. Both the 181 optical index and extinction coefficient follow the Cauchy dispersion evolution as a function of 182 wavelength for any incident angle of the particle flux. WO<sub>3</sub> thin films prepared with a normal 183 incidence of the particle flux ( $\alpha = 0^{\circ}$ ) exhibit the highest refractive index together with the lowest 184 extinction coefficient. For a reference wavelength of 589 nm,  $n_{589} = 2.17$  (and  $k_{589}$  is below  $1.42 \times 10^{-10}$ 185 <sup>3</sup>). This value is below that of the bulk WO<sub>3</sub> material since  $n_{bulk} = 2.50$  for the same given 186

187 wavelength [45]. It shows that the films sputter deposited at normal incidence are quite compact but188 nonetheless contain significant amounts of defects and voids.

A systematic change of the incident angle of the particle flux from 0 to 80° leads to a clear decrease 189 190 of the refractive index of tungsten oxide thin films from  $n_{589} = 2.17$  down to 1.90, respectively. This drop becomes very significant when the incident angle is higher than 40°. This effect has already 191 been observed for other metallic oxide thin films prepared by GLAD [46-48]. It is mainly ascribed 192 to the growth of a more porous structure versus incident angle. In evaporation or sputtering 193 processes, the deposited film's planar density is determined by the shadow length and thus, can be 194 tuned by the incident angle  $\alpha$ . Varying the amount of bulk material in the film is a way to change its 195 refractive index. 196

Similarly, extinction coefficient is nearly constant close to  $1.50 \times 10^{-3}$  at 589 nm up to an incident 197 angle of 60°. Hence, it remains close to values corresponding to typical dielectric and transparent 198 compounds. However, for an incident angle of  $80^{\circ}$  where  $k_{589}$  is higher than  $4.27 \times 10^{-3}$ . Such 199 increase of the extinction coefficient correlates with the increase of the surface roughness 200 commonly measured for high incident angles. Indeed, the low values of k in the visible region is a 201 qualitative indication of the good surface smoothness of thin films [49]. Furthermore, the high k202 value obtained for  $\alpha = 80^{\circ}$  suggests the presence of marked inhomogeneities in the films (defects, 203 disordering, oxygen vacancies, surface corrugation), especially a rougher film/air interface favoured 204 for high glancing angles of deposition. 205

The packing density p and, hence, the porosity  $\pi$  of the WO<sub>3</sub> GLAD films ( $\pi = 1 - p$ ) are significant characteristics of sputter deposited materials. They can be calculated based on the effective media approximation, and thus using the mixture rule proposed by Bruggemann [50]:

$$\chi_a \left( \frac{\varepsilon_a - \varepsilon_{eff}}{\varepsilon_a + 2 \times \varepsilon_{eff}} \right) + \chi_b \left( \frac{\varepsilon_b - \varepsilon_{eff}}{\varepsilon_b + 2 \times \varepsilon_{eff}} \right) = 0$$
(1)

210 Where *a* and *b* components are randomly distributed in space with volume fractions of  $\chi_a$  and  $\chi_b$ , 211 respectively ( $\chi_a + \chi_b = 1$ ). The dielectric properties of the medium are described by an effective

permittivity  $\varepsilon_{eff}$ , and that of a and b components are  $\varepsilon_a$  and  $\varepsilon_b$ , respectively. For our films, we 212 considered that a component is the WO<sub>3</sub> bulk material and b component is the vacuum. As a result, 213  $\varepsilon_{eff}$  is the permittivity of the film. Assuming that the bulk tungsten trioxide compound has a 214 refractive index of  $n_b = 2.50$  at 589 nm [45] and from the refractive index of the film  $n_f$  at 589 nm, 215 packing density and so, porosity have systematically been calculated and compared to the refractive 216 index as a function of the incident angle  $\alpha$  (Fig. 6). Refractive index and porosity exhibit a reverse 217 evolution as the incident angle  $\alpha$  rises. WO<sub>3</sub> films deposited by conventional incidence ( $\alpha = 0^{\circ}$ ) 218 show the highest refractive index with  $n_{589} = 2.18$  and thus, the lowest porosity with  $\pi$  lower than 219 21 %. As expected, index is below that of the bulk material because of the total sputtering pressure 220 (0.18 Pa) used to deposit the films. Thermalisation effect of the sputtered particles and especially, 221 222 intrinsic low energy bombardment in sputtered thin films are both influenced by the sputtering pressure. They can favour a structure with an open grain boundaries and large columns, leading to a 223 significant void fraction in the deposited film. As a result, density of WO<sub>3</sub> deposited film is lower 224 than that of the bulk. 225

It is also worth of noting that refractive index and porosity are nearly constant up to an incident 226 angle of 50°. Index rapidly drops from  $n_{589} = 2.14$  down to 1.78 when  $\alpha$  changes from 50 to 80° 227 whereas the porous structure is enhanced and  $\pi$  reaches 45 % for  $\alpha = 80^{\circ}$ . It is mainly attributed to 228 the shadowing effect, which prevails on the surface diffusion of adatoms increasing the deposition 229 angle. These results well agree with previous investigations focused on oxide thin films [47, 48]. 230 Varying the amount of bulk material in the film provides a means of tuning its optical properties 231 according to a monotonic and continuous relationship between n and  $\alpha$ . For highly oblique angles 232  $(\alpha > 80^{\circ})$ , refractive index should approach unity and porosity should tend to 100 %. However, the 233 lowest index and thus the maximum porosity for WO<sub>3</sub> coatings prepared in this study, obviously 234 depend on the film preparation conditions, but the measurements techniques (spectrometry in 235 transmission by Swanepoel's method, ellipsometry) and environment (humidity) can also influence 236 237 the reachable index and porosity values.

Because of the peculiar architecture of the GLAD thin films, anisotropic behaviours like 238 birefringence can also be expected. Thus, transmittance spectra were measured with two x and y 239 orthogonal directions of incident linear polarized light ( $T_x$  and  $T_y$  in the x and y directions, 240 241 respectively and according to axes defined in Fig. 1). The in-plane birefringence is defined as the difference between the two in-plane refractive indices  $\Delta n = n_x - n_y$ , where  $n_x$  and  $n_y$  are determined 242 by the Swanepoel's method from  $T_x$  and  $T_y$ , respectively. Figure 7 illustrates the influence of the 243 incident angle  $\alpha$  on the birefringence  $\Delta n$  calculated at 617 nm. This birefringence first increases 244 with the incident angle then reaches a maximum value of  $\Delta n = 0.023$  for  $\alpha = 50^{\circ}$ . The fact that there 245 is an optimised birefringence was also reported by other authors for ZrO<sub>2</sub> [42], ZnS [48], Ta<sub>2</sub>O<sub>5</sub> [51] 246 or TiO<sub>2</sub> [52] films. Furthermore, the value of the maximum  $\Delta n$  can be enhanced using a serial 247 bideposition technique as described by Hodginkson and Wu [51]. For tilted columnar films 248 prepared from standard oblique deposition, the highly porous structure obtained for the highest 249 incident angles does not improve the optical anisotropy. The optimized birefringence can not solely 250 be connected to the porosity, but rather to the biaxial columnar structure. This latter is especially 251 produced for incident angles close to 60°. From simulations and experiments performed by Tait et 252 al. [35], films produce a columnar structure with columns exhibiting an elliptical section versus the 253 incident angle. A structural anisotropy develops parallel to the substrate surface because of the 254 255 shadowing effect. This effect, mainly in the direction of the incident vapour flux, leads to the formation of growth islands connected to each other by chains perpendicular to the plane of 256 incidence or to the direction of shadowing. The authors established that for an incident angle close 257 to 60°, the shadowing effect prevails on the surface diffusion. By further increasing the  $\alpha$  angle, the 258 number of islands falls because of shadowing effect is even more marked. Consequently, the 259 average distance between islands increases. Then, they become disconnected from each other in all 260 directions, resulting in a loss of anisotropy. 261

The Swanepoel's method can also be used to calculate the evolution of the absorption coefficient  $\xi$ as a function of wavelength. Therefore, the optical band gap  $E_g$  of WO<sub>3</sub> films can be determined from the Tauc's relationship according to the following equation [53]:

$$265 \quad \xi h \upsilon = C \left( h \upsilon - E_g \right)^w \tag{2}$$

Where C is a constant and w is 1/2, 3/2, 2 or 3 for transitions being direct and allowed, direct and 266 forbidden, indirect and allowed, and indirect and forbidden, respectively. The values of optical band 267 gap energy  $E_g$  can be obtained by extrapolating the absorption coefficient to zero absorption in the 268  $(\xi h v)^{1/w}$  against photon energy h v plot. According to Hjelm et al. [54], WO<sub>3</sub> compound exhibits 269 indirect and allowed band gap transitions with w = 2. Thus, the  $E_g$  value was extracted from  $(\xi h v)^{1/2}$ 270 versus hv plot for WO<sub>3</sub> films prepared with different incident angles (Fig. 8). Without inclining the 271 particle flux ( $\alpha = 0^{\circ}$ ), the optical band gap  $E_g$  is 3.11 eV. It is higher than that of the WO<sub>3</sub> bulk 272 material, which is 2.62 eV [55] but in agreement with typical values (more than 3 eV) reported for 273 tungsten trioxide thin films [56]. This high energy gap of oxide thin films compared to the bulk 274 value is mainly associated to the small crystallite size (smaller than 15 nm from XRD results in Fig. 275 2). An increase of the incident angle up to  $\alpha = 60^{\circ}$  does not significantly modify the optical band 276 gap since  $E_g$  slightly decreases down to 3.05 eV. A further increase of the incident angle until  $\alpha$  = 277 80° leads to reduce  $E_g$  down to 2.90 eV. It can not be ascribed to the improvement of the long range 278 order since it was shown from XRD analyses that the crystallite size reaches 30 nm for  $\alpha = 40^{\circ}$  and 279 did not evolve as the incident angle  $\alpha$  increased up to 80° (cf. § 3.1). It is rather correlated with an 280 increase of growth and structural defects, which are favoured for high incident angles. Thus, this 281 decrease of the optical band gap for incident angles higher than 60° could be interpreted as being 282 283 due to more defects in the film, creating more impurity states in the band gap.

It is also worth of noting that these structural defects and the short range order both facilitate the creation of disorder in the material, favouring a tail of density of states. At lower values of the absorption coefficient  $\xi$ , the extent of the exponential tail of the absorption edge is characterized by the Urbach energy  $E_u$  indicating the width of the band tails of the localized states within the optical band gap. It is given by [57]:

289 
$$\xi h \upsilon = \xi_0 \exp\left(\frac{h \upsilon}{E_u}\right)$$
 (3)

Where  $\xi_0$  is a constant. It is obvious that the plot of  $\ln(\xi)$  versus hv should follow a linear behaviour 290 and allows determining the Urbach energy. This latter was systematically calculated and compared 291 to the optical band gap  $E_g$  as a function of the incident angle  $\alpha$  (Fig. 9). An increase of the Urbach 292 energy from  $E_u = 74$  up to 141 meV corresponds to the decrease in the optical band gap from  $E_g =$ 293 3.11 down to 2.90 eV as  $\alpha$  rises from 0 to 80°. A linear evolution of  $E_g$  versus  $E_u$  can be suggested, 294 which is in agreement with past investigations devoted to thin films [58]. It correlates with an 295 improvement of the crystallinity of the films observed from XRD results and corroborates similar 296 linear evolutions previously obtained by others [59] for films going from the amorphous to the 297 polycrystalline structure. A quantitative relationship between the values of  $E_g$  and  $E_u$  under changes 298 in structural site disorder can be determined with linear coefficients closely linked to structural 299 defects in the materials (bond length, bond angle, chemical disorder) [60]. For our WO<sub>3</sub> GLAD thin 300 films, the increase of the local disorder as the incident angle rises (increase of  $E_u$  and reverse 301 302 evolution of  $E_g$ ) can be assigned to the secondary grain growth of the voided columnar structure, especially produced for very high incident angles due to a broad incident flux distribution [61]. As a 303 304 result, the density of defects in the porous structure (e.g. dangling bonds) rises versus the incident angle, leading to higher Urbach energies. 305

# 307 4. Conclusion

Tungsten oxide WO<sub>3</sub> thin films with inclined columnar structures were prepared by dc reactive 308 magnetron sputtering. The glancing angle deposition technique was implemented to deposit these 309 310 oriented columnar architectures. Then, a systematic change of the incident angle of the particle flux was performed from  $\alpha = 0$  to 80°. A clear columnar inclination was produced for incident angles 311 higher than 50°. The resulting columnar angles were tuned from  $\beta = 0$  to 54° leading to an 312 emphasized porous microstructure (45 % of porosity) for the most inclined columns. XRD analyses 313 revealed diffracted signals corresponding to the WO<sub>3</sub> monoclinic structure with an improved 314 crystallinity as the incident angle increased. Similarly, optical properties like refractive index and 315 extinction coefficient were calculated from optical transmittance measurements in the visible 316 region. Refractive index was significantly reduced from  $n_{589} = 2.11$  down to 1.90 as the incident 317 angle increased from  $\alpha = 0$  to 80°. Extinction coefficient remained nearly constant and close to k<sub>589</sub> 318 =  $1.50 \times 10^{-3}$  up to  $\alpha = 60^{\circ}$  then became higher than  $4.27 \times 10^{-3}$  for the highest incident angles. 319 Variations of the optical behaviours were correlated to the highly porous structure. Voids separating 320 the oriented columns become more significant for incident angles higher than  $\alpha = 60^{\circ}$  because of 321 the shadowing effect prevailing over the surface adatoms diffusion. Voids and pinholes observed 322 are asymmetric in the x- and y-directions, which introduce anisotropy and birefringence in thin 323 films. The maximum in-plane birefringence was found to be  $\Delta n = 0.023$  for an incident angle of 324 50°. A linear and reverse evolution of the optical band gap versus Urbach energy was noticed with a 325 systematic change of the incident angle, which was correlated with an increase of the density of 326 defects in the highest porous structures. 327

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## 415 **Figure captions**

416 Figure 1

Surface and cross-section observations by SEM of WO<sub>3</sub> thin films sputter deposited on (100) Si with two different incident angles  $\alpha$  of the sputtered particles: a) and b)  $\alpha = 70^{\circ}$ ; c) and d)  $\alpha = 80^{\circ}$ . Direction of incoming particle flux, incident angle  $\alpha$ , column angle  $\beta$  and (x, y, z) axes are indicated. The scale bar is the same for all images.

421

422 Figure 2

423 X-ray diffraction patterns of the tungsten oxide thin films deposited on (100) Si with various 424 incident angles  $\alpha$  of the particle flux ( $\alpha = 0$ , 40 and 80°). Diffracted signals (\*) corresponding to the 425 monoclinic WO<sub>3</sub> structure are detected (Si = silicon substrate).

426

427 Figure 3

428 Optical transmittance spectra in the visible range of tungsten oxide thin films deposited on glass 429 substrate for incident angles  $\alpha = 0$ , 40 and 80°. Clear interference fringes are measured, which are 430 typical of transparent thin films.

431

432 Figure 4

433 Refractive index n as a function of wavelength  $\lambda$  in the visible range for tungsten oxide thin films 434 deposited on glass substrate with incident angles  $\alpha = 0$ , 40, 60 and 80°. A Cauchy dispersion law 435 was used to fit the evolution of *n* versus  $\lambda$ .

436

437 Figure 5

438 Extinction coefficient k as a function of wavelength  $\lambda$  in the visible range for tungsten oxide thin

films deposited on glass substrate with incident angles  $\alpha = 0, 40, 60$  and  $80^{\circ}$ .

441 Figure 6

Refractive index  $n_{589}$  at  $\lambda = 589$  nm and porosity  $\pi$  of WO<sub>3</sub> thin films versus incident angle  $\alpha$ . Porosity was determined from the packing density based on the Bruggemann effective medium approximation. Incident angles higher than 50° lead to the most significant changes of the refractive index and porosity. Dashed lines are guides for the eye.

446

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447 Figure 7
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In-plane birefringence  $\Delta n$  at  $\lambda = 617$  nm for WO<sub>3</sub> thin films as a function of the incident angle  $\alpha$ . A maximum of anisotropy is obtained for an incident angle of 50°. Dashed line is guide for the eye.

450

451 Figure 8

Typical plot of the absorption coefficient  $(\alpha h v)^{1/2}$  versus photon energy hv for WO<sub>3</sub> thin films prepared for incident angles  $\alpha = 0$ , 40 and 80°. Indirect and allowed transitions were assumed to deduce the optical band gap according to the Tauc's relationship. Solid lines in the figure refer to extrapolation for determining the optical band gap.

456

457 Figure 9

Linear evolution of the optical band gap  $E_g$  as a function of Urbach energy  $E_u$  of WO<sub>3</sub> thin films deposited with a systematic increase of the incident angle  $\alpha$  from 0 to 80°. Dashed line is guide for the eye.



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Figure 3



Figure 4





Figure 5

Figure 6



Figure 7



Figure 8





